

Location Restrictions for Ash Landfill Expansion

Leland Olds Station Basin Electric Power Cooperative Stanton, Mercer County, North Dakota

AECOM Project Number: 60545172 November 20, 2017

Location Restrictions Report Ash Landfill Expansion Leland Olds Station

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Executive Summary

This Locations Restrictions Report for the Basin Electric Power Cooperative Leland Olds Station Ash Landfill Expansion has been prepared in accordance with the requirements specified in 40 Code of Federal Regulations (CFR) §257.60 through §257.64, which states the coal combustion residuals (CCR) Rule requirements for location restrictions¹. More specifically, the location restrictions sections are as follows:

- §257.60 Placement Above the Uppermost Aquifer
- §257.61 Wetlands
- §257.62 Fault Areas
- §257.63 Seismic Impact Zones
- §257.64 Unstable Areas

Each requirement of the CCR Rule requires the owner or operator to obtain certification from a qualified professional engineer stating that the demonstration meets the requirements of the applicable CCR Rule citation prior to placing CCR in the new unit. The Leland Olds Station CCR Ash Landfill Expansion represents a lateral expansion and meets the location restriction requirements, as outlined by this report.

¹ U.S. Environmental Protection Agency. (USEPA). (2015). *Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals From Electric Utilities; Final Rule*, 40 CFR §257. Federal Register, Volume 80, Subpart D, April 17, 2015

1. Introduction

The purpose of the CCR Location Restrictions Report for the Basin Electric Power Cooperative Leland Olds Station Ash Landfill Expansion presented in this report is to document that the requirements in 40 Code of Federal Regulations (CFR) §257.60(a), §257.61(a), §257.62(a), §257.63(a), and §257.64(a) have been met to support certification for the existing active CCR units to remain in operation. These regulations require the owner or operator to obtain certification from a qualified professional engineer stating that the demonstration meets the specified aquifer separation, wetlands, fault distance, seismic acceleration, and unstable area requirements of the CCR Rule prior to placing CCR in the Ash Landfill Expansion area.

2. Facility and CCR Unit Description

Basin Electric Power Cooperative (BEPC) owns and operates the Leland Olds Station (LOS) located near Stanton, Mercer County, North Dakota. The station is located approximately four miles southeast of Stanton along the Missouri River (Figure 2.1-Site Location Map, Appendix A). The LOS is a lignite-based electric generating station with two units that generate a combined power of 669 megawatts. The plant first began commercial operation in June 1966.

As part of their continuing operations, BEPC is planning to expand their current operational ash landfill located at the former Glenharold Coal Mine. The location of the operational landfill and proposed Ash Landfill Expansion area are presented in Figure 2.2 (Site Map) included in Appendix A. The Glenharold Coal Mine was a Coal (Lignite) surface mine that ended operations in 1982. After mine closure, the land was reclaimed beginning with soil replacement in 1985. Reclamation operations were completed at the site in 1996, which included reestablishment of native grasslands, native woodlands, and permanent ponds for use as livestock water source and wildlife habitat.

The primary waste type that will be accepted by the proposed Ash Landfill Expansion will consist of CCR as defined by the United States Environmental Protection Agency (EPA), which includes bottom ash/boiler slag, fly ash and flue-gas desulfurization (FGD) waste, which is a synthetic form of gypsum (calcium sulfate). Minor amounts of other solid wastes generated at the power plant will also be accepted, as authorized in North Dakota Department of Health (NDDH) solid waste management facility permit SP-0143 (NDDH, 2017).

3. §257.60 Placement Above the Uppermost Aquifer

3.1 §257.60(a) Citation

New CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must be constructed with a base that is located no less than 1.52 meters (five feet) above the upper limit of the uppermost aquifer, or must demonstrate that there will not be an intermittent, recurring, or sustained hydraulic connection between any portion of the base of the CCR unit and the uppermost aquifer due to normal fluctuations in groundwater elevations (including the seasonal high water table).

3.2 Separation of Aquifer to Base of CCR Unit

The LOS Ash Landfill Expansion is subject to Section §257.60 of the CCR Rule concerning the placement of the base of the CCR unit above the uppermost aquifer². As stated on page 21362 of the Preamble of the CCR Rule, the base is considered to be located at the bottom of the liner components:

...the minimum vertical separation be at least three to five feet from the base of the liner components. After additional research, EPA is finalizing a minimum buffer of five feet instead of two feet. EPA's research confirmed the commenter's claims. In addition, EPA determined that several states consider five feet between the base of the surface impoundment and the top of the uppermost aquifer to be the minimum distance that is protective of human health and the environment. These are California, Michigan, Nebraska, New York, West Virginia, and Wisconsin. The Agency has concluded from geographic and climatic spacing of these states that the hydrogeologic conditions within them encompass the range of conditions found in the United States. Therefore, EPA is finalizing a minimum buffer of five feet instead of two feet.

Site subsurface investigations have been performed at the site location in 2011 and 2016. In 2011, BEPC contracted Braun Intertec Corporation to perform a site subsurface investigation that included installation of five (5) monitoring wells. In 2016, a supplemental site subsurface investigation was performed by AECOM under contract with BEPC. As part of the supplemental site subsurface investigation, 10 geotechnical soil borings and 11 site characterization borings were completed by Terracon and Cascade drill crews, respectively. In addition, an extensive laboratory testing program was performed on samples recovered from the geotechnical soil borings. Upon boring completion, the 11 site characterization borings were converted into monitoring wells. Locations of the geotechnical borings and monitoring wells installed at the site are shown on Figure B-1 in Appendix B. Additional information regarding drilling and sampling procedures, well installation procedures, and laboratory test results from the 2016 subsurface investigation can be found in the "Supplemental Site Characterization Report (AECOM, 2017)."

Based on the conditions observed during the subsurface investigations performed in 2011 and 2016, the general encountered soil profile consisted of layers of mine spoils underlain by native hard cohesive soils with layers of lignite. Mine spoils within the proposed Ash Landfill Expansion footprint were encountered near ground surface (+1955.4 to +1891.1 feet NAVD29) to depths ranging between 44.5 and 100 feet below ground surface (+1871.9 to +1835.2 feet NAVD29). Laboratory results from the 2016 supplemental investigation indicate that the underlying mine spoil material and native hard cohesive soils are classified as high plasticity clay (USCS: CH). Boring logs containing soil information and depths explored from the 2016 supplemental investigation are presented in Appendix B.

A review of AECOM's drawings for proposed Ash Landfill Expansion base grades indicate that the minimum base liner elevation is +1886 feet NAVD29. The base liner system for the proposed expansion will consist of a 1-foot drainage layer underlain by a 60-mil High Density Polyethylene (HDPE) liner and 2

² Excerpt from the Preamble of the CCR Rule (Page 21362): EPA is revising the definition of "uppermost aquifer" to specify that the measurement of the upper limit of the aquifer must be made at a point nearest to the natural ground surface to which the aquifer rises during the wet season. This definition of "uppermost aquifer" will encompass large seasonal variations, and is more appropriate parameter than "seasonal high groundwater table" as suggested by several commenters and the proposed "natural water table" because it is more clearly defined

feet of compacted clay. When considering the base liner thickness, the minimum subgrade elevation of the proposed Ash Landfill Expansion is +1883 feet NAVD29. The permit drawing of the Ash Landfill Expansion base grades is included in Appendix C.

Of the monitoring wells that have been installed at the site, two (2) of them are within the proposed Ash Landfill Expansion footprint and six (6) are near the footprint perimeter. A quarterly sampling program has been implemented since the installation of the 2011 monitoring wells. In September 2016, water level measurements were performed in the 2011 and in some of the 2016 monitoring wells. The geologic cross sections in Appendix D show the base of the landfill and the piezometric surface derived from water level measurements taken during the September 2016 monitoring event. Groundwater measurements from September 2016 were compared to the minimum subgrade elevation of the proposed Ash Landfill Expansion and are presented in Table 1. In addition, the Ash Landfill Expansion minimum subgrade elevation was also compared to groundwater levels observed since 2011 in monitoring wells within and near the proposed Ash Landfill Expansion footprint and are presented in Appendix Expansion footprint and are presented in Appendix Expansion footprint and are presented in Figure 3.2 included in Appendix E.

Monitoring Well	Groundwater Elevation [NAVD29, ft]	Subgrade Elevation [NAVD29, ft]	Separation Distance [ft]
MW-2011-1 ⁽¹⁾	1847.4	1883.0 ⁽²⁾	35.6
MW-2011-2	1844.9	1883.0 ⁽²⁾	38.1
MW-2011-3	1844.1	1883.0 ⁽²⁾	38.9
MW-2011-4	1843.8	1883.0 ⁽²⁾	39.3
MW-2011-5	1851.0	1883.0 ⁽²⁾	32.0
MW-2016-1 ⁽¹⁾	1836.8	1883.0 ⁽²⁾	46.2
MW-2016-2 ⁽¹⁾	1836.0	1883.0 ⁽²⁾	47.0
MW-2016-3	1839.8	1883.0 ⁽²⁾	43.2
MW-2016-4	1843.0	1883.0 ⁽²⁾	40.0
MW-2016-5	1845.3	1883.0 ⁽²⁾	37.7
MW-2016-6	1847.0	1883.0 ⁽²⁾	36.0
MW-2016-7 ⁽¹⁾	1862.8	1883.0 ⁽²⁾	20.2
MW-2016-8 ⁽¹⁾	1846.2	1883.0 ⁽²⁾	36.8

Table 1. Groundwater Elevation Data from September 2016

Note: (1) The locations of these wells are not within or near the proposed Ash Landfill Expansion footprint

(2) Lowest elevation based on AECOM design drawings. Subgrade elevation at actual well location may be greater than +1883 NAVD29 feet; therefore greater separation distance will exist.

Source: Supplemental Site Characterization Report by AECOM

In summary, the comparison of the minimum subgrade elevation of the proposed LOS Ash Landfill Expansion to the unconfined uppermost aquifer indicates a greater than 5 feet separation exists between the upper limit of the uppermost aquifer and the base of the CCR surface impoundment. In addition, the proposed expansion will have an impermeable HDPE liner and low permeable clay liner that will limit the hydraulic interaction between the landfilled material and the in-place site soils. Therefore, the proposed LOS Ash Landfill Expansion meets the requirements of §257.60(a).

3.3 Federal Requirement [40 CFR § 257.60]

Certification Statement 40 CFR § 257.60 – Placement of the Lateral Expansion of an Existing CCR Surface Impoundment Above the Uppermost Aquifer

CCR Unit: Leland Olds Station Ash Landfill Expansion

I, John Cannon, being a Registered Professional Engineer in good standing in the State of North Dakota, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, for the above referenced CCR Units, that the information contained in the Location Restrictions Report dated November 20, 2017 meets the requirements of 40 CFR § 257.60.

John Cannon Printed Name

November 20, 2017 Date



4. §257.61 Wetlands

4.1 §257.61(a) Wetlands Citation

New CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must not be located in wetlands, as defined in §232.2 of this chapter, unless the owner or operator demonstrates by the dates specified in paragraph (c) of this section that the CCR unit meets the requirements of paragraphs (a)(1) through (5) of this section.

(1) Where applicable under section 404 of the Clean Water Act or applicable state wetlands laws, a clear and objective rebuttal of the presumption that an alternative to the CCR unit is reasonably available that does not involve wetlands.

(2) The construction and operation of the CCR unit will not cause or contribute to any of the following:

(i) A violation of any applicable state or federal water quality standard;

(ii) A violation of any applicable toxic effluent standard or prohibition under section 307 of the Clean Water Act;

(iii) Jeopardize the continued existence of endangered or threatened species or result in the destruction or adverse modification of a critical habitat, protected under the Endangered Species Act of 1973; and

(iv) A violation of any requirement under the Marine Protection, Research, and Sanctuaries Act of 1972 for the protection of a marine sanctuary.

(3) The CCR unit will not cause or contribute to significant degradation of wetlands by addressing all of the following factors:

(i) Erosion, stability, and migration potential of native wetland soils, muds and deposits used to support the CCR unit;

(ii) Erosion, stability, and migration potential of dredged and fill materials used to support the CCR unit;

(iii) The volume and chemical nature of the CCR;

(iv) Impacts on fish, wildlife, and other aquatic resources and their habitat from release of CCR;

(v) The potential effects of catastrophic release of CCR to the wetland and the resulting impacts on the environment; and

(vi) Any additional factors, as necessary, to demonstrate that ecological resources in the wetland are sufficiently protected.

(4) To the extent required under section 404 of the Clean Water Act or applicable state wetlands laws, steps have been taken to attempt to achieve no net loss of wetlands (as defined by acreage and function) by first avoiding impacts to wetlands to the maximum extent reasonable as required by paragraphs (a)(1) through (3) of this section, then minimizing unavoidable impacts to the maximum extent reasonable, and finally offsetting remaining unavoidable wetland impacts through all appropriate and reasonable compensatory mitigation actions (e.g., restoration of existing degraded wetlands or creation of man-made wetlands); and

(5) Sufficient information is available to make a reasoned determination with respect to the demonstrations in paragraphs(a)(1) through (4) of this section.

4.2 Wetlands Study

BEPC contracted AECOM to perform an environmental and wetland delineation within the proposed Ash Landfill Expansion in Mercer County. The purpose of the delineation was to provide a summary of available desktop data and wetland delineations conducted on August 19, 2016 and an evaluation of potential waters of the United States (WOTUS). In addition, a desktop analysis and literature search were also performed to identify federally listed species of concern with potential to occur within the site area. The executive summary and figures from the AECOM report titled, "*Environmental and Wetland Delineation Report for LOS Landfill Expansion*" are included in Appendix F.

A desktop analysis and literature search indicated that seven threatened and endangered (T&E) species of concern with potential to occur within the site area. As part of the analysis, each species was assigned a "determination affect." The assigned determinations for the species identified ranged from "no effect" to "may effect, but not likely to occur."

For the wetlands study, four wetlands were delineated within the site area by AECOM. After evaluation, AECOM concluded that the wetlands appeared to be non-relatively permanent waters (non-RPW) that are formed by geomorphic position, are isolated from jurisdictional waters, and appear without significant nexus. In summary, the delineated wetlands were formed following mine land reclamation when soils settled or as a result of road construction.

4.3 Federal Requirement [40 CFR §257.61]

Certification Statement 40 CFR § 257.61 – Location of the Lateral Expansion of an Existing CCR Surface Impoundment in Wetlands

CCR Unit: Leland Olds Station Ash Landfill Expansion

I, John Cannon, being a Registered Professional Engineer in good standing in the State of North Dakota, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR Unit, that the demonstration that the CCR Unit is not located in wetlands, as included in the Location Restrictions Report dated November 20, 2017 meets the requirements of 40 CFR §257.61.

John Cannon Printed Name

November 20, 2017 Date



5. §257.62 Fault Areas

5.1 §257.62(a) Citation

New CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must not be located within 60 meters (200 feet) of the outermost damage zone of a fault that has had displacement in Holocene time unless the owner or operator demonstrates by the dates specified in paragraph (c) of this section that an alternative setback distance of less than 60 meters (200 feet) will prevent damage to the structural integrity of the CCR unit.

5.2 Distance to Holocene Faults

As stated in the CCR Rule, a CCR unit is considered to be in a fault area if it's within 200 feet of the outermost damage zone of a fault that has seen displacement during the Holocene epoch, or within the last 12,000 years. As stated on page 21366 of the Preamble of the CCR Rule:

To investigate active faults, EPA expects owners and operators of CCR units to follow standard engineering and geologic practices. Technical considerations include:

(1) A geologic reconnaissance of the site to determine the location of active faults. Such a reconnaissance would include utilizing the seismic analysis maps and tools (Quaternary fault maps, earthquake probability maps) of the United States Geological Survey (USGS) Earthquake Hazards Program (http:// earthquake.usgs.gov/hazards/apps/); and

(2) A site fault characterization within 1000 meters of a site to determine whether it is within 60 meters of an active fault. Such characterizations would include subsurface exploration, including drilling or trenching, to locate any fault zones and evidence of faulting, trenching perpendicular to any faults or lineaments found within 60 meters of the site, and determination of the age of any displacements.

AECOM researched the United States Geological Survey (USGS) Geographic Information Systems (GIS) Database for known Holocene faults. Since the Holocene faults are defined within the Quaternary Period, which is the last 2.6 million years to present, a figure presenting a USGS map showing Quaternary faults in proximity to the LOS Ash Landfill Expansion is provided in Appendix G. In addition, the North Dakota Geologic Survey has produced a geologic map of Mercer and Oliver Counties (Appendix G).

Findings from the research performed did not indicate the presence of active faults within 1000 meters of the CCR units. Therefore, no further action (e.g., a site characterization) was performed.

Based on the results of the evaluation described herein, the LOS Ash Landfill Expansion is not located within 60 meters (200 feet) of the outermost damage zone of a fault that has seen displacement during Holocene time.

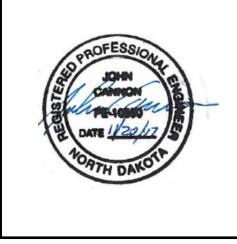
5.3 Federal Requirement [40 CFR §257.62]

Certification Statement 40 CFR § 257.62 – Location of the Lateral Expansion of an Existing CCR Surface Impoundment within 60 Meters of a Fault Area

CCR Unit: Leland Olds Station Ash Landfill Expansion

I, John Cannon, being a Registered Professional Engineer in good standing in the State of North Dakota, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR Unit, that the demonstration regarding that the CCR Unit is not located within 60 meters (200 feet) of the outermost damage zone of a fault that has had a displacement in Holocene time, as included in the Location Restrictions Report dated November20, 2017, meets the requirements of 40 CFR §257.62.





6. §257.63 Seismic Impact Zones

6.1 §257.63(a) Citation

CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must not be located in seismic impact zones unless the owner or operator demonstrates by the dates specified in paragraph (c) of this section that all structural components including liners, leachate collection and removal systems, and surface water control systems, are designed to resist the maximum horizontal acceleration in lithified earth material for the site.

6.2 Seismic Impact Zones

As stated on page 21471, the CCR Rule defines a *seismic impact zone* as "an area having a 2% or greater probability that the maximum expected horizontal acceleration, expressed as a percentage of the earth's gravitational pull (g), will exceed 0.10 g in 50 years". The USGS produced a national map of the two-percent probability of exceedance in 50 years map of peak ground acceleration (Figure 6.1). The LOS Ash Landfill Expansion is in the area of less than 0.1g, and the USGS provides a method to calculate the PGA of specific sites.

The United States Geologic Survey National Seismic Hazards Mapping Project, PSHA Deaggregation program, 2008 version was used to find the PGA for the site location. The results of the Deaggregation program are found in Figure 6.2. The results for the Ash Landfill Expansion are presented in Table 2.

Table 2. Peak Ground Acceleration at Leland Olds Station

Location	Longitude	Latitude	Peak Ground Acceleration
Leland Olds Station	-101.3714	47.2469	0.022 g

The PSHA deaggregation program reports all PGA results for lithified earth materials, which corresponds to seismic site classes A, B, or C. The PGA is below 0.1 g and meets the criteria. Therefore, the LOS Ash Landfill Expansion is not located in a seismic impact zone.

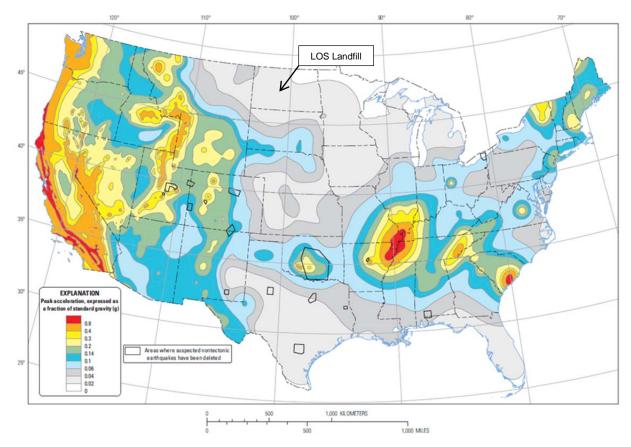
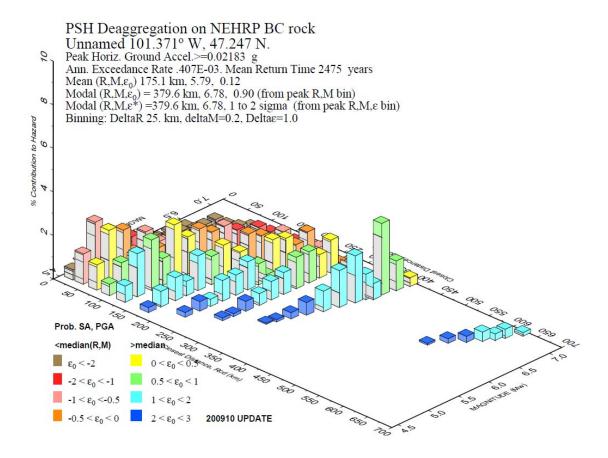


Figure 6.1 Two-Percent Probability of Exceedance in 50 Years Map of Peak Ground Acceleration



CIT Mar 14 13:58:57 Distance (R), magnitude (M), epsilon (E0,E) deaggregation for a site on rock with average vs= 760. m/s top 30 m. USGS CGHT PSHA2008 UPDATE Bins with It 0.05% contrib. omitted

Figure 6.2 The PSHA Deaggregation Program Result (PGA=0.022 g)

6.3 Federal Requirement [40 CFR §257.63]

Certification Statement 40 CFR § 257.63 – Location of the Lateral Expansion of an Existing CCR Surface Impoundment in a Seismic Impact Zone

CCR Unit: Leland Olds Station Ash Landfill Expansion

I, John Cannon, being a Registered Professional Engineer in good standing in the State of North Dakota, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR Unit, that the demonstration that the CCR Unit is not located in a seismic impact zone, as included in the Location Restrictions Report dated November 20, 2017, meets the requirements of 40 CFR §257.63.



John Cannon Printed Name

November 20, 2017 Date

7. §257.64 Unstable Areas

7.1 §257.64(a)-(b) Citation

(a) An existing or new CCR landfill, existing or new CCR surface impoundment, or any lateral expansion of a CCR unit must not be located in an unstable area unless the owner or operator demonstrates by the dates specified in paragraph (d) of this section that recognized and generally accepted good engineering practices have been incorporated into the design of the CCR unit to ensure that the integrity of the structural components of the CCR unit will not be disrupted.

(b) The owner or operator must consider all of the following factors, at a minimum, when determining whether an area is unstable:

- (1) On-site or local soil conditions that may result in significant differential settling;
- (2) On-site or local geologic or geomorphologic features; and
- (3) On-site or local human-made features or events (both surface and subsurface).

7.2 Unstable Areas, Settlement, Collapsible Soils

All CCR landfill lateral expansions are subject to the unstable areas location restriction.

Due to the site history, a geotechnical subsurface investigation was completed as part of the design process. The subsurface investigation included drilling 10 geotechnical soil borings within and near the proposed Ash Landfill Expansion footprint. After completion of drilling activities, a laboratory testing program that included direct shear, triaxial shear, and consolidation testing was completed on select recovered samples. Results from geotechnical drilling and laboratory testing were used to analyze the subsurface foundation soils for settlement and overall stability of base grades based on the proposed Ash Landfill Expansion design. Results from the material tests and the methods used for the geotechnical analysis can be found in the "Supplemental Site Characterization Report (AECOM, 2017b)."

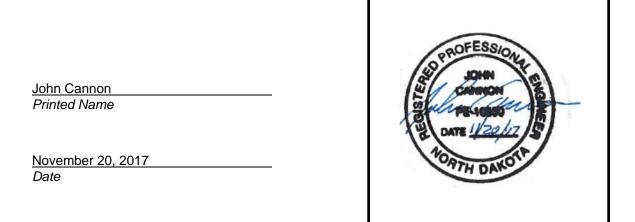
Results from the geotechnical analysis indicated that settlement will occur as the Ash Landfill Expansion is constructed. Although settlement will occur, the anticipated amount will be within tolerance of the landfill design. In addition, results from the stability analysis indicate that proposed base grades of inplace site soils should remain stable during construction. Based on the soils encountered and the geotechnical analysis performed, the expansion is considered to be stable based on the factors outlined in §257.64(b).

7.3 Federal Requirement [40 CFR §257.64]

Certification Statement 40 CFR § 257.63 – Location of the Lateral Expansion of an Existing CCR Surface Impoundment in an Unstable Area

CCR Unit: Leland Olds Station Ash Landfill Expansion

I, John Cannon, being a Registered Professional Engineer in good standing in the State of North Dakota, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR Unit, that the demonstration that the CCR Unit is not located in an unstable area, as included in the Location Restrictions Report, November 20, 2017, meets the requirements of 40 CFR §257.64..



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8. Limitations

In preparing this report, AECOM has reviewed background information, design basis, and other additional data furnished to AECOM by BEPC, as well as relevant available information from previous and current investigations performed by AECOM and others at the site. AECOM has relied on this information as furnished without independent verification, and is not responsible for the accuracy or completeness of this information. AECOM shall not be held responsible for conditions or consequences arising from relevant facts that were concealed, withheld, or not fully disclosed by BEPC at the time this report was prepared. In addition, the conclusions expressed in this report are subject to certain conditions and assumptions, which are noted in this report and below. Any party reviewing this report must carefully review and consider all such conditions and assumptions.

The conclusions made in this report are based on the assumption that the subsurface soil, rock, and groundwater conditions at the site do not deviate appreciably from those conditions disclosed in the site-specific exploratory borings. The conclusions in this report are also based on AECOM's understanding of current plant operations, maintenance, storm water handling, and ash handling procedures at the station based on information provided by BEPC. The passage of time may result in changes in site conditions and variations, technology, economic conditions, and regulatory provisions, all which could render the report inaccurate.

This report was prepared by AECOM in accordance with generally accepted engineering and scientific practice in effect at the time of AECOM's assessment of the subject property. This report was prepared pursuant to an agreement between AECOM and BEPC and is for the exclusive use of the BEPC. Any reliance on this report shall be at the user's sole risk.

9. References

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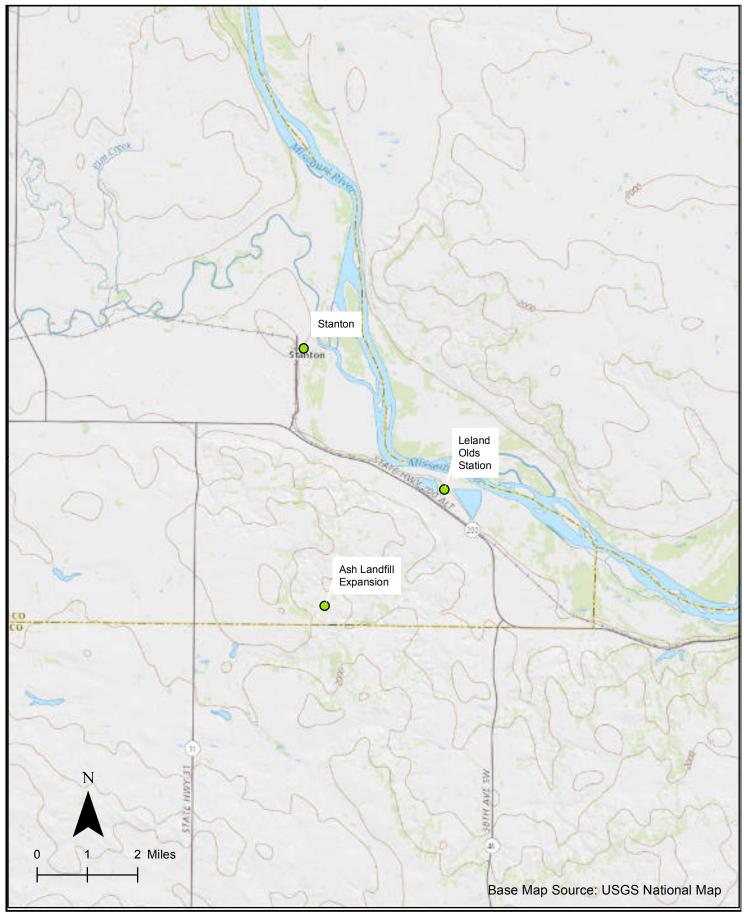
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Appendix A – Site Maps



Location Restrictions Report Basin Electric Power Cooperative Project No.: 60545172 Site Location Map Ash Landfill Expansion Leland Olds Station Mercer County, North Dakota

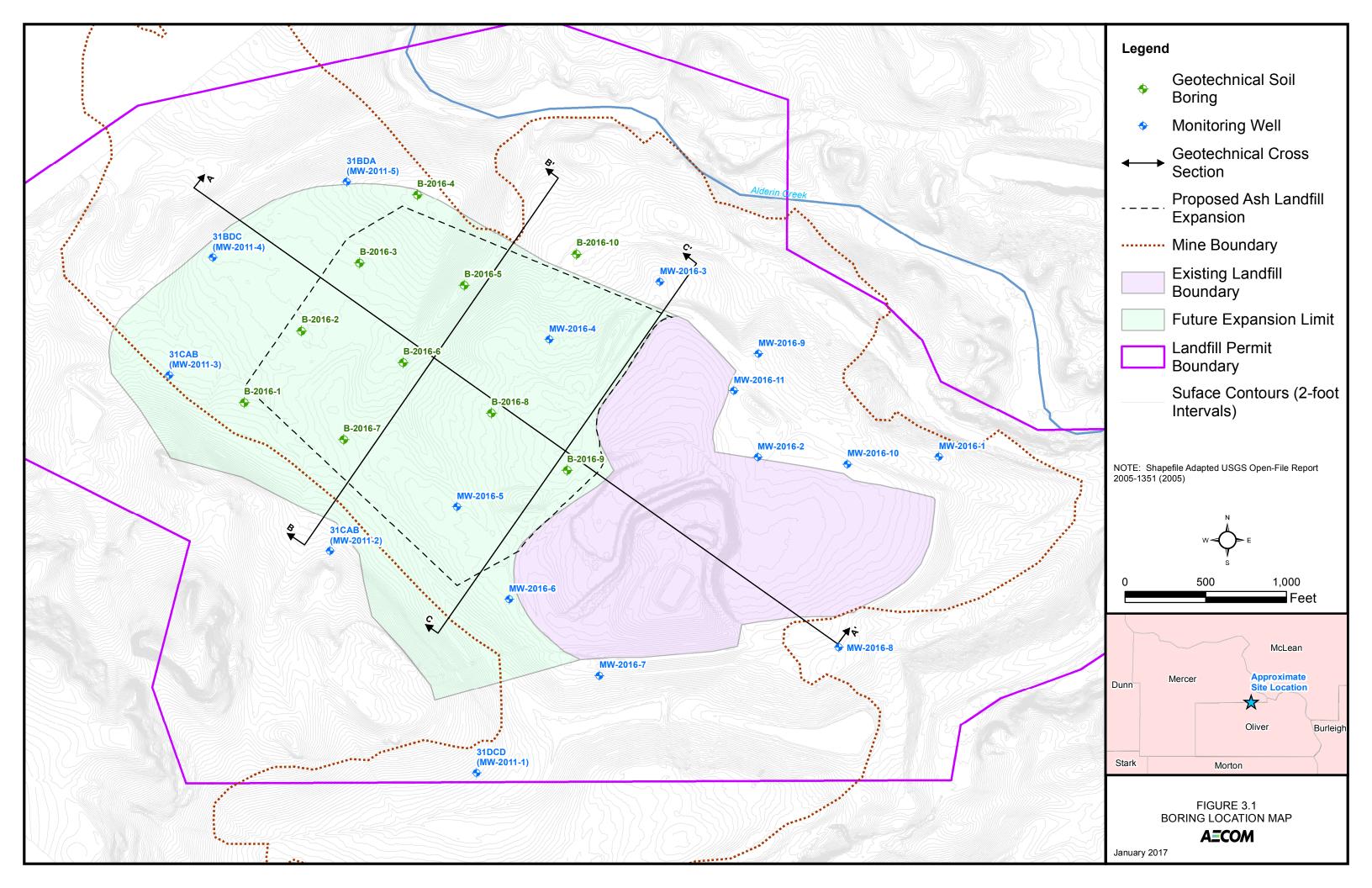


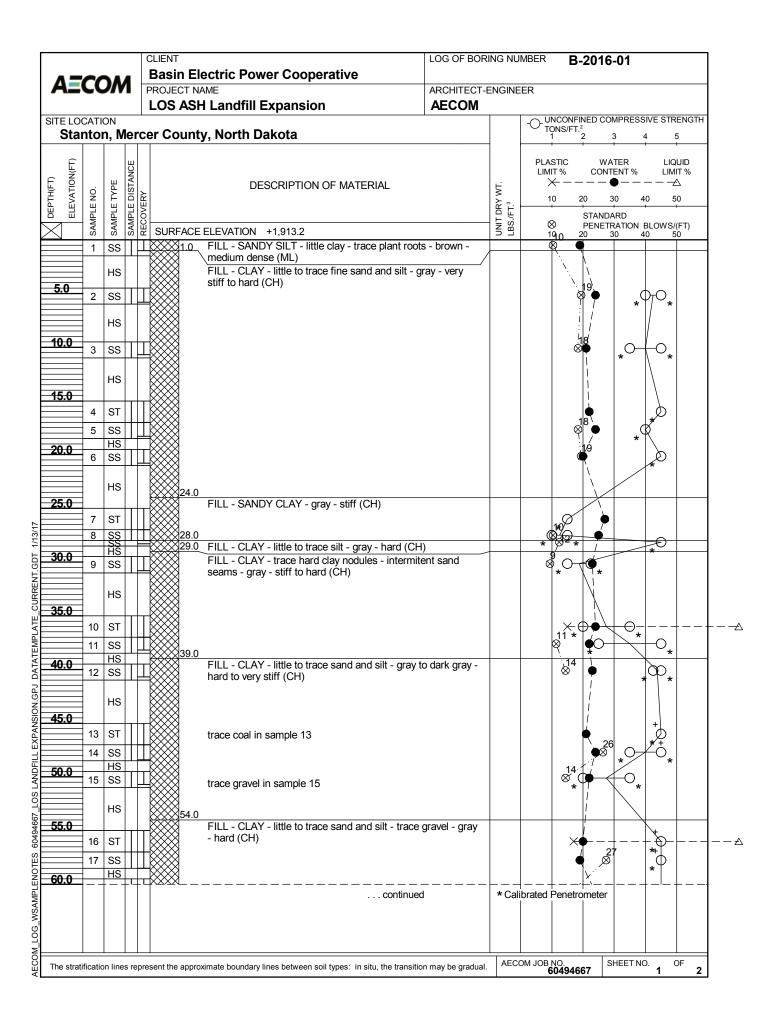
FIGURE 1



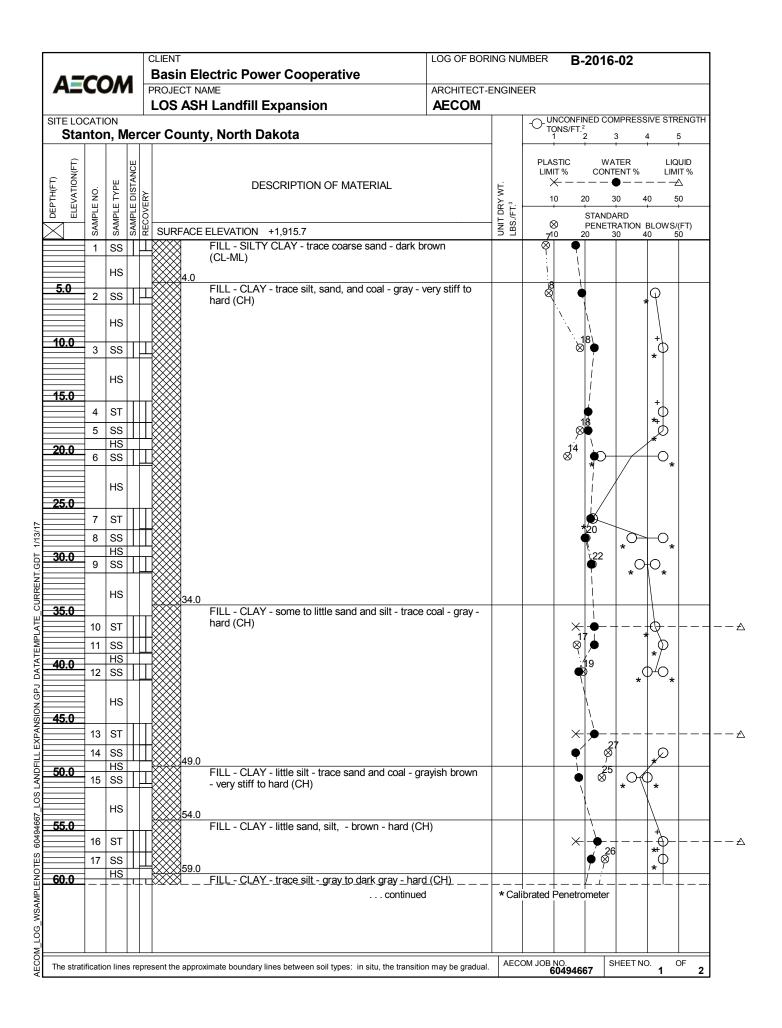
SITE MAP ASH LANDFILL EXPANSION BASIN ELECTRIC POWER COOPERATIVE LELOND OLDS STATION MERCER COUNTY, NORTH DAKOTA

Appendix B – Boring Location Map, 2016 Boring Logs/Well Diagrams





	-			1	ENT Basin Electric Power Cooperative	LOG OF E	BORI	NG NU	MBER	B-	2016	-01			
AE	C)/	1	P	ROJECT NAME OS ASH Landfill Expansion	ARCHITE AECOI		ENGINE	ER						
	CATI	ON		-		7200							SIVE STR	RENGTH	
Sta	nto	n, N	ler	ce	r County, North Dakota				О ТС 1	NS/FT.	2	3	4	5	
DEPTH(FT) ELEVATION(FT)	۰ON.	SAMPLE TYPE	SAMPLE DISTANCE	5	DESCRIPTION OF MATE	ERIAL		UNIT DRY WT. LBS./FT. ³	LIMI					IT %	
	-LE I	ц Ц	L L	Ы МЕ				DRY FT. ³	+		0 3 H		40 5 +	+	
<u> </u>	SAMPLE NO.	SAMI	SAMI	RECOVERY	SURFACE ELEVATION +1,913.2	(Continu	ed)	UNIT LBS./	8				BLOWS	(FT)	
	18	SS	Т	⊐₿	FILL - CLAY - little to trace sand an	nd silt - trace gravel - gra	ay			<u> </u>			Ĩ*Ψ		
<u>65.0</u>		нs			- hard (CH)						 		+		
	19 <u>20</u> 20A	ST SS		₿	XXX66.5 XXX67:0 、FILL - SILTY GRAVEL - light gray -	- dry - extremely dense						34	*		
	20A	ŠŠ HS	+	Ц	(GM)	, ,					ا	34 *	-0-		
70.0	21	SS	$\left \right $	┱	69.5 FILL - CLAY - little to trace silt - gra					13	É	1			
		HS			FILL - CLAY - little silt - trace fine s stiff (CH) 74.0					*	/*				
75.0	22	ST		Ŧ	SENTINEL BUTTE FORMATION - gray to gray - hard (CH)	CLAY - trace silt - bluis	h			•			+		Ø
	23	SS		\square	Šhelby tube refusal at 75.5 feet					Ţ			*		Q
<u>00 0</u>		HS											+		63
80.0 81.0	24	SS			81.0 End of Boring				ibrated F	•			<u>*</u>		63 ⊗
					Standard Penetration Test performe hammer Boring backfilled with chipped bento										
		The s	stra	tific	ation lines represent the approximate boundary	lines between soil types						-			
ORTHING	j	5779	04.	547		/25/16		OM OFF				Viscon			
ASTING		<u>1782</u>	<u>313</u>	.19	BORING COMPLETED	D 2 /25/16	ENT	ERED B	Y B	SHE	ET NO.	2 OF	2		
/L	1782313.198				tered WD / cave in @ 75' RIG/FOREMAN D-90/MF	R (Terracon)	APP'D BY BH BH 60494667			NO.					



		• •		1	LIENT Basin Electric Power Coope	erative	LOG OF E	BORII	NG NU	MBER	B	2016	-02			
A <u></u>	C)	Λ	Ρ	ROJECT NAME				NGINE	ER						
				-	-					-O-U	NCONFI DNS/FT. 1	NED CO		SIVE STR		
Sta	nto	on, n ∣		Ce	r County, North Dakota						1	2	3	4	5	
(FT)			ЦЦ								STIC IT %		ATER TENT %		UID IT %	
(FT) TION	, o	PE	STAN		DESCRIPTION	OF MATERIAL			Ч.		<		•			
DEPTH(FT) ELEVATION(FT)	N I	L L L	LED	VER					DRY \ =T. ³	1	0 :	20 : TAND	+	40 5	50	
$\overline{\mathbf{A}}$	SAMPLE NO.	SAMPLE TYPE	SAMPLE DISTANCE	RECC	SURFACE ELEVATION +1,915.7		(Continu	ed)	UNIT DRY WT. LBS./FT. ³		⊗ 0 ;			BLOWS	(FT)	
	18	SS		Ī	FILL - CLAY - trace silt -	gray to dark gray - hard		/				<u> </u>		<u> </u> *0		
		нз										Ň				
65.0					FILL - CLAY - little silt - c	lark gray to brown - ver	y stiff to							+		
	19				hard (CH)						×		- 8	+	<u>+ </u>	
	20	SS HS		Ц	trace coal in sample 19								∖ ≁(<u></u> {^∗		
70.0	21 21/	SS				black						Ø-··-	· · _ · · _	<u>, 0</u> .		
	1				71.0 LIGNITE - dark brown to SENTINEL BUTTE FOR	MATION - CLAY - little	to trace silt	t -								;
75.0		HS			bluish gray to gray - hard	(CH)										
	22	SS		\square							•			*	ļ 🖗))
		HS													/	
<u>80.0</u> 81.0	23	SS	+		81.0										54 ⊗	
01.0			++		End of Boring				* Cal	brated	Penetro	pmeter		*		
					Boring advanced to 79.5 auger											
					Standard Penetration Tes hammer	t performed with auton	natic									
					Boring backfilled with chi	oped bentonite										
		<u> </u>				hannalaur Brenn I. (-14:5:11							
ORTHING					ation lines represent the approximate	STARTED	n soll types		Situ, tł OM OFF			-	gradua Viscon			
ASTING		578			BORING	7/22/16			ERED B			EET NO.	OF			
		178	2669	9.57	2	7/22/16			ML				2	2		
VL		Not	Enc	ou	itered WD / cave in @ 41'	D-90/MR (Terracon)		APP'	D BY Bł	I	AEC		^{3 NO.} 60494	667		

					LIENT Basin Electric Power Cooperative	LOG OF BOF	king NU	JMBER B-2016-03					
4=	C)/	1	F	ROJECT NAME LOS ASH Landfill Expansion	ARCHITECT-	ENGINE						
					-	I		-O-UNCONFINED COMPRESSIVE STRENGTH TONS/FT. ² 1 2 3 4 5					
Sta	ntoi	n, Ⅳ ∣		°C€	r County, North Dakota		-						
ELEVATION(FT)	ō	ΥPE	SAMPLE DISTANCE	×	DESCRIPTION OF MATERIAL		WT.	PLASTIC WATER LIQUID LIMIT % CONTENT % LIMIT % ★●					
ELEV	SAMPLE NO.	SAMPLE TYPE	LED	OVER			LINIT DRY WT. LBS./FT. ³	10 20 30 40 50 STANDARD					
1	SAMF	SAMF	SAMF	RECO	SURFACE ELEVATION +1,918.7		UNIT LBS:/	STANDARD ⊗ PENETRATION BLOWS/(FT) 10 12 20 30 40 50					
	1	SS		Ι	FILL - SANDY SILT - trace clay and plant ro	ots - brown - dry							
		нѕ			(ML)								
5.0	2	SS			FILL - CLAY - trace sand and silt - brownish brown - very stiff (CH)	gray to dark							
	2	33			×								
		нs											
0.0	3	ST	$\left \right $										
	4	SS	\parallel		××								
5.0	4	HS			**								
	5	SS		Ц	××								
		нs											
0.0					**								
	6	ST			22.0			10 • *					
	7	SS HS		Ц	FILL - CLAY - trace to little silt - internittent s gray - soft to hard (CH)	soft clay layers -							
5.0	8	SS		Ι	trace coal in sample 8								
		нѕ			27.5								
0.0		110			FILL - CLAY - trace sand and silt - gray - ha	iu (CH)							
	9	ST			××								
	10	SS			34.0								
5.0	11	HS SS		Т	FILL - CLAY - little to trace silt and fine sand to gray - very stiff to hard (CH)	l - brownish gray							
			1										
0.0		HS			×								
0.0	12	ST		Τ	×			×					
	13	SS			×								
5.0	14	HS SS		Т	***								
					×								
		HS			××								
0.0	15	ST	$\left \right $	$\left \right $	××								
	15 16	SI	\parallel	\mathbb{H}	××								
5.0	-	HS			55.0								
2.2	17 176 178	<u> </u>	Ħ	峀	55.5 FILL - fine to coarse SILTY GRAVEL - light	gray - dense	\vdash						
		нs			(GM) FILL - CLAY - little sand and silt - seams of	lignite, sand,							
0.0					and silt - brown to gray - very stiff to hard (C	·		┤┟`_ ↓_└					
					conti	nued	* Cal	librated Penetrometer					
		n line	s re	nreg	ent the approximate boundary lines between soil types: in situ, the trai	nsition may be gradual	AEC	COM JOB NO. 60494667 SHEET NO. 0F 1 2					

			CLIENT Basin Electric Power C		LOG OF BOP	RING NU	MBER	3-2016-	03		
AECO	DM	F	PROJECT NAME	-		-ENGINE	ER				\neg
	ON							IFINED CON	IPRESSIVE :	STRENGT	ГН
		erce	er County, North Dakot	а				T. ² 2 3	MPRESSIVE	5	
_											
DEPTH(FT) ELEVATION(FT) PLE NO.							PLASTIC LIMIT %	WA ⁻ CONTE		liquid Limit %	
DEPTH(FT) ELEVATIOI PLE NO.	YPE		DESCRI	PTION OF MATERIAL		Ę	×-			- –	
	Г Ц Ц					DRY T.³	10	20 3		50	_
ELEVATI ELEVATI	SAMPLE TYPE	SAMPLE DISTANCE RECOVERY		0.7	(2 1 1	(UNIT DRY WT. LBS./FT. ³	\otimes	STANDA PENETR	RD ATION BLO\ 0 40	VS/(FT)	
		n 🗠	SURFACE ELEVATION +1,91	sand and silt - seams of	(Continued)) > =	10	20 3	0 40	50	_
18	ST		and silt - brown to	gray - very stiff to hard (C	H)			_ 21	*		
19	SS	I						•ø ∣	*		
65.0 20	HS SS	ПΤ					8		00		
									Ŭ \ ` *		
	HS							i i			
70.0									N		
21	ST						→ 1 ⊗	ç∣• −		-+-	
22	SS		trace coal in samp	le 21			8		-+),	
75.0	HS		75.0					Ĩ/`∽.	34	<u>^</u>	
23	SS	ЦĻ	75.5 LIGNITE - black	FORMATION - SANDY				1	*		
	HS		coal - grayish brow		CLAY - trace			/			
80.0				, , , , , , , , , , , , , , , , , , ,				/			
24	ST		81.5 Challey tube refu					♦			
83.5 25	SS	ΗŤ	81.5 Shelby tube refuse 83.5 SENTINEL BUTT	FORMATION - CLAY - t	race silt - bluish			6			57 ⊗
03.5			gray to gray - hard			* Cali	brated Pene	trometer	*		Ť
			End of Boring Boring advanced t	o 80.0 feet with 3.25-inch	hollow-stem						
			auger	5 60.0 Teel with 5.25-inch	nonow-stern						
			Standard Penetrat hammer	ion Test performed with a	utomatic						
				ith chipped bentonite							
		ratifi	pation lines concept the approx	vimate houndary lines hat	Neen soil tursos:	in eitu #		maybar			4
ORTHING	i ne st	Iauti	cation lines represent the appro	ORING STARTED		ECOM OFF	105				=
ASTING	57876	8.18	1	ORING COMPLETED				HEET NO.	/isconsin OF		\neg
	17830	29.4	7	7/22/16		MERED B	B		2 2 NO. 50494667		
VL				IG/FOREMAN		P'D BY					

			LIENT	LOG OF BOR	Ring Nu	MBER	B-20	16-04		
AECC	M	-	Basin Electric Power Cooperative ROJECT NAME	ARCHITECT-		ED				
			LOS ASH Landfill Expansion	AECOM						
SITE LOCATIO				ALCOM			CONFINED	COMPRES	SIVE STR	ENGTH
		rce	r County, North Dakota				NS/FT. ² 2	COMPRESS 3	4	5
DEPTH(FT) ELEVATION(FT) SAMPLE NO.	SAMPLE TYPE SAMPLE DISTANCE	RECOVERY	DESCRIPTION OF MATERIAL		UNIT DRY WT. LBS./FT. ³	PLAS LIMIT X 10	% C 		LIM — — —	UID IT %
	AMP	ECO	SURFACE ELEVATION +1,943.7		INIT D	⊗	PEN	NDARD	BLOWS/	(FT)
<u>م</u>	SS 0		FILL - SILTY CLAY - trace gravel and plant ro	ots - dark		10 8	<u>0 20</u>	30 4	40 5	0
· ·			xxx2.0 brown (CL-ML)							
	HS SS		FILL - CLAY - little to trace silt - trace fine san brownish gray - very stiff (CH)	d - gray to			12			
10.0	HS SS						*			
15.0	HS							\sum		
4	SS	1					₽ 	*1		
20.0	HS					4	0			
	SS		trace coal in sample 5				• **	*		
25.0 6	SS		trace coal in sample 6			×	9			
20.0	нs		FILL - CLAY - trace silt and fine sand - gray -	hard (CH)			12			
30.0 7	SS								*	
35.0 8	SS							23	*	
40.0	нѕ							`. `. `.	+	
40.0 9 9A	SS SS		40.5 41.5 FILL - LIGNITE and SHALE fragments					● ⊗¯·· _ ·	<u> </u>	
45.0 40	нѕ		SENTINEL BUTTE FORMATION - CLAY - litt gray - hard (CH)	le to trace silt -					39+ 8	
10	SS						*	,%	*	
50.0	HS									
50.0 11	SS		coal seam in sample 11						*	
	нs									
55.0 12	SS						¢		. 40 ⊗ () *	
	нs									
			continu		*Cal	— — + brated P	⊥⊥ _ enetrome		¥!	
The stratification	n lines r	repre	sent the approximate boundary lines between soil types: in situ, the trans	ition may be gradual.	AEC	OM JOB N 60	0. 494667	SHEET N	^{O.} 1	DF 2

				CLIENT Basin Electric Power Coope		BORING I	RING NUMBER B-2016-04						
A E	C)/	1	PROJECT NAME	ARCHITI	ECT-ENGI	NEER						
	<u></u>			LOS ASH Landfill Expansion	AECO	M							
ITE LOO			ler	er County, North Dakota			L-0-1	TONS/FT. ²	ED COM 3		5		
(F			щ					ASTIC	WAT		LIQUID		
DEPTH(FT) ELEVATION(FT)		Ц Ц	SAMPLE DISTANCE	DESCRIPTION		₊ :	LIN	ИТ % ——-			LIMIT %		
DEPTH(FT) ELEVATION	SAMPLE NO.	SAMPLE TYPE	E DIS			UNIT DRY WT.	LBS./FT.	10 20	30) 40	50		
	AMPL	AMPL	AMPL	SURFACE ELEVATION +1,943.7	+1.943.7 (Continued)						N BLOWS/(FT)		
\sim	ൾ 13	ൾ SS	ŝ		(Contin IATION - CLAY - little to trace s	,	5	10 20	30) 40 8	9 1 50		
		нs		gray - hard (CH) 63.0									
65.0	14	SS		LIGNITE									
	14	33											
		HS											
70.0	15	SS SS		70.0 SENTINEL BUTTE FORM	IATION - CLAY - trace silt and f	ine					+		
		нs		sand - gray - hard (CH)					/		*	1.1.1	
75.0	<u> </u>								j		+ 47	. · · ·	
	16	SS							?		*		
		нs		78.0	IATION - SILTY CLAY - little fin	e	_		<u> </u>		.		
80.0 81.0	17	SS		sand - gray - hard (CL-ML 81.0		-				33 ⊗	* 0		
				End of Boring Boring advanced to 79.5 f	eet with 3.25-inch hollow-stem	*(Calibrated	Penetron			*		
				auger	performed with automatic								
				hammer									
				Boring backfilled with chip	ped bentonite								
		The	stra	fication lines represent the approximate	ooundary lines between soil type	es: in situ	, the trar	sition ma	ay be gi	radual.			
ORTHING	3	5791	89.4	83 BORING S	TARTED 7/21/16	AECOM	OFFICE	Oshk	osh, W	liscons	in		
579189.483 ASTING		BORING C	OMPLETED 7/21/16	ENTERED	ENTERED BY SHEET NO. OF MLB 2 2								
1783387.04				04	//21/10	MLB 2 2 APP'D BY AECOM JOB NO. BH 60494667							

				CLIE Ba		ectric Power Cooperative	LOG OF BOR	ring NU	MBER	B-2016	-05			
AEC	0	M		PRC	JECT N/		ARCHITECT-							
TE LOCA						-				ONFINED CO	MPRESSIV	E STRENGTH		
Stant	on _:	, IVIC	erc	er v	Count	y, North Dakota		_	1	2	3 4	5		
4(FT)			NCH NCH						PLASTIC LIMIT %		TER ENT %	LIQUID LIMIT %		
DEPTH(FT) ELEVATION(FT) PI F NO	<u>,</u>	ΥPE	SAMPLE DISTANCE RECOVERY			DESCRIPTION OF MATERIAL		WT.	×	(
		SAMPLE TYPE						L UNIT DRY WT. LBS./FT. ³	10	20 3 STANDA	80 40 +	50		
		SAM	SAM	SL	JRFACE	ELEVATION +1,891.1		UNIT LBS.	⊗ 5 ¹⁰		RATION BL	OWS/(FT) 50		
1	1 5	ss	μ	₿	\bigotimes	FILL - CLAY - little to trace silt - trace plant rou gray - very stiff (CH)	ots - brownish		Ǿ	*R				
	H	IS		\bigotimes	<u>₩3.0</u>	FILL - CLAY - little to trace silt - trace coal - gi	ay - hard (CH)		<u>`</u>					
5.0 2	2 8	SS	TP	Ѭ	\otimes				Ø	•	*			
		IS		\otimes	\otimes									
10.0 3		SS	+	\bigotimes	<u>9.5</u>	FILL - CLAY - little to trace silt and coal - gray	ish brown to							
		55		₩	\bigotimes	brown - soft to medium (CH)		,	171					
45.0	ł	IS		\bigotimes	\bigotimes									
15.0	1 9	ST	Ш	₩	\bigotimes					×+	┣━− -			
5	5 5	ss		×					TVA					
20.0		HS SS		×	× 19.0	FILL - CLAY - little silt - trace coal and clinker	- grayish		*	X	- -			
				×	23.0	brown - very stiff (CH)				*	*			
25.0	ŀ	IS			$\bigotimes^{23.0}$	FILL - CLAY - little sand and silt - trace coal -	gray - very stiff			i				
23.0	7 5	ST	П	₿	\bigotimes	to hard (CH)				Å		*		
	3 5	ss	╎╢	\mathbb{X}	29.0					€ ²⁰		-Õ		
30.0		HS SS	Π	×	××29.0	FILL - CLAY - little to trace silt, sand, coal, and				× 0-				
				×	33.0	grayish brown to brown - very stiff to hard (CH)					*		
35.0	ŀ	IS		×	× <u>55.0</u>	FILL - CLAY - little sand and silt - trace coal -	gray - very stiff							
	0 8	ST	Ш	₿	\otimes	to hard (CH)				×	+.			
1		SS	Ш	\otimes	39.0					25	▶+	-0,		
40.0		HS SS	$^{++}$	-		FILL - CLAY - little to trace silt and coal - dark stiff (CH)	gray - very							
					\otimes	coal seam from 40.1 to 40.3 feet				*	*			
45.0		IS			<u> </u>							16		
14		ST SS SS	Ħ		45.5	LIGNITE SENTINEL BUTTE FORMATION - CLAY - litt	le to trace silt -			•	32 ⊗···−,	+ 46		
	ł	HS				bluish gray to gray - hard (CH)								
50.0	5 5	ss	$^{++}$							↓	i33 ⊗	+		
		нs									``\ *	*		
55.0			╷│.							i		+ 46		
1	6 5	SS	Щ							ו				
	ŀ	IS												
60.0	- + -	-+	t t		//						+	_ !+		
						continu	eu	* Cal	ibrated Per					
								<u> </u>						
The stratifica	ation	lines	repr	esent	the approx	ximate boundary lines between soil types: in situ, the trans	tion may be gradual.	. AEC	OM JOB NO. 604	94667 ^S	HEET NO.	1 OF 2		

			_		LIENT Rasin Flo	etric Powe	r Cooperative	LOG OF	BORING	g NU	MBER	B-2	016-0	05			
A E	C)/	1	PF	ROJECT NA	ME	-	ARCHITE		GINE	ER						
SITE LO	CATI			L	.OS ASH	Landfill Ex	pansion	AECO	M			CONFINE		PRESS	VE STR	ENGTH	
			ler	се	r County	, North Dak	ota				-O-UN TO 1	NS/FT. ² 2	3	4	5		
(L			ш								PLAS	, TIC	WATI	ER	LIQ	UID	
DEPTH(FT) ELEVATION(FT)		ш	SAMPLE DISTANCE								LIMIT	-%				Т%	
DEPTH(FT) ELEVATION	Ň	SAMPLE TYPE	DIST	Σ		DESC	RIPTION OF MATERIAL		TW Y	UNIT URT WI.	10		30	4			
	SAMPLE NO.	MPLE	MPLE	RECOVERY					T DR	NU I	+		ANDAF		······································		
\triangleleft			SAI	Ш Ш Ш		ELEVATION +1		(Continu		LBS	8 10	20	NETRA 30	ATION E	3LOWS/(FT) D	
	17	SS				SENTINEL BU bluish gray to g	TTE FORMATION - CLAY - ray - hard (CH)	little to trace sil	lt -			T			*		
		нs				0,0	, , ,								/ :		
<u>65.0</u>	18	SS	$\left \right $	T											****		
					67.0										* ~ .	<u>`.</u>	
		HS				LIGNITE										`	· _ 1
70.0	19	ss	╞╍╞	퍼	X												`&
		нs			72.0	SENTINEL BUT	TTE FORMATION - CLAY -	dark orav - han	d								
75.0						(CH)		aan gruy - nar	-						+		7
75.0	20	SS	Щ									ę			* •		7 ⊗
		HS			78.0												
80.0							TTE FORMATION - fine CLA gray - dense (SC)	YEY SAND -				Į,		35. ⊗			
<u>80.0</u> 81.0	21	SS		Lł.	////81.0	End of Boring	g.u) usiloo (00)			* Cali	bratod E	enetrom) otor	\otimes			
						Boring advance	d to 79.5 feet with 3.25-inch	hollow-stem		" Call			elei				
						auger Standard Penet	ration Test performed with a	utomatic									
						hammer	d with chipped bentonite										
						Doning backhile	d with chipped bentonite										
ORTHING		The	stra	tific	ation lines r	epresent the ap	Proximate boundary lines be	ween soil type	S: in si								
		5786	31.4	494			7/27/16					Oshko			in		
ASTING		1783	677	.34	3		BORING COMPLETED 7/27/16		ENTER	RED B'		SHEET	2		2		
														NO. 04946			

	-			1	LIENT Basin B	Electric Power Cooperative	LOG OF BOR	RING NU	IMBER	B	2016	-06		
4=0			1	Ρ	ROJECT		ARCHITECT-	ENGINE						
re loc Stan			ler	се	r Cour	nty, North Dakota				NCONFI DNS/FT.	NED CO	MPRES	SIVE STR	ENGTH 5
ION(FT)	SAMPLE NO.	SAMPLE TYPE	STANCE		<u> </u>	DESCRIPTION OF MATERIAL		L LINIT DRY WT. LBS./FT. ³	PLA LIMI	STIC T % ← — —	W/ CONT 	+ TER TENT % ● — — 30 4	LIC LIM	UID IT %
	AMPI	AMPI	AMPI	RECOVERY		CE ELEVATION +1,909.8		INIT D	¢			RATION	BLOWS	
	თ 1	ഗ SS	s S			FILL - SILTY CLAY - trace sand, coal, an	d plant roots -		1	0 <u>14</u> 2 Ø	20 :	<u>30 4</u>	40 <u>5</u>	0
		HS			<u> </u>	brown - hard to very stiff (CL-ML)							*	
5.0	2	SS		Ц		FILL - CLAY - little to trace silt, sand, and gray to gray - medium to very stiff (CH)	l coal - brownish		×	;	Ó			
		нs												
).0	3	SS	Τ	I										
5.0		НS												
5.0	4	ST		T						do.	,			
	5	SS		Ī						þ.*				
0.0	6	HS SS							7	\mathbf{n}^{\star}	_			
_	0	55		╧		hard 4-inch clay seem in sample 6			*	۲*				
i.0		HS												
	7	ST		\Box						,do	•			
_	8	SS		I		trace clinker in samples 8 and 9					\			
).0	9	HS SS		Т										
_									*	*				
5.0		HS		k										
	10	ST	Τ	T		hard clay seam in sample 10				¢≁-	 ∳ −	<u></u>	-	
\equiv	11	SS		Ī					*	×12	•			
.0	12	HS SS		Т						i				
									*	۲×				
5.0		HS		k k										
	13	ST		T							 ↓	<u> </u>	L	
	14	SS				hard clay seam in sample 14				Ð	ė.			
.0	15	HS SS	\square	\exists		· · · · ·				:13 *	$\downarrow \dot{\diamond}$			
\equiv	.5	00							*		/*			
		HS		k							<i>.</i> /			
5.0	16	ST	$\left \right $	T						×	Ќ		ļ	L
	10			╫	57	FILL - CLAY - little to trace silt, sand, and	l coal - brown - very			*		5		
0.0		HS				stiff (CH)	,				₩~	*		
				T			ntinued	* Cal	librated	Penetro	meter			
				1				1	1		I	1	1	I

				С	LIENT		LOG OF B	BORI	NG NU	MBER	B-201	6-06		
A =					Basin Electric Power	Cooperative								
A	C	JN	1		ROJECT NAME		ARCHITE		NGINE	ER				
				l	OS ASH Landfill Ex	pansion	AECON	M						
SITE LO					" County North Dal	-1-					CONFINED C NS/FT. ² 2			
518	nto	n, IV	ier	Ce	r County, North Dak	ota				1	2	3	4	5
Ê			ш							PLAS1	TIC W	ATER	LIQ	UID
DEPTH(FT) ELEVATION(FT)			ANC							LIMIT		ITENT %		IT %
DEPTH(FT) ELEVATION	ġ	μΥΡΕ	DIST	≿	DESC	RIPTION OF MATERIAL			T	へ 10		30		50
ILEV	Ē	Ē	Ē	N N N					DRY =1. ³		STAN		+ 3	+
	SAMPLE NO.	SAMPLE TYPE	SAMPLE DISTANCE			000.0	(Cantinu	a d)	UNIT DRY WT. LBS./FT. ³	\otimes	PENE	TRATION		
\square	ω 18	SS S	s S		SURFACE ELEVATION +1	,909.0 ttle to trace silt, sand, and coal -	(Continue	,		10	2021	$\frac{30}{0}$	40 5	i0
					Stiff (CH)			, y				* *		
	1	HS		k	hard clay seam	in sample 18								
65.0	10	0.7		Ţ	65.5									
	19 20 20A	25	H	Ŧ		se sand to fine gravel sized grain	IS	7					+	55 ⊗
						TE FORMATION - CLAY - trace	e silt - bluisł	h				γT	*	,.
70.0		HS			gray to gray - ha	ard (CH)							+44	Í
70.0	21	SS									Ý		*	
	1										/			
	1	HS									ľ			N.
75.0	22	SS	Т	Т							4			⊗
											Y		*	:
	1	HS									ĺ.			:
80.0 81.0											1		+	51 ⊗
81.0	23	SS	μ		81.0 End of Boring				* Cali	brotod Dr			*	×
					Boring advance	d to 79.5 feet with 3.25-inch holl	ow-stem		^ Call		enetromete			
					auger									
					Standard Penet hammer	ration Test performed with auton	natic							
						d with chipped bentonite								
					-									
1														
		The s	stra	tific	ation lines represent the an	proximate boundary lines betwee	n soil types	s: in	situ. th	le transit	ion mav be	gradua	I.	I
NORTHIN	G					BORING STARTED			OM OFF		Oshkosh,			
EASTING		5781	51.	055	5	7/26/16 BORING COMPLETED		ENTE	ERED B	Y	SHEET NO	. Of	-	
		1783	299	9.15	58	7/26/16			MLI	3		2	2	
WL		65.0	w	5/6	cave in @ 54'	RIG/FOREMAN D-90/MR (Terracon)		APP'	о вү ВН		AECOM JO	0B NO. 60494	667	

AECOM_LOG_WSAMPLENOTES 60494667_LOS LANDFILL EXPANSION.GPJ DATATEMPLATE_CURRENT.GDT 1/13/17

					LIENT Basin Electric Power Cooperative	LOG OF BOF	KING NU	IMBER B-2016-07
A <u></u>	C)N		PF	ROJECT NAME OS ASH Landfill Expansion	ARCHITECT-	-ENGINE	
			lo		r County, North Dakota	I		UNCONFINED COMPRESSIVE STRENGTH
518	nto	n, IV			County, North Dakota		-	
UEP IN(F I) ELEVATION(FT)	E NO.	SAMPLE TYPE	SAMPLE DISTANCE	ERY	DESCRIPTION OF MATERIAL		L UNIT DRY WT. LBS./FT. ³	PLASTIC WATER LIQUID LIMIT % CONTENT % LIMIT % ★ - - ● 10 20 30 40 50
	SAMPLE NO.	WPLE	MPLE	RECOVERY			UT DF S./FT	STANDARD Ø PENETRATION BLOWS/(FT)
\leq	ທີ 1	් SS	ŝ	₽ T ×	SURFACE ELEVATION +1,924.8 FILL - SILTY CLAY - trace sand and plant r	oots - dark brown	8	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
		HS			- dry to moist - hard (CL-ML)			
5.0	2	SS	Τ	Į	FILL - CLAY - little to trace silt, sand, and co gray - stiff to hard (CH)	oal - dark gray to		
10.0	3	HS SS		TX				
		HS						
15.0	4	ST		Į	trace hard clay nodules in sample 4			
20.0	5	SS HS		Ľ	×			
20.0	6	SS		Ц.	trace hard clay nodules in sample 6			
25.0		нs		XXXX	FILL - CLAY - some sand and silt - gray to o stiff to stiff (CH)	dark gray - very		
20.0	7	ST SS		Į				
30.0	9	HS SS						
		нѕ						
35.0	10	ST		Į				
40.0	11	SS HS			39.0 FILL - CLAY - little to trace silt, sand, and c	oal - brownish		
-0.0	12	SS HS		LX XX	gray to gray - very stiff to hard (CH)			
45.0	13	ST						× +
	14	SS		ЦĮ	×			
50.0	15	HS SS		Į				
55.0		нs			54.0 FILL - CLAYEY to SANDY SILT - little to tra	ace coal - dark		
	16	ST			brown to brown - hard (CL-ML)			
60.0	17	SS HS			59.0			
3010	1			Ť	···· conti		* Cali	+
					ent the approximate boundary lines between soil types: in situ, the tra			OM JOB NO. 60494667 SHEET NO. 1 OF 1 2

	-			CLIENT Basir	n Electric Power	Cooperative	LOG OF E	BORING N	UMBER	B-2016-0	07	
AE	CC)//	1	PROJEC		-	ARCHITE					
									-O-UNCO TONS/		PRESSIVE	STRENGTH
Star	ntoi	1, N	ler	cer Co	unty, North Dak	ota			1	2 3	4	5
DEPTH(FT) ELEVATION(FT)	ö	/PE	SAMPLE DISTANCE		DESC	RIPTION OF MATERIAL		۸T.	PLASTIC LIMIT %			LIQUID LIMIT %
DEPTH(FT) ELEVATION	LEN	ΓE						DRY	: 10	20 30	· ·	50
	SAMPLE NO.	SAMPLE TYPE	SAMF		ACE ELEVATION +1	924 8	(Continu	(pe) UNIT DRY WT.	⊗ 10	STANDAF PENETRA 162030	TION BLOV	VS/(FT) 50
	18	SS	Ţ.		FILL - CLAY - li	ttle to trace silt - trace coa					*	30
65.0		HS		г	gray - very stiff f	to stiff (CH)						
	19	ST										-+
	20	SS HS		L								
70.0	21	SS HS										
75.0				-888								
	22 23	ST			76.5 SENTINEL BUT	TE FORMATION - CLAY	- little to trace silt	·_		•	+	54
	23	SS HS			bluish gray - ha					!	*	
80.0 81.0	24	SS			81.0					•	+	51 ⊗
					End of Boring	d to 79.5 feet with 3.25-in	ch hollow stom	* Ca	alibrated Pen	etrometer	*	
					auger							
					Standard Penet	ration Test performed with	n automatic					
					Boring backfilled	d with chipped bentonite						
		The s	strat	ification I	ines represent the app	proximate boundary lines	petween soil types	: in situ,	the transition	n may be gr	adual.	
ORTHING	;					BORING STARTED		AECOM O		shkosh, Wi		
EASTING		5776	74.8	41		7/25/16 BORING COMPLETED		ENTERED		SHEET NO.	OF	
		1782	930	.337		7/25/16		М	LB	AECOM JOB N	2 2	
NL						RIG/FOREMAN		APP'D BY				

4=	CC)/	1		Basii PROJE		ectric Power Cooperative	ARCHITECT-	ENGINE	ER		-2016			
							Landfill Expansion	AECOM							
ITE LOO Star			lei	ce	er Co	untv	y, North Dakota			-O-U	NCONF DNS/FT. 1	INED CC 2 2	MPRESS	SIVE STRI 4 5	
							•				, STIC	1	ATER	LIQ	
DEPTH(FT) ELEVATION(FT)		ш	SAMPLE DISTANCE				DESCRIPTION OF MATERIAL			LIM			TENT %		Т %
UEP I H(F I) ELEVATION	NO.	TYP.	E DIST	ERY			DESCRIPTION OF MATERIAL		۲۷ WT °°			20	30 4	10 50	
	SAMPLE NO.	SAMPLE TYPE	MPLE	RECOVERY					UNIT DRY WT. LBS./FT. ³	ć	, 3	STAND		BLOWS/(FT)
\leq	න් 1	ೆ SS	\$	ž	SURF	ACE	ELEVATION +1,944.6 FILL - SILTY CLAY - trace sand, coal, and pla	nt roots - dark	5 8		0 <u>13</u>			10 50	
	1					2.0	brown (CL-ML) FILL - CLAY - little to trace silt and coal - gray				<u>, ``</u>				
5.0		HS					FILL - CLAY - little to trace slit and coal - gray brown - very stiff to hard (CH)	511 DI UWI (O			: 9	\`_			
	2	SS	μ	H								ļ	₩		
		HS					collected bulk sample of auger cuttings from 2	0 to 9 5 feet				//	(
10.0	3	SS	\mathbf{T}				concored bank compre or auger cuttings 110112			×		6			
				F							*	*			
15.0		HS									9				
13.0	4	SS	ļΓ	Щ			collected bulk sample of auger cuttings from 9	.5 to 19.5 feet		Ŕ	þ				
		HS											\mathbf{N}		
20.0	5	SS	$\left \right $	\mathbb{H}							11 ⊗	Ļ	$ \rangle$	+0	
	0	55		H									*	\ *	
05.0		HS				24.0									
25.0	6	ST	\parallel				FILL - CLAYEY SILT to SILTY CLAY - trace fi - medium to stiff (CL-ML)	ne sand - gray				i		+	
	7	SS	╢	$\left \right $							⊗ ¹²	bo	-	*	
30.0	8	HS SS		Ħ						TV	12	*	`		
	Ø	33	₽	Ħ						*	×.	Ţ			
		HS				33.0	FILL - CLAY - little to trace silt - gray - hard to	very stiff (CH)				$\left \right\rangle$	\leftarrow		
35.0	9	ST	$\left \right $	$\left \right $				- 、 /					$\left \right\rangle$		
		SS	\parallel								4 ¹³			[Ī
40.0		HS		Ħ							13 ⊗	* 7 *	\searrow		
	11	SS	μ	H								Ĭ	*		
		HS													
45.0	40	<u></u>	$\left \right $									l			
	12 13	ST SS	\parallel										× *		
50.0		HS		H		49.0	FILL - CLAY - some sand and silt - trace coal	- intermittent			*		¥*		
	14	SS	\prod	H			sand and silt seams - brown - very stiff to hard					Ţ	+		
		НS										il I			
55.0			$\left \right $	$\left \right $										×_	
	15	ST		Щ									-	*	⊿
60.0	16	SS HS		Щ		59.0					ļ/			*	
<u>60.0</u>				F	KXXXX			 ed	× Cali	 brated	⊢∠ Penetr	↓ ometer	-	++	

	-		_		LIENT Basin Fl	ectric Power	Cooperativo	LOG OF E	BORING NU	JMBER	B-2016	-08		
AE	C)/	1	Ρ	ROJECT N		-	ARCHITE		EER				
ITE LO	- A T I				-03 A3r		ansion	AECO			NFINED CC	MPRESS		ENGT
			ler	ce	r Count	y, North Dak	ota			TONS	/FT. ² 2	3 4		
ELEVATION(FT)	SAMPLE NO.	SAMPLE TYPE	SAMPLE DISTANCE	ERY		DESCI	RIPTION OF MATERIAL		Q UNIT DRY WT. LBS./FT. ³	PLASTIC LIMIT % X	CON ⁻	ATER TENT % •	LIQ LIMI — — — — 2 0 5	Т% \
	IPLE	ЪГЕ	IPLE	RECOVERY					() UNIT DRY LBS./FT. ³		STAND	ARD		
\langle	SAN	SAN	SAN	잂	SURFACE	ELEVATION +1,	944.6	(Continu		⊗ 10	PENET 20 22	RATION E	BLOWS/	(FT) 0
	17	SS		I	XXX	FILL - CLAY and	d SILT - little to trace sar	nd - brownish gray	-		হ্ৰ 🖉			-
65.0		HS			65.5	stiff (CL-ML)								
	18	ST		T		FILL - CLAY - lif	tle to trace silt - gray - ha	ard (CH)			•		÷O	
	19	SS		॑╢				x - 7			N.	34 ⊗	*	
=0.4	13	HS	+	┶	69.0		(01)0						*	
70.0	20	SS	Ш	Ţ	70.5	FILL - fine SILT	Y SAND - trace clay - lig	ht brown - medium			20.··			
	20A	- 33	┝┸┦		XXXX `		CLAY - some silt - trace of	coal - brown - hard	-/	₹		*	~°*	
7 5.0		HS				(CH)				, ,			+	
	21	ST		Ц							●	32	*	
	22	SS		Ц	79.0						Þ	32 8	_⊕	
80.0	00	HS		┱		FILL - fine CLA	YEY SAND - intermitent	hard clay layers -				30 Ø		
81.0	23	SS		4	XXX 81.0	gray - dense (SO End of Boring	C)			librated Pen	-			
DRTHING	6	5778	39.	047	,	represent the app	roximate boundary lines BORING STARTED 7/27/10 BORING COMPLETED 7/27/10	6	: in situ, t AECOM OF ENTERED B ML	FICE C	n may be Dshkosh, N SHEET NO.	•		
		1783	ō45	.50	13		RIG/FOREMAN		APP'D BY		AECOM JOI		2	
L							RIG/EUREMAN		A PP'I BY		AECOM JOI	SIN()		

AEC	.0	M		Basin Electric Power CooperativeROJECT NAMEARCHITECTOS ASH Landfill ExpansionAECOM	-ENGINE	ER	
ITE LOC	ATIO	N					COMPRESSIVE STRENGTH
			erc	r County, North Dakota		TONS/FT. ² 1 2	3 4 5
DEP I H(F I) ELEVATION(FT)	ö	/PE	DECOVEDV	DESCRIPTION OF MATERIAL	NT.		NATER LIQUID NTENT % LIMIT % - ● — — — — — — — — — — — — — —
DEPTH(FT) ELEVATIOI	SAMPLE NO.	SAMPLE TYPE			 UNIT DRY WT. LBS./FT. ³	10 20	30 40 50 H H H
	SAMF	SAMF		SURFACE ELEVATION +1,955.4	 UNIT DRY LBS./FT.³		TRATION BLOWS/(FT) 30 40 50
	1	SS	μ	FILL - SILTY CLAY - trace sand, coal, and plant roots - dark brown - hard (CL-ML)		8 9	
5.0		нs		FILL - CLAY - little sand and silt - trace coal - grayish brown - stiff to very stiff (CH)		8	
	2	SS	Ц	collected bulk sample of auger cuttings from 1.5 to 9.5 feet			▶
		нs					
10.0	3	ss	ф	FILL - fine CLAYEY SAND - little silt - gray - moist - loose (SC)			<u>ອ</u>
		нs		XX 13.0			
15.0	4	ss	\mathbf{h}	FILL - CLAY - little to trace silt and coal - trace hard clay nodules - gray - stiff (CH)		50	
				collected bulk sample of auger cuttings from 9.5 to 20.0 feet			
20.0		HS		FILL - SANDY CLAY - trace clay - gray - moist (CH)			
	5	ST	\square	22.0			-+
	6	ss	Ħ	FILL - CLAY - little to trace silt and sand - gray - very stiff			
<u>25.0</u>		HS SS	\square	FILL - fine CLAYEY SAND - little silt - gray - moist - medium			0.
			ſ	dense (SC)			*
30.0		HS		FILL - CLAY - trace silt and coal - gray - hard (CH)			
	8	ST		×		10	*
		SS HS	P	34.0			- ●
35.0		SS	þ	FILL - SANDY CLAY - little silt - trace coal - gray - hard (CH)		8 • É	*
		нв		38.0			
40.0			\parallel	FILL - CLAY - little to trace silt - dark gray to gray - hard to very stiff (CH)			
		ST	Щ				25 *
		SS HS	Щ			2 ²	
45.0		SS	Р				*
		нs					
50.0	_		$\left \right $				
		ST		×		, ¹⁴	
55.0		SS HS				× 13 ⊗	
55.0	16	SS	벁				*
		нs		×			
60.0			+	××L		<u> </u> ++	_
				continued	*Cali	ibrated Penetromete	

			CLIENT		LOG OF B	BORING NU	MBER E	8-2016-09	
AECC			Basin Electric Pow	er Cooperative					
		•	PROJECT NAME LOS ASH Landfill E	vnansion		CT-ENGINEI	ER		
SITE LOCATIO)N			хранзіон	ALCON			FINED COMPRE	SSIVE STRENGTH
		erc	er County, North Da	akota			TONS/F	T. ² 2 3	4 5
DEPTH(FT) ELEVATION(FT) PLE NO.	YPE	SAMPLE DISTANCE	DES	SCRIPTION OF MATERIAL		WT.	PLASTIC LIMIT %	WATER CONTENT %	<u>A</u>
DEPTH(FT) ELEVATION SAMPLE NO.	SAMPLE TYPE					() UNIT DRY WT. LBS./FT. ³	10	20 30 STANDARD	40 50
SAM S	SAM	SAM	SURFACE ELEVATION	+1,955.4	(Continue	ed)	⊗ 10		N BLOWS/(FT) 40 50
17	ST		FILL - CLAY very stiff (CH	 little to trace silt - dark gray to gra 	ay - hard to				
	SS HS	1		,			10		
	SS	Ţ					⊗ ^{13_}	~ *	
70.0	нs								
	ST								*
	SS HS	Ц	73.5 FILL - SILTY	CLAY - gray - hard (CL-ML)				25	
	SS	Ţ						● ※	*
80.0	HS								
	ST	Τ	FILL - CLAY	- little to trace silt, sand, and coal -	brownish			★ 30	*
83.5 24	SS		83.5 gray to gray - End of Boring	hard (CH)			orated Penet		
			auger Standard Per hammer	ced to 80.0 feet with 3.25-inch holl netration Test performed with autor lled with chipped bentonite					
<u> </u>	ĥe s	trat	ication lines represent the a	approximate boundary lines betwee	en soil types	in situ, th	e transition	may be gradu	ıal.
ORTHING	57748			BORING STARTED 7/28/16		AECOM OFFI	05	hkosh, Wisco	
ASTING	784			BORING COMPLETED 7/28/16		ENTERED BY	SH	HEET NO. 2	OF 2
/L	_			RIG/FOREMAN		APP'D BY		ECOM JOB NO.	

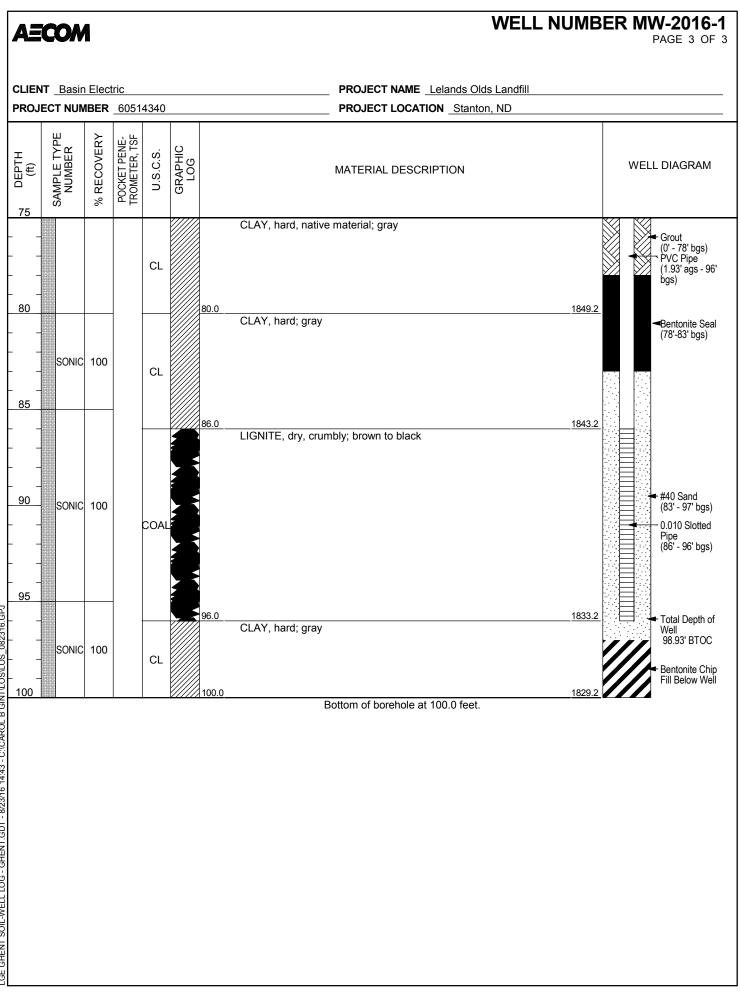
Stanton, Me		ROJECT NAME LOS ASH Landfill Expansion	ARCHITECT-I	ENGINE	ER
LEVATION(FT) ELEVATION(FT) C SAMPLE NO. S SAMPLE TYPE SAMPLE TYPE	erc		AECON		
LEVATION(FT) ELEVATION(FT) C SAMPLE NO. S SAMPLE TYPE SAMPLE TYPE		r County, North Dakota			-O-UNCONFINED COMPRESSIVE STRENGTH TONS/FT. ² 1 2 3 4 5
A Wess		r County, North Dakota			
A Mes Saw					PLASTIC WATER LIQUID LIMIT % CONTENT % LIMIT %
A Mes Saw		DESCRIPTION OF MATERIAL		.ΤW	×
A Mes Saw	OVER			DRY FT. ³	10 20 30 40 50 STANDARD
	REC	SURFACE ELEVATION +1,910.5		UNIT DRY WT. LBS./FT. ³	 PENETRATION BLOWS/(FT) 10 20 30 40 50
HS		FILL - CLAYEY SILT - little sand - trace plant brown - dry to moist (ML)	roots - light		
5.0 2 SS	Г	6.0			
		FILL - CLAY - little to trace silt and coal - gray	rish brown to		
HS 10.0		brownish gray - stiff to very stiff (CH)			
3 SS	Ш				
нз					
15.0 4 SS	+	FILL - CLAY - trace to little silt and coal - gray (CH)	- medium		
4 33					*
HS	Ц				
20.0 5 SS		21.0			
HS		FILL - SILTY CLAY - trace coal - gray - stiff to (CL-ML)	o very stiff		
25.0					
6 SS		27.0			
HS		FILL - fine CLAYEY SAND - little silt - trace c	oal - gray to		
30.0 7 SS	+	bluish gray - medium dense to loose (SC)			
					*
HS					
35.0 8 SS					
HS					
40.0					ТУ
9 SS					
HS		43.0 FILL - CLAY - little to trace sand, silt, and coa	l - gravish	$\left \right $	
45.0 10 SS		brown - medium to stiff (CH)			
HS HS		47.0 FILL - fine CLAYEY SAND - little silt - gray to	bluish arav -		
50.0		loose to medium dense (SC)			ту 9 _/
11 SS	Щ	***			
HS		***			
55.0 12 SS	+	***			
	╵┤┸	57.0			
HS		FILL - CLAY - little silt - trace coal - grayish b very stiff (CH)	rown - stiff to		
<u>60.0 </u>	╡	××××		L	↓' _ `_ ↓
		ent the approximate boundary lines between soil types: in situ, the trans			DM JOB NO. 60494667 SHEET NO. OF 1 2

<u> </u>				CLIENT Basin Electric Po	wer Cooperative	LOG OF BO		^{JMBER} B-2016-10 50 feet NW	
A=	C	JN	1	PROJECT NAME	· · · · · · · · · · · · · · · · · · ·	ARCHITEC		EER	
SITE LO	CATI			LOS ASH Landfil	Expansion	AECOM			ENG
			lera	er County, North	Dakota			$\begin{array}{c} -\underbrace{\text{TONS/FT.}^2} \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ \end{array}$	
) N(FT)			NCE					PLASTIC WATER LIQU LIMIT % CONTENT % LIMI	Т%
DEPTH(FT) ELEVATION(FT)	Ň	SAMPLE TYPE	SAMPLE DISTANCE		DESCRIPTION OF MATERIAL		UNIT DRY WT. LBS./FT. ³	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
	SAMPLE NO.	AMPLE	SAMPLE DI				NIT DR SS./FT.	STANDARD	FT)
X	ൾ 13		ο Ο		I +1,910.5 AY - little silt - trace coal - grayis	(Continue) h brown - stiff to	a) 5 9		
		нѕ		very stiff (CH)				
65.0	14	SS							
		нs							
70.0	15	SS							
		нs				trace all dark			
75.0	16	SS		gray - hard	BUTTE FORMATION - CLAY	- trace silt - dark		• + •	~
		нs							
<u>80.0</u> 81.0	17	SS		81.0					Q
				End of Bo Boring adv	ring vanced to 79.5 feet with 3.25-in	ch hollow-stem	*Ca	librated Penetrometer	
				auger	Penetration Test performed with				
				hammer	kfilled with chipped bentonite				
				Bonny bac	killed with chipped bentonite				
		The s	strat	fication lines represent th					
	J	5788	25.7	26	BORING STARTED 7/28/16				
		1784	372.	785	BORING COMPLETED 7/28/16		NTERED E	.B 2 2	
NL					77' RIG/FOREMAN D-90/MR (Terr	A	PP'D BY	AECOM JOB NO. 60494667	

ROJECT NUMBER <u>60514</u> PATE STARTED <u>8/7/2016</u> PRILLING CONTRACTOR _ PRILLING METHOD <u>Rotan</u> OGGED BY <u>Ryan Klutes</u> COORDINATES <u>577563.4</u>	4340 COMPLETED 8/7/20 Cascade Drilling y Sonic CHECKED BY A. Lanning	PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton, ND GROUND ELEVATION 1929.2 ft GROUND WATER LEVELS: AT TIME OF DRILLING	ev 1861.33 ft Casing Top Elev: 1.93 (ft)
POCKET PENE- POCKET PENE- TROMETER, TSF	U.S.C.S. GRAPHIC LOG	MATERIAL DESCRIPTION	Casing Type: 2" PVC Pipe WELL DIAGRAM Top of Casing (estimated 1.93' aqs)
0 5 5 5 5 6 6 7 7 7 7 7 7 7 7 7 7 7 7 7	CL 16.0 CL 20.0	ked material; light brown	- Grout (0' - 78' bgs) - PVC Pipe (1.93' ags - 96' bgs) - 1913.2

	IT <u>Basir</u> ECT NUN			4340		PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton, ND	I	
د DEPTH 32 (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION		WELL DIAGRAM
<u>35</u> - - 40	SONIC	100		CL		CLAY, sticky, reworked material; brown	1889.2	Grout (0' - 78' bgs) PVC Pipe (1.93' ags - 96 bgs)
- - 45	SUNIC	100		CL		SILTY CLAY, reworked material; light brown	1884.2	bgs)
- - - 50	SONIC	100				SANDY CLAY, very hard, crumbly; red		
- - 55_	SONIC	100		6				
- - 60 - - - 65	SONIC	100		CL				
- - 70 - -	SONIC	100		CL		CLAY, very hard, native material; gray	1863.2	

⁽Continued Next Page)

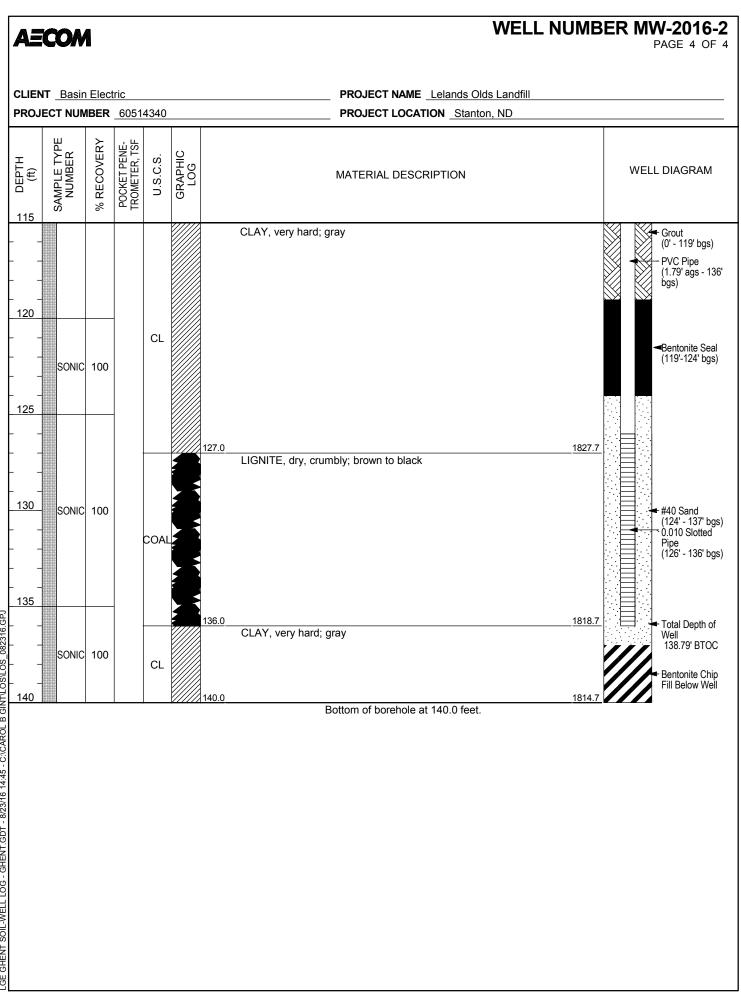


LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:43 - C:\CAROL B GINT\LOS\LOS 082316.GPJ

						PAGE 1 OF
CLIENT Basi	n Electr	ic			PROJECT NAME Lelands Olds Landfill	
PROJECT NU	IBER _	6051434	10		PROJECT LOCATION Stanton, ND	
					GROUND ELEVATION 1954.7 ft	HAMMER TYPE Not Applicable
					GROUND WATER LEVELS:	
COORDINATE				KED BY <u>A. Lanning</u> 5497.98 E	$\underline{\Psi} \text{ AFTER DRILLING } 107.05 \text{ ft / E}$	
						Casing Top Elev: 1.79 (ft)
H ZR	(ER)	C TSF	; ₽			Casing Type: 2" PVC Pipe
DEPTH (ft) APLE TY JUMBER	00	OMETER, T	GRAPHIC LOG		MATERIAL DESCRIPTION	WELL DIAGRAM
o DEPTH (ft) SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	5 ¹⁹			Top of Casing (estimated 1.79 ags)
A Construction of the second s	100	с с		20.0	reworked material; brown worked material; brown to light brown	

A	ECOA	A				WELL NUMB	ER MW-2016-2 PAGE 2 OF 4
	INT Basi					PROJECT NAME Lelands Olds Landfill	
PRO	JECT NU	MBER	6051	4340		PROJECT LOCATION Stanton, ND	
HL DEPTH 32	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
_	_			CL		SILTY CLAY, reworked material; gray	
_	_					<u>37.0</u> <u>1917.7</u>	Grout (0' - 119' bgs)
- - 40	- - 	100		CL		CLAY, sticky, reworked; brown 40.0 1914.7	(0' - 119' bgs) PVC Pipe (1.79' ags - 136' bgs)
- - - 45	- SUNI 	, 100	-	CL		S.A.A., brown to light brown	bgs)
- - - - - - - - - 55	- SONI(- SONI(2 100		CL		46.0 1908.7 SILTY CLAY, reworked material; light brown to gray 1908.7 54.0 1900.7 SILTY CLAY, reworked material; gray 1900.7	
	-		-	CL		58.0	
- TNSOL	-			CL		CLAY, reworked material; brown to gray	
16 14:44 - C:\CAROL B GINTI 9 9	- SONI(100				CLAYEY SILT, crumbly, reworked material; gray	
LGE GHENT SOIL-WELL LOG - GHENT GDT - 8/23/16 14:44 - C:/CAROL B GINTLOS/LOS_082316.GPJ 22 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	- - - - - - - - -	2 100		CL		72.0	

WELL NUMBER MW-2016-2 AECOM PAGE 3 OF 4 CLIENT Basin Electric PROJECT NAME Lelands Olds Landfill PROJECT NUMBER 60514340 PROJECT LOCATION Stanton, ND SAMPLE TYPE NUMBER POCKET PENE-TROMETER, TSF % RECOVERY GRAPHIC LOG U.S.C.S. DEPTH (ft) WELL DIAGRAM MATERIAL DESCRIPTION 75 CLAY, very sticky, reworked material; brown Grout (0' - 119' bgs) PVC Pipe (1.79' ags - 136' CL 78.0 1876.7 b̀gs) CLAY, reworked material; gray CL 80 80.0 1874.7 SONIC 100 CLAY, stiff, reworked material; gray CL 82.0 1872.7 LIGNITE; brown COA 84.0 1870.7 CLAY, reworked material; gray with orange clay fragments 85 CL 90 90.0 1864 SONIC 100 CLAY, with lignite fragments, reworked material; brown to light brown CL 95 LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:44 - C:\CAROL B GINT\LOS\LOS_082316.GPJ 97.0 1857.7 CLAY, hard, trace silt, native material; gray Slow drilling CL SONIC 100 100 100.0 1854.7 CLAY, very hard; gray 105 SONIC 100 Ţ CL 110 SONIC 100 115

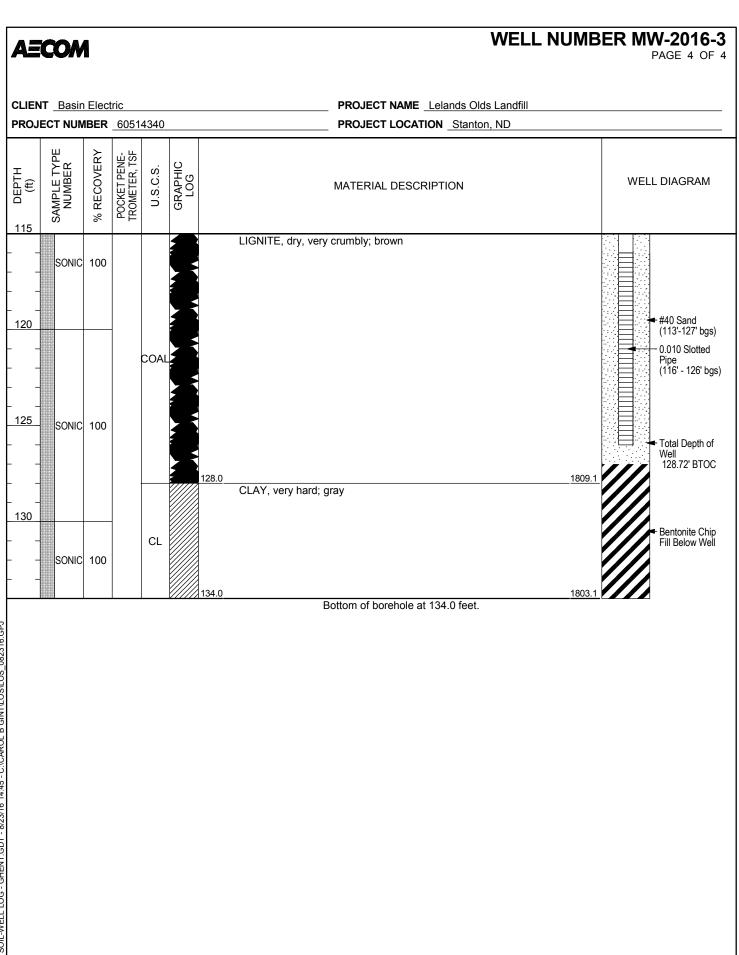


LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:45 - C:\CAROL B GINT\LOS\LOS 082316.GPJ

AECON	1					WELLI	NUME	BER I	WW-2016-3 PAGE 1 OF 4
DATE STARTE	MBER ED <u>8/</u>	_60514 5/2016	4340		COMPLETED <u>8/5/2016</u>	PROJECT LOCATION _Stanton, ND GROUND ELEVATION _1937.1 ft GROUND WATER LEVELS:	_ HAMM	ER TYPE	
DRILLING MET LOGGED BY COORDINATE	Ryan	Klutes		CHECI	KED BY <u>A. Lanning</u> 1880.82 E	AT END OF DRILLING			
o DEPTH (ft) SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		Casing	Top Elev: 1.72 (ft) Type: 2" PVC Pipe /ELL DIAGRAM Top of Casing (estimated 1.72' ags)
sonic sonic 	100	-	CL		CLAY, with fragme brown	ents of lignite, reworked material; brown to light			
 	2 100	-			10.0 CLAY, trace silt, re	eworked material; brown	<u>1927.1</u>		Grout (0' - 109' bgs) PVC Pipe (1.72' ags - 126' bgs)
	2 100	_	CL				4040.4		
 25 30 SONIC	2 100	-	CL		24.0 SILTY CLAY, rewo	orked material; gray	<u>1913.1</u> 1905.1		
			CL			I, very sticky, reworked material; brown (Continued Next Page)	1300.1		

A	ECON	A				WELL NUMBE	R MW-2016-3 PAGE 2 OF 4
	ENT <u>Basi</u>			4340		PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton, ND	
				-0-0			
DEPTH	SAN	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
- - - 40 - - -	-	100		CL		CLAY, trace gravel, very sticky, reworked material; brown <u>43.0</u> CLAY, with gray silt, reworked material; dark brown	Grout (0' - 109' bgs) PVC Pipe (1.72' ags - 126' bgs)
 		2 100		CL			
	- - -	2 100		CL		60.0 1877.1 CLAY, very sticky, reworked material; dark brown 62.5 1874.6 SILTY CLAY, hard, reworked material; gray	
	-	2 100		CL		68.0 1869.1 CLAY, reworked material; brown to orange 74.0 1863.1 CLAY, sticky, reworked material; brown	

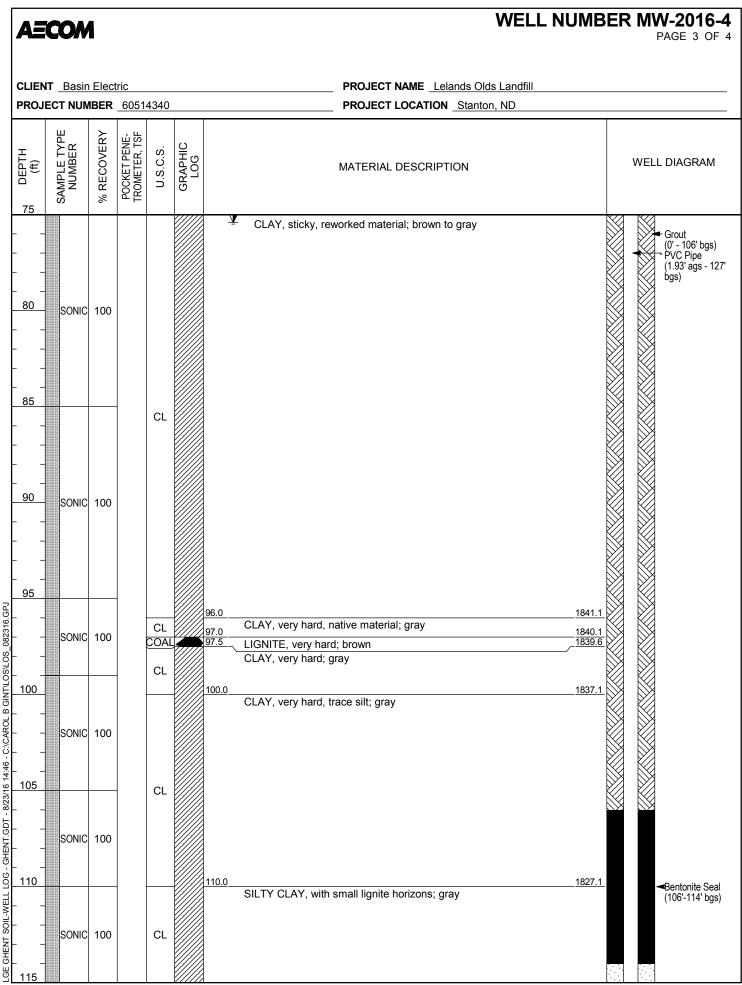
A	CON	1				WELL NUMB	ER M	W-2016-3 PAGE 3 OF 4
CLIEN	IT Basir	n Elec	tric			PROJECT NAME Lelands Olds Landfill		
PROJ		IBER	6051	4340		PROJECT LOCATION Stanton, ND		
HLL (ft) 25	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WEL	LL DIAGRAM
 85	SONIC	100		CL		CLAY, sticky, reworked material; brown <u>84.0</u> CLAY, trace silt, very hard, native soil; gray Very hard drilling		Grout (0' - 109' bgs) PVC Pipe (1.72' ags - 126' bgs)
	SONIC	100				Very hard drilling		
 - 95	SONIC	100		CL		Ā		
	SONIC	100				<u>100.0</u>		
100 14:49 - C:/CAKOF B GININ	SONIC	100				CLAY, very hard; gray Very hard drilling		← Grout (0' - 109' bgs) ○ PVC Pipe (1.72' ags - 126' bgs)
GHEN1.GD1 - 8/23/	SONIC	100		CL				
110 110 801-WETT F06-	SONIC	100	_					■Bentonite Seal (109-113')
EHEN 2010 - 115						115.0 1822.1		• • •



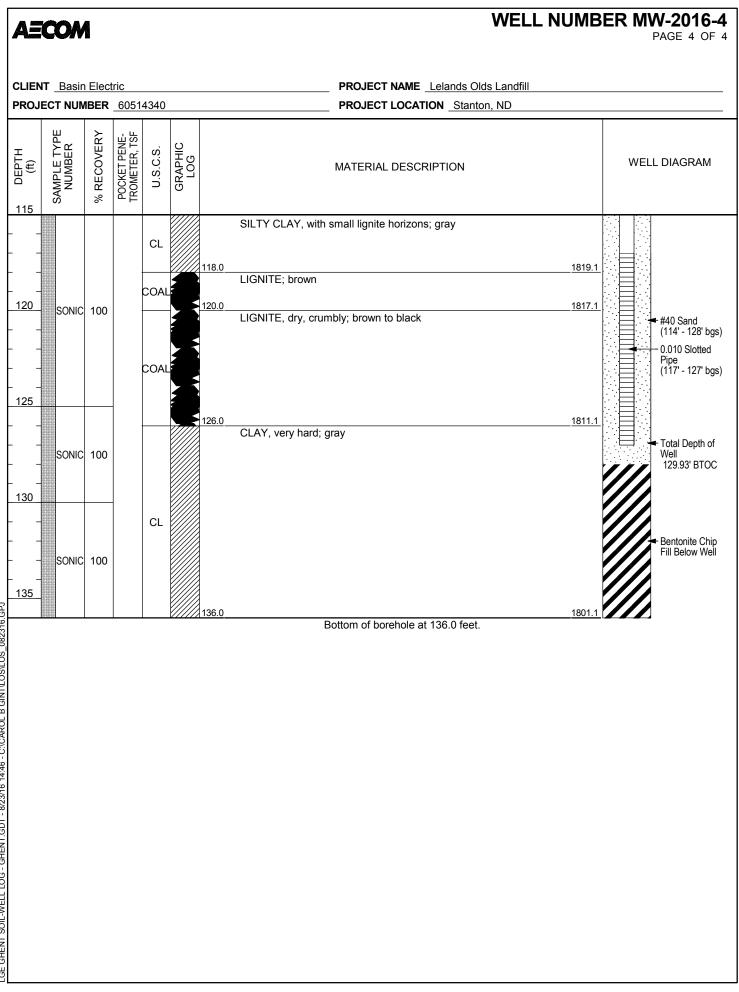
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Æ	CON	1						WEL	L NUMB	ER	MW-2016-4 PAGE 1 OF 4
CLIEN	T Basir	n Elect	tric					PROJECT NAME _Lelands Olds Landfill			
								PROJECT LOCATION Stanton, ND			
DATE	STARTE	D 8/2	2/2016			COMP	LETED <u>8/4/2016</u>	GROUND ELEVATION 1937.1 ft	HAMME	R TYP	E Not Applicable
								GROUND WATER LEVELS:			
	ING MET										
							A. Lanning				
COOR		S <u>578</u>	8282.62	2 N	1784	1229.27	Έ	V AFTER DRILLING _75.41 ft /	/ Elev 1861.69	ft	
	비	7	цŖ							Casing Casing	g Top Elev: 1.93 (ft) g Type: 2" PVC Pipe
Η	T≺I ØER	VEF	PEN ER, T	S.	GRAPHIC LOG						
DEPTH (ft)	PLE		AET METE	U.S.C.S.	Lod			MATERIAL DESCRIPTION			
	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF		5					◄	Top of Casing (estimated 1.93'
0		0.		0	<u> </u>	0.5			4000.0		ags)
				OL		0.5	ORGANIC SILT, to CLAY reworked ma	p soll; black aterial; red to brown		×.	
							0				
	SONIC	100		CL							
										×.	×.
5						1			4004.0		
						5.5	CLAYEY SILT, rew	orked material; light brown to gray	1931.6		
							,			\mathbb{X}	X
10											Grout (0' - 106' bgs)
	SONIC	100		ML							
				IVIL						₩ -	PVC Pipe (1.93' ags - 127'
										\mathbb{K}	bgs)
										×.	×
15											
						16.0	CLAY sticky rewo	rked material; brown to light brown	1921.1		
							OLAT, Sticky, Tewor	inced matchal, blown to light brown			
3											
										×	
20	SONIC	100									
5											
										\mathbb{N}	
				CL							
25											
			1		<i>\////</i>					\bowtie	
										\bowtie	×
					<i>\////</i>	1				\mathbb{M}	\bowtie
					V////					\bowtie	\bigotimes
30	SONIC	100								\boxtimes	
					¥////	31.0		rked material; light brown	1906.1	\bigotimes	
					V////		Lenses of sticky bro			\boxtimes	
				CL				-			
С1970					<i>\////</i>					Ň	×
35					V////					\mathbb{M}	

EA	CON	1				WELL NUME	BER MW-2016-4 PAGE 2 OF 4
	NT <u>Basir</u> ECT NUN			4340		PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton, ND	
PROJ				4340		PROJECT LOCATION _Station, ND	
HTHD (ff) 32	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
	-			CL		SILTY CLAY, reworked material; light brown Lenses of sticky brown clay 38.0 CLAYEY SILT, crumbly, reworked material; gray	Grout (0' - 106' bgs)
 45	- SONIC 	100		ML		45.0 1892.1	PVC Pipe (1.93' ags - 127' bgs)
 <u></u>	- - - SONIC	100		CL		CLAY, trace silt, reworked material; light brown to gray	
 <u>- 55</u>	-		-			51.0	
	SONIC	100		ML			
						64.0	- 🕅 📓
	SONIC	100	-	CL		CLAT, SUCKY, reworked material; moist, drown to light drown	
				COAI		73.0 1864.1 73.5 LIGNITE, crumbly; brown to black 1863.6	
75				CL		CLAY, sticky, reworked material; brown to gray	



⁽Continued Next Page)



LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:46 - C:\CAROL B GINT\LOS\LOS_082316.GPJ

PROJECT NUMBER _60514340 PROJECT LOCATION _Stanton, ND DATE STARTED _8/10/2016 COMPLETED _8/10/2016 GROUND ELEVATION _1935.2 ft HAMMER TYPE _Not Applicable DRILLING CONTRACTOR _Cascade Drilling GROUND WATER LEVELS: GROUND WATER LEVELS: DRILLING METHOD _Rotary Sonic AT TIME OF DRILLING AT END OF DRILLING LOGGED BY _Ryan Klutes _ CHECKED BY _A. Lanning _ COORDINATES _577257.45 N 1783618.06 E ¥ AFTER DRILLING _49.81 ft / Elev 1885.39 ft U	PROJECT NUMBER 60514340 PROJECT LOCATION Stanton, ND DATE STARTED 8/10/2016 COMPLETED 8/10/2016 GROUND ELEVATION 1935.2 ft HAMMER TYPE Not Applicable DRILLING CONTRACTOR Cascade Drilling GROUND WATER LEVELS: AT TIME OF DRILLING	AECOM	WELL NUMBER MW-2016-5 PAGE 1 OF 3
DATE STARTED 8/10/2016 COMPLETED 8/10/2016 GROUND ELEVATION 1935.2 ft. HAMMER TYPE Not Applicable DRILLING CONTRACTOR Cascade Drilling GROUND WATER LEVELS: AT TIME OF DRILLING	DATE STARTED 8/10/2016 COMPLETED 8/10/2016 GROUND ELEVATION 1935.2 11 HAMMER TYPE Not Applicable. DRILLING CONTACTOR Cascade Drilling CORDINATE LEVELS: AT END OF DRILLING	CLIENT Basin Electric	PROJECT NAME Lelands Olds Landfill
LOGGED BY Name CHECKED BY A. Lanning	LOGGE DP Y Rvan Klutes	DATE STARTED _8/10/2016 COMPLETED _8 DRILLING CONTRACTOR _Cascade Drilling	/10/2016 GROUND ELEVATION _1935.2 ft HAMMER TYPE _Not Applicable GROUND WATER LEVELS: GROUND WATER LEVELS:
COORDINATES 577257.45 N 1783618.06 E Image: Coordinates in the image: Co	COORDINATES 577257.45 N 1783618.06 E Y AFTER DRILLING 4981 ft / Elev 1885.39 ft H_B_B_B H_B_B_B H_B_B_B H_B_B_B IS IS <td< td=""><td></td><td></td></td<>		
Huge Verticating Type: 2" PVC Pipe WELL DIAGRAM Verticating Type: 2" PVC Pipe WELL DIAGRAM Verticating Type: 2" PVC Pipe WELL DIAGRAM Casing Type: 2" PVC Pipe WELL DIAGRAM Casing Type: 2" PVC Pipe Verticating Type: 2" PVC Pipe Verticatin	Hard August of the second		
0 -	0 -		Casing Top Elev: 1.11 (ft) Casing Type: 2" PVC Pipe
- SONIC 100 CLAY, reworked material; brown - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -	SONC 100 CLAY, reworked material; brown 5 CLAY, reworked material; brown 10 SONC 100 10 SONC 100 15 CL 20 CLAY, with lignite fragments, reworked material; brown 20 CLAY, with lignite fragments, reworked material; brown 21 SONC 100 25 SONC 100 26 SONC 100 27 SONC 100 28 SONC 100 29 SONC 100 20 CLAY, with lignite fragments, reworked material; brown 19152 30 SONC 100 310 SANDY CLAY, reworked material; light brown 1904.2		Top of Casing (estimated 1.11)
	25 SONIC 100 30 35 SONIC 100 CL CL CL CL SANDY CLAY, reworked material; light brown 1904.2	SONIC 100 SONIC 100 CL	eworked material; brown Grout (0' - 97' bgs) - PVC Pipe (1.11' ags - 118'

	IT <u>Basir</u> ECT NUN			4340		PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton, ND				
6 DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION		WELL DIAGRAM		
	SONIC	100		CL		CLAY, reworked material; brown	1891.7	Grout (0' - 97' bgs) PVC Pipe (1.11' ags - 118'		
 _ <u>45 _</u> 			-	CL		SANDY CLAY, reworked material; gray	1888.2	bgs)		
 <u>50</u>	SONIC	100		CL		CLAY, sticky, reworked material; brown				
 <u>55</u>			-	CL		52.0 SANDY CLAY, reworked material; brown with orange clay horizons	1883.2			
 <u>60</u>	SONIC	100				60.0 SANDY CLAY, trace gravel, reworked material; gray	_1875.2			
 _ <u>_ 65</u>			-	CL		65.0	1870.2			
 	SONIC	100		CL						
 			-	CL		CLAY, with lignite fragments, very hard; gray	1862.2			
80	SONIC	100		CL		CLAY, sticky, trace gravel and lignite fragments, reworked materials; brown	_ <u>1857.7</u> _ <u>1855.2</u>			
				CL		CLAY, with lignite fragments, reworked materials; brown to light brown				
 			_	CL		CLAY, with lignite, reworked horizons; brown with orange clay horizons	<u>1851.2</u>			

A	CON					WELL NUME	BER MW-2016-5 PAGE 3 OF 3
	IT Basir	1 Elect	ric			PROJECT NAME Lelands Olds Landfill	
				4340		PROJECT LOCATION Stanton, ND	
DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
 <u>90</u> 	SONIC	100		CL		CLAY, with lignite, reworked horizons; brown with orange clay horizons 88.5 1846. SANDY CLAY, very hard, crumbly, reworked material; light brown	Control (0' - 97' bgs) PVC Pipe (1.11' ags - 118' bgs)
	SONIC	100		CL		94.0	
 _ 105 	SONIC	100		CL		100.0 CLAY, trace silt, very hard; gray Very hard drilling	2 →Bentonite Seal (97'-105' bgs)
	SONIC			COAI		110.0	2
	SONIC	100		CL		116.0 1819.: CLAY, hard; gray	Total Depth of Well 120.11' BTOC Bentonite Chip Fill Below Well
					<u>,,,,,,,,</u>	Bottom of borehole at 123.0 feet.	

AECOM		WELL	NUMBER MW-2016-6 PAGE 1 OF 3
		PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton, ND	
DATE STARTED _8/9/2016 DRILLING CONTRACTOR _ DRILLING METHOD _Rota	COMPLETED <u>8/9/2016</u> Cascade Drilling ry Sonic CHECKED BY <u>A. Lanning</u>	GROUND ELEVATION <u>1936.3 ft</u> GROUND WATER LEVELS: AT TIME OF DRILLING AT END OF DRILLING	
DEPTH (ft) (ft) sample type NUMBER % RECOVERY POCKET PENE- TROMETER, TSF		MATERIAL DESCRIPTION	Casing Top Elev: 2.15 (ft) Casing Type: 2" PVC Pipe WELL DIAGRAM Top of Casing (estimated 2.15' ags)
SONIC 100 	CLAY, reworked	I material; brown to light brown	
		worked material; brown	1925.3
	CL 31.0		(2.15' ags - 113' bgs)
	CL SANDY CLAY, r	eworked material; gray	1901.3

A E	CON					WELL NUME	BER MW-2016-6 PAGE 2 OF 3				
	NT <u>Basin</u>			1310		PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton ND					
PRUJ			<u> </u>	+340		PROJECT LOCATION Stanton, ND					
(ft) 22 (ft) 22	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM				
35						CLAY, reworked material; light brown					
 40				CL		40.0	Grout (0' - 95' bgs) PVC Pipe (2.15' ags - 113' bgs)				
	SONIC	100		CL		SILTY CLAY, stiff, reworked material; gray	bgs)				
45						45.0					
	- SONIC	100		CL		SANDY CLAY, very soft, reworked material; gray with brown clay lenses					
	SONIC	100		CL		60.0 1876.3 SANDY CLAY, reworked material; gray with brown clay lenses 1876.3 71.5 1864.8 SANDY CLAY, with lignite fragments, reworked material; gray 1864.8					
	-			CL							

AECOM PAGE 3 OF 3 CLIENT Basin Electric PROJECT NAME Lelands Olds Landfill PROJECT NUMBER 60514340 PROJECT LOCATION Stanton, ND SAMPLE TYPE NUMBER POCKET PENE-TROMETER, TSF % RECOVERY GRAPHIC LOG U.S.C.S. DEPTH (ft) WELL DIAGRAM MATERIAL DESCRIPTION 75 SANDY CLAY, with lignite fragments, reworked material; gray Grout (0' - 95' bgs) PVC Pipe CL (2.15' ags - 113' b̀gs) 1857.3 79.0 CLAY, with lignite fragments, reworked material; brown 80 SONIC 100 CL 84.0 1852.3 CLAY, very hard, native material; gray 85 SONIC 100 90 CL SONIC 100 LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 13:37 - C.\CAROL B GINT\LOS\SAMPLE TEMPLATE.GPJ 95 SONIC 100 Bentonite Seal (95'-100' bgs) 100 100.0 1836.3 CLAY, very hard, native material; gray Very hard drilling SONIC 100 CL 105 106.0 1830.3 LIGNITE, crumbly; brown SONIC 100 0.010 Slotted Pipe (103' - 113' bgs) COAL 110 SONIC 100 113.0 1823.3 Total Depth of CLAY, very hard; gray CL Well 114.0 1822.3 116.15' BTOC Bottom of borehole at 114.0 feet.

WELL NUMBER MW-2016-6

NECC	M					vv	ELL NUMBER MW-201 PAGE 1				
	Basin	Elect	ric			PROJECT NAME Lelands Olds Lar	ndfill				
ROJECT	NUM	BER				PROJECT LOCATION Stanton, ND					
ATE STA	RTE) <u>8/8</u>	3/2016		(COMPLETED <u>8/8/2016</u> GROUND ELEVATION <u>1926</u>	GROUND ELEVATION _ 1926.6 ft HAMMER TYPE _ Not Applicable				
RILLING	CON	TRAC	TOR _	Case	ade Dr	lling GROUND WATER LEVELS:					
RILLING											
						¥					
) JORDIN/	ATES	_ 576	5226.36	5 N	17850	<u>171.11 E</u> ¥ AFTER DRILLING <u>72.</u> €	93 ft / Elev 1853.67 ft				
비		۲۲	цŖ				Casing Top Elev: 1.7 (ft Casing Type: 2" PVC P				
(ft) SAMPLE TYPE	BER	% RECOVERY	POCKET PENE- TROMETER, TSF	C.S.	GRAPHIC LOG		WELL DIAGRA				
(ft) IPLE T	IN I	ECC	METI	U.S.C.S.	LOR	MATERIAL DESCRIPTION					
SAM	z	% R	TRO	ر	U D		Top of Cas (estimated				
0						CLAY, sticky, reworked material; brown to light brown	ags)				
-											
S	ONIC	100									
5				CL							
_											
-											
-											
0						.5	<u>1917.1</u> Grout (0' - 56' bg				
S	ONIC	100				SILTY CLAY, reworked material; gray					
							PVC Pipe (1.70' ags				
							bgs)				
_				CL							
5											
-											
-											
						9.0	1907.6				
0						CLAY, reworked material; brown to light brown					
-											
-											
5				CL							
S S	ONIC	100									
0						0.0 SILTY CLAY, reworked material; gray	1896.6				
-						SILTI CLAT, TEWOREU Material, gray					
-											
-				CL							
5											
						6.0	1890.6				
				_		CLAY, sticky; brown	Grout				
				CL			(0' - 56' bg				
100000000					11/1/1						

	IT Basir					PROJECT NAME Lelands Olds Landfill			
PROJ	ECT NUN	IBER	60514	1340		PROJECT LOCATION Stanton, ND			
6 DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION		WEL	L DIAGRAM
-	SONIC	100		CL	43.	CLAY, sticky, reworked material; brown CLAYEY SILT, hard, reworked material; gray			bgs)
<u>45</u> - -				ML	47.	CLAY, sticky, reworked material; brown	_1879.1		
50	SONIC	100		CL CL	51.	CLAY, with lignite and gravel fragments, reworked material; brown			
<u>55</u> -				CL	54.	SILTY CLAY, reworked material; gray			
- - 60 -	SONIC	100	-	CL	<u>58.</u> 60.	CLAY, sticky, reworked material; brown	<u>1868.1</u> <u>1866.6</u>		Bentonite Se (56'-61 bgs')
- - 65				CL	<u>65.</u>		1861.6		
- - 70	SONIC	100		CL	66.	LIGNITE, powdery; black to brown	1860.6		 #40 Sand (61' - 76' bgs) — 0.010 Slotted Pipe (65' - 75' bgs)
- - 75 -					74.	∑ CLAY, very hard; gray	1852.6		 G5 - 75 bgs, Total Depth c Well 77.70' BTOC
- - 80 -	SONIC	100		CL					← Bentonite Ch Fill Below We

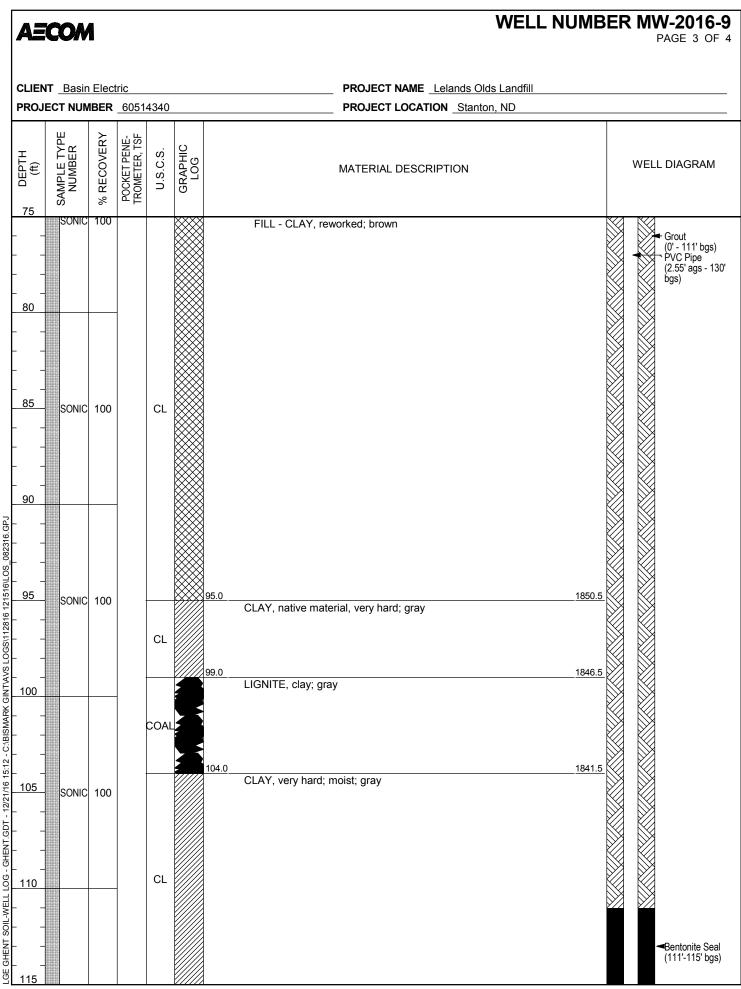
DATE STARTE DRILLING CON DRILLING MET	IBER D <u>8/8</u> ITRAC	_60514 3/2016 TOR _ Rotan Klutes 3383.7	1340 Casc y Sor	COMPL ade Drilling iic CHECKED BY		878.97 ft
DEPTH (ft) SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	Casing Top Elev: 1.67 (ft) Casing Type: 2" PVC Pipe WELL DIAGRAM Top of Casing (estimated 1.67' ags)
	100				AY, reworked material; brown	
	100		CL	14.0		- Grout (0' - 87' bgs) - PVC Pipe (1.67' ags - 106' bgs)
			CL	20.0	NDY CLAY, reworked material; light brown AY, reworked material; brown with light brown sandy clay zons	_1916.9
	100		CL			

A	CON	1				WELL NUMB	ER MW-2016-8 PAGE 2 OF 3				
	IT <u>Basir</u> ECT NUN			4340		PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton, ND					
C DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF		GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM				
 40	SONIC	100		CL		CLAY, reworked material; brown with light brown sandy clay horizons	Grout (0' - 87' bgs) PVC Pipe (1.67' ags - 106'				
 <u>45</u>		. 100		CL		CLAY, with sandy clay, reworked material; brown with gray clay horizons	bgs)				
 <u>50</u>	SONIC	100	00	,	CL		47.5 1889.4 CLAY, reworked material; brown 1889.4 52.0 1884.9				
316.GPJ			-	CL		CLAY, with lignite, reworked material; brown 55.0 SANDY CLAY, reworked material; brown					
	SONIC	100	D	CL	CL CL	Image: Set of the system 1878.4 CLAY, with lignite fragments, sticky, reworked material; brown 1876.9 CLAY, sticky, reworked material; brown 1876.9					
- 8/23/16 14:52 - C:/CARC - 0 - 0 - 0 - 0 - 0 - 0 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1			-	CL		64.0 1872.9 SANDSTONE, poorly cemented, very crumbly; red to orange					
LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:52 - C:\CAROL B GINTILOSLOS_082316.GPJ	SONIC	100	SAN	IDST	ONE						

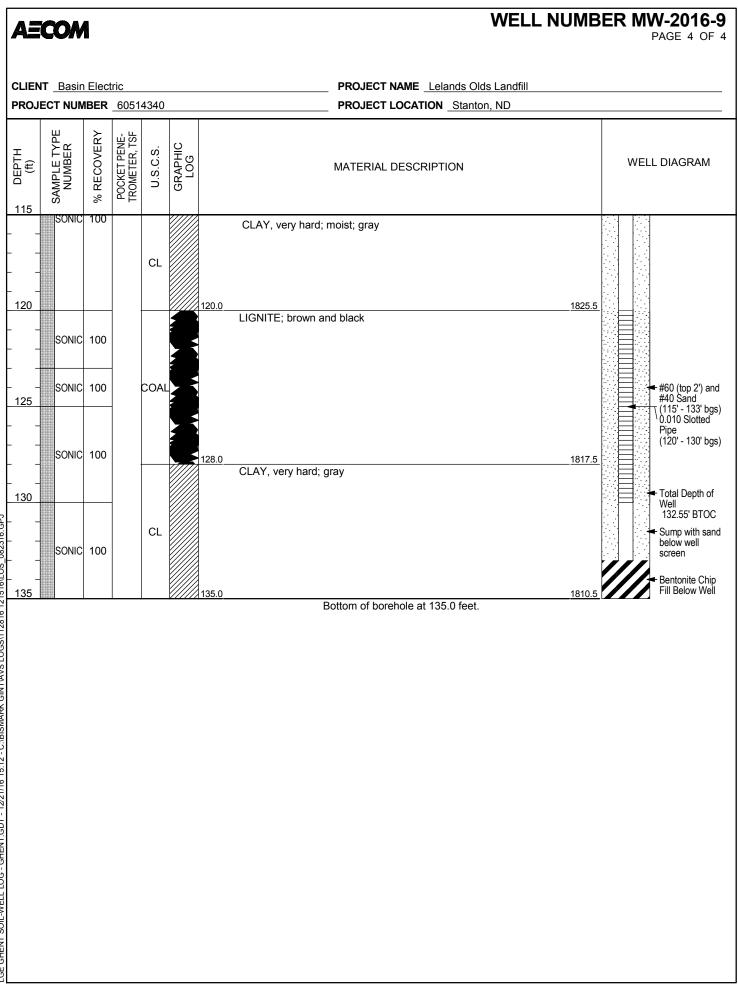
WELL NUMBER MW-2016-8 AECOM PAGE 3 OF 3 CLIENT Basin Electric PROJECT NAME Lelands Olds Landfill PROJECT NUMBER 60514340 PROJECT LOCATION Stanton, ND SAMPLE TYPE NUMBER POCKET PENE-TROMETER, TSF % RECOVERY GRAPHIC LOG U.S.C.S. DEPTH (ft) WELL DIAGRAM MATERIAL DESCRIPTION 75 SANDSTONE, poorly cemented, very crumbly; red to orange Grout (0' - 87' bgs) PVC Pipe (1.67' ags - 106' SANDSTONE b̀gs) 80 80.0 1856.9 SONIC 100 CLAY, very hard; light brown CL 83.5 1853.4 CLAY, very hard, native material; gray 85 90 Bentonite Seal (87'-93' bgs) SONIC 100 CL 95 LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:52 - C:\CAROL B GINT\LOS\LOS 082316.GPJ SONIC 100 - #40 Sand (93' - 107' bgs) 100 100.0 1836.9 LIGNITE, crumbly; brown to black 0.010 Slotted Pipe (96' - 106' bgs) COAL SONIC 100 105 106.0 1830.9 Total Depth of CLAY, hard; gray CL Well 107.0 1829.9 108.67' BTOC Bottom of borehole at 107.0 feet.

PROJECT NUMBER <u>6051</u> DATE STARTED <u>11/2/201</u> DRILLING CONTRACTOR DRILLING METHOD <u>Rotan</u>	4340 6 COMPLETED 11/3/2016 Cascade Drilling ry Sonic	PROJECT NAME <u>Lelands Olds Landfill</u> PROJECT LOCATION <u>Stanton, ND</u> GOUND ELEVATION <u>1945.505 ft</u> GROUND WATER LEVELS: AT TIME OF DRILLING	
	CHECKED BY A. Lanning 26 N 1785499.348 E		
 DEPTH (ft) SAMPLE TYPE SAMPLE TYPE NUMBER % RECOVERY POCKET PENE- TROMETER, TSF 	U.S.C.S. GRAPHIC LOG	MATERIAL DESCRIPTION	Casing Top Elev: 2.55 (ft) Casing Type: 4" PVC Pipe WELL DIAGRAM Top of Casing (estimated 2.55' ags)
- - - - - - - - <td>CL</td> <td>vorked; brown</td> <td>• Grout (0' - 111' bgs) • PVC Pipe (2.55' ags - 130' bgs)</td>	CL	vorked; brown	• Grout (0' - 111' bgs) • PVC Pipe (2.55' ags - 130' bgs)

AECOM						WELL	WELL NUMBER MW-2016-9 PAGE 2 OF 4			
	IT <u>Basir</u> ECT NUN			4340		PROJECT NAME _Lelands Olds Landfill PROJECT LOCATION _Stanton, ND				
(ff) 35	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM			
	SONIC	100		CL		FILL - CLAY, reworked; brown	Grout (0' - 111' bgs) PVC Pipe (2.55' ags - 130 bgs)			
 70	SONIC	100								
 75										



⁽Continued Next Page)



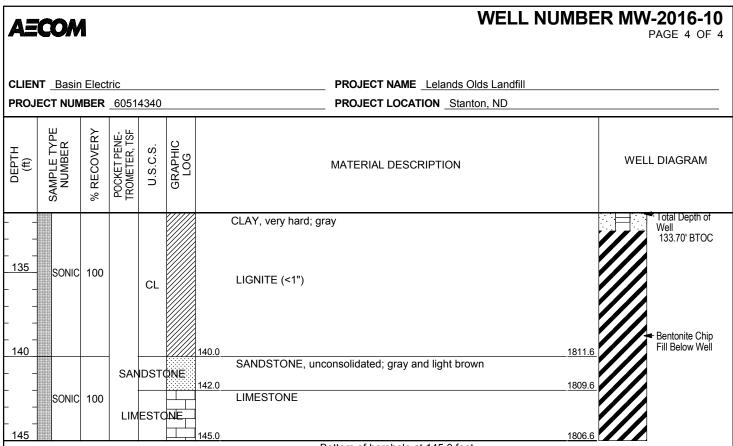
LGE GHENT SOIL-WELL LOG - GHENT.GDT - 12/21/16 15:12 - C.\BISMARK GINTAVS LOGS/112816 121516\LOS_082316.GPJ

CLIENT Basin Electric PROJECT NUMBER 60514340 DATE STARTED 11/4/2016 COMPLETED 11/5/2016 DRILLING CONTRACTOR Cascade Drilling DRILLING METHOD Rotary Sonic LOGGED BY Ryan Klute CHECKED BY A. Lanning COORDINATES 577524.198 N 1786051.255 E					comp ade Drilling hic CHECKED BY	LETED <u>11/5/2016</u>	PROJECT NAME <u>Lelands Olds Landfill</u> PROJECT LOCATION <u>Stanton, ND</u> GROUND ELEVATION <u>1951.612 ft</u> GROUND WATER LEVELS: AT TIME OF DRILLING AT END OF DRILLING	
DEPTH (ft)	SAMPLE IYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION	Casing Top Elev: 1.7 (ft) Casing Type: 4" PVC Pipe WELL DIAGRAM Top of Casing (estimated 1.7' ags)
 	SONIC			CL		FILL - CLAY, rewor	ked; brown	- Grout (0' - 114' bgs) - PVC Pipe (1.7' ags - 132' bgs)
 25 30 30	SONIC	100						
 <u>35</u> 40	SONIC	100						

EA	ico/	M				WELL N	UMBER MW-2016-10 PAGE 2 OF 4
	CLIENT Basin Electric					PROJECT NAME Lelands Olds Landfill	
PROJ	IECT NU	JMBEF	R <u>605</u>	14340		PROJECT LOCATION Stanton, ND	
(#) 6	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER. TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
		IC 100				FILL - CLAY, reworked; brown	Grout (0' - 114' bgs) PVC Pipe (1.7' ags - 132' bgs)
5:10 - C./BISMARK GINTAVS LOGS/112816 12151	- SON	IC 100)	CL			
LGE GHENT SOIL-WELL LOG - GHENT GDT - 12/21/18 15:10 - C.\BISIMARK GINTAVS LOGS/12816 121 20 20 20 20 20 20 20 20 20 20	- SON - SON 	IC 100)				
	SON	IC 100				(Continued Next Page)	

	ECON	1				WELL NUMBE	-2016-10 PAGE 3 OF 4
CLIE	NT Basir	n Elect	tric			PROJECT NAME Lelands Olds Landfill	
				4340		PROJECT LOCATION _Stanton, ND	
DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	DIAGRAM
 			-	CL		FILL - CLAY, reworked; brown 94.0 LIGNITE; black and brown	- Grout (0' - 114' bgs) PVC Pipe (1.7' ags - 132' bgs)
<u>95</u> - - 100	- SONIC	100	-	COAL		96.0	
- <u>105</u> - <u>105</u> - <u>110</u>	- SONIC - SONIC 	100		CL			
918 110 918 110 919 110 910 100 910 100 910 100 910 100 910 100 910		100					■Bentonite Seal (114'-117' bgs)
125 - 125 - 125 - 125 - 130 - 130	- SONIC	: 100		COAL		122.0 1829.6 LIGNITE; brown 130.0 1821.6 CLAY, very hard; gray	#60 (top 2') and #40 Sand (117' - 132.5' bgs) 0.010 Slotted Pipe (122' - 132' bgs)

⁽Continued Next Page)



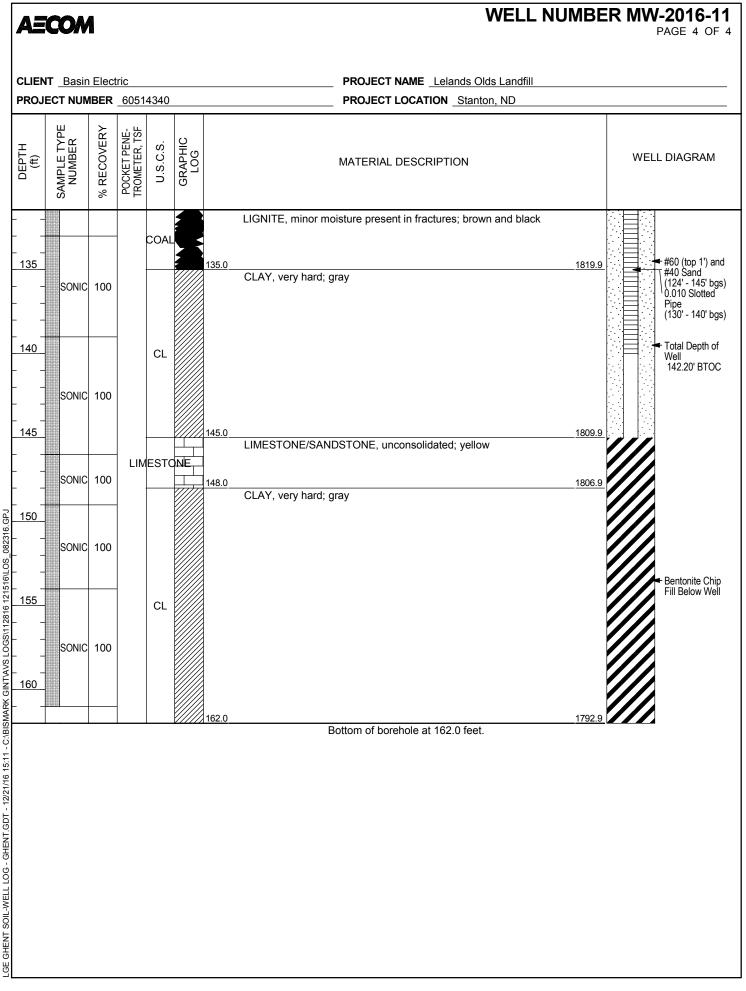
Bottom of borehole at 145.0 feet.

DATE STARTED _11/18/2016 COMPLETED _11/20/2016 DRILLING CONTRACTOR _Cascade Drilling DRILLING METHOD _Rotary Sonic LOGGED BY _Ryan Klute CHECKED BY _A. Lanning COORDINATES _577977.515 N				4340 16 Casc ry Son	COMPLE cade Drilling nic CHECKED BY	ETED <u>11/20/2016</u>	PROJECT NAME <u>Lelands Olds Landfill</u> PROJECT LOCATION <u>Stanton</u> , ND GROUND ELEVATION <u>1954.851 fm</u> GROUND WATER LEVELS: AT TIME OF DRILLING AT END OF DRILLING	t HAMMER TYPENot Applicable
DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION	Casing Top Elev: 1.2 (ft) Casing Type: 4" PVC Pipe WELL DIAGRAM
 	SONIC			CL		FILL - CLAY, rewor	ked; brown	ags)
 30	SONIC	100						
 35 40	SONIC	100						

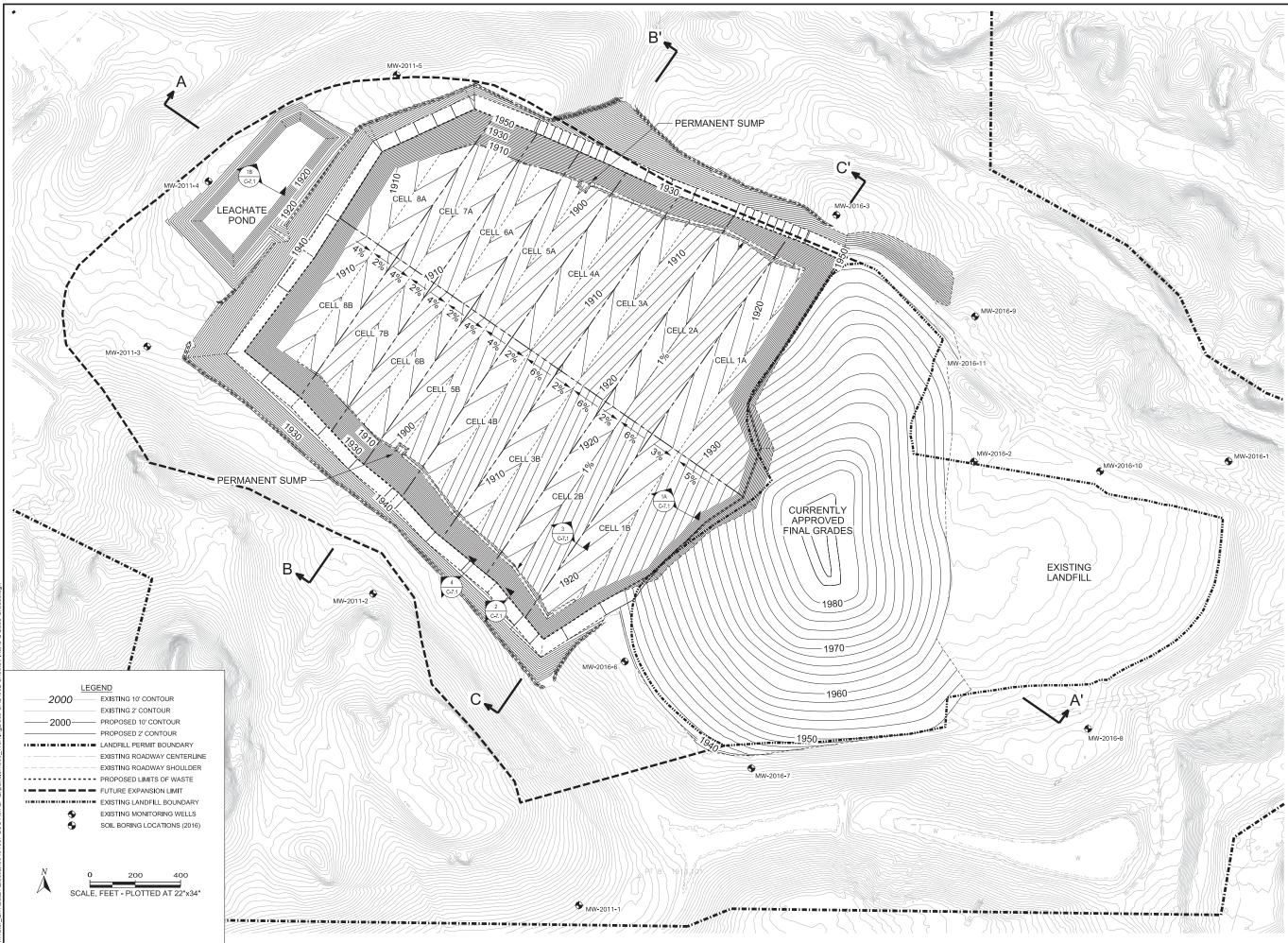
A	ECON	8				WELL NUMB	ERI	WW-2016-11 PAGE 2 OF 4
CLIE	NT Basir	n Elec	tric			PROJECT NAME Lelands Olds Landfill		
PRC		/IBER	6051	4340		PROJECT LOCATION Stanton, ND		
DEPTH (#)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION		WELL DIAGRAM
40 -		100		CL		FILL - CLAY, reworked; brown		Grout (0' - 120' bgs) PVC Pipe (1.2' ags - 140' bgs)

⁽Continued Next Page)

EA	CON					WELL NUMBE	ER N	/-2016-11 PAGE 3 OF 4
	IT <u>Basir</u> ECT NUN			4340		PROJECT NAME _Lelands Olds Landfill PROJECT LOCATION _Stanton, ND		
DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION		L DIAGRAM
 - 90 			-	CL		FILL - CLAY, reworked; brown 94.0 SANDSTONE/CHERT, unconsolidated, reworked material; orange		← Grout (0' - 120' bgs) ▼ PVC Pipe (1.2' ags - 140' bgs)
<u>95</u> 100	SONIC	100	SAN	CL		97.0 FILL - CLAY, reworked; brown and orange 100.0 FILL - CLAY, reworked, minor lignite fragments; brown and		
SO2346:GPJ	SONIC	100		CL		orange 103.0 1851.9 FILL - CLAY, reworked material; orange 186.0 106.0 1848.9 CLAY/SILT, very hard; gray 1848.9		
VS LOGSVI12816 121516/L			-	CL		110.0 LIGNITE (<1") 1844.9 CLAY, crumbly, native material; gray		
115	SONIC	100		CL		120.0 1834.9		
TTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTT	SONIC	100	-	CL		CLAY, very hard; gray		■Bentonite Seal (120'-124' bgs)
	SONIC	100		COAL		128.0 1826.9 LIGNITE, minor moisture present in fractures; brown and black		



Appendix C – Permitted Base Grade Plan Sheet



lectric/60494667 LOS Ash LF Expansion/900_WorkingDocs-CAD/902-Sheets/Final/C-2 Base Gre

PROJECT

LELAND OLDS STATION ASH LANDFILL EXPANSION - PHASE 6 SPECIAL WASTE LANDFILL PERMIT SP-143

CLIENT

BASIN ELECTRIC POWER COOPERATIVE 1717 EAST INTERSTATE AVE BISMARCK, NORTH DAKOTA 58503-0564

CONSULTANT

AECOM 800 LASALLE AVENUE, SUITE 500 MINNEAPOLIS, MN 55402 612-376-2000 tel 612-376-2271 fax www.aecom.com

REGISTRATION



ISSUE/REVISION

1	2017-02-24	ISSUED-PERMIT SUBMITTAL
l/R	DATE	DESCRIPTION

NOTES

TOPOGRAPHIC SURVEY BY KBM, NOVEMBER 2015. TOPOGRAPHY UPDATED BY BEPC, OCTOBER 5, 2016.

COORDINATES ARE ND STATE PLANE SOUTH, NAD 1929.

PROJECT NUMBER

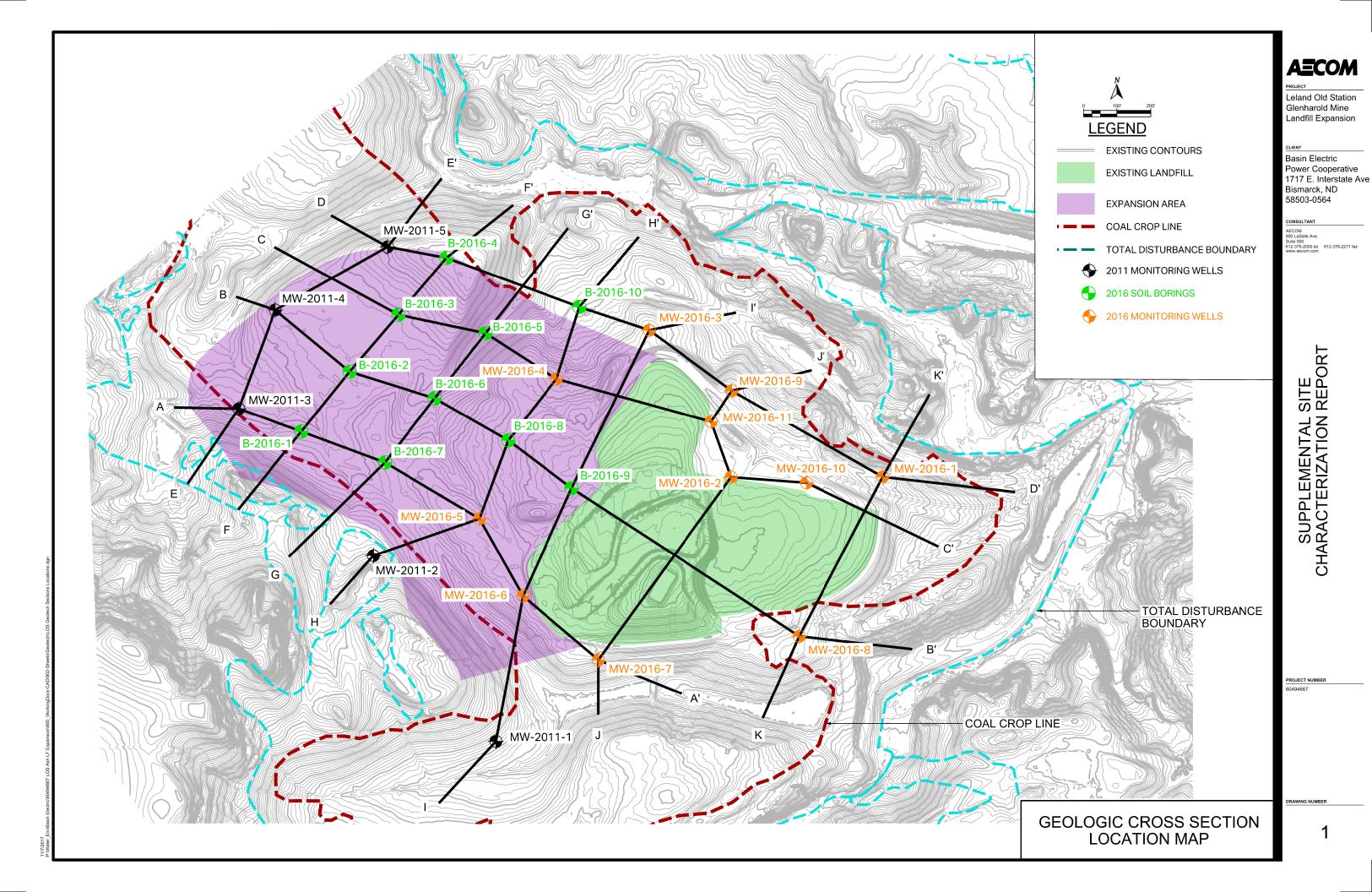
60494667

SHEET TITLE BASE GRADES

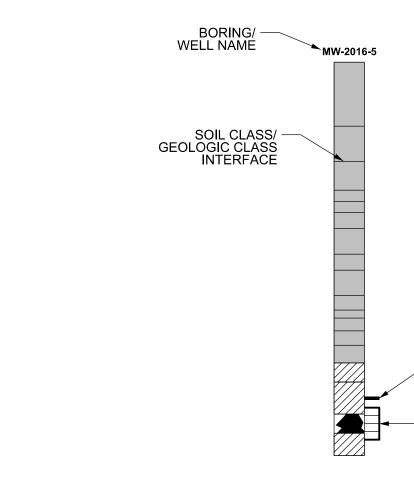
SHEET NUMBER

C-2.0

Appendix D – Geologic Cross Sections



 EXISTING GRADE	FILL (SEE LOGS FOR DESCRIPTIONS)
 PROPOSED EXPANSION BASE GRADE	COAL/LIGNITE
 PROPOSED EXPANSION FINAL GRADE	CLAY
 EXISTING LANDFILL BASE GRADE	
 EXISTING LANDFILL FINAL GRADE	 SANDSTONE
 CONTACT BETWEEN GEOLOGIC UNITS	SILTY CLAY
 INFERRED CONTACT BETWEEN GEOLOGIC UNITS	CLAYEY SAND
 PIEZOMETRIC SURFACE (SEPT. 27, 2016, 3rd QUARTER)	LIMESTONE



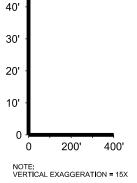
- 1. ELEVATIONS ARE BASED ON THE NORTH AMERICAN VERTICAL DATUM OF 1927. HORIZONTAL DATUM IS BASED ON THE NORTH DAKOTA STATE PLANE COORDINATE SYSTEM OF 1927 SOUTH ZONE.
- 2. BORING LOG ELEVATIONS REPRESENT GROUND SURFACE ELEVATIONS AT THE TIME OF DRILLING.
- 3. FINAL BORING LOGS BASED ON FIELD VISUAL IDENTIFICATION AND GEOTECHNICAL LABORATORY TEST RESULTS.
- 4. THE DEPTH AND THICKNESS OF SUBSURFACE STRATA INDICATED ON THESE CROSS-SECTIONS WERE GENERALIZED FROM AND INTERPOLATED BETWEEN BORINGS. INFORMATION ON ACTUAL SUBSURFACE CONDITIONS EXISTS ONLY AT THE LOCATION OF THE BORINGS.
- 5. GROUNDWATER ELEVATIONS WERE OBTAINED ON SEPTEMBER 27, 2016.

LEGEND OF THE GEOLOGIC CROSS SECTIONS

SCREENED ZONE

BOTTOM OF SEAL





50'



Leland Old Station Glenharold Mine Landfill Expansion

CLIENT

Basin Electric Power Cooperative 1717 E. Interstate Ave Bismarck, ND 58503-0564

CONSULTANT

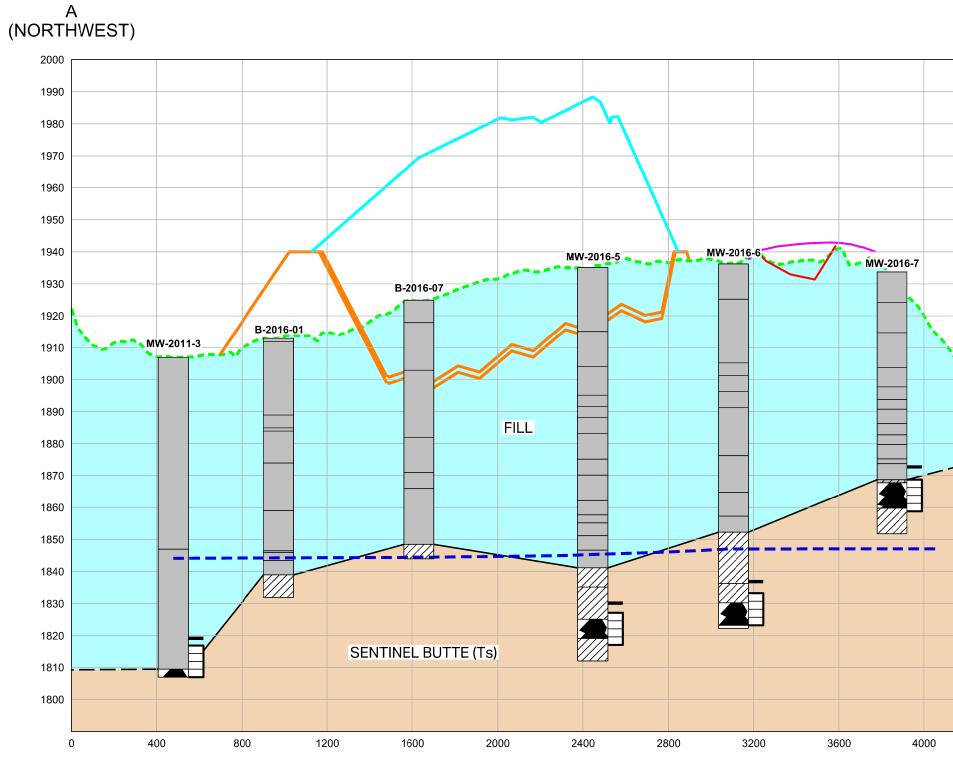
AECOM 300 LaSalle Ave Suite 500 512-376-2000 tel 612-376-2271 fax www.aecom.com

> SUPPLEMENTAL SITE CHARACTERIZATION REPORT

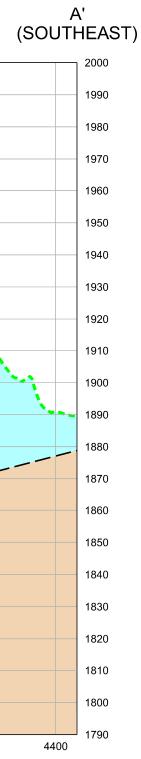
PROJECT NUMBER 60494667

RAWING NUMBER

2



GEOLOGIC CROSS SECTION A - A'





Leland Old Station Glenharold Mine Landfill Expansion

Basin Electric Power Cooperative 1717 E. Interstate Ave Bismarck, ND 58503-0564

ONSULTANT

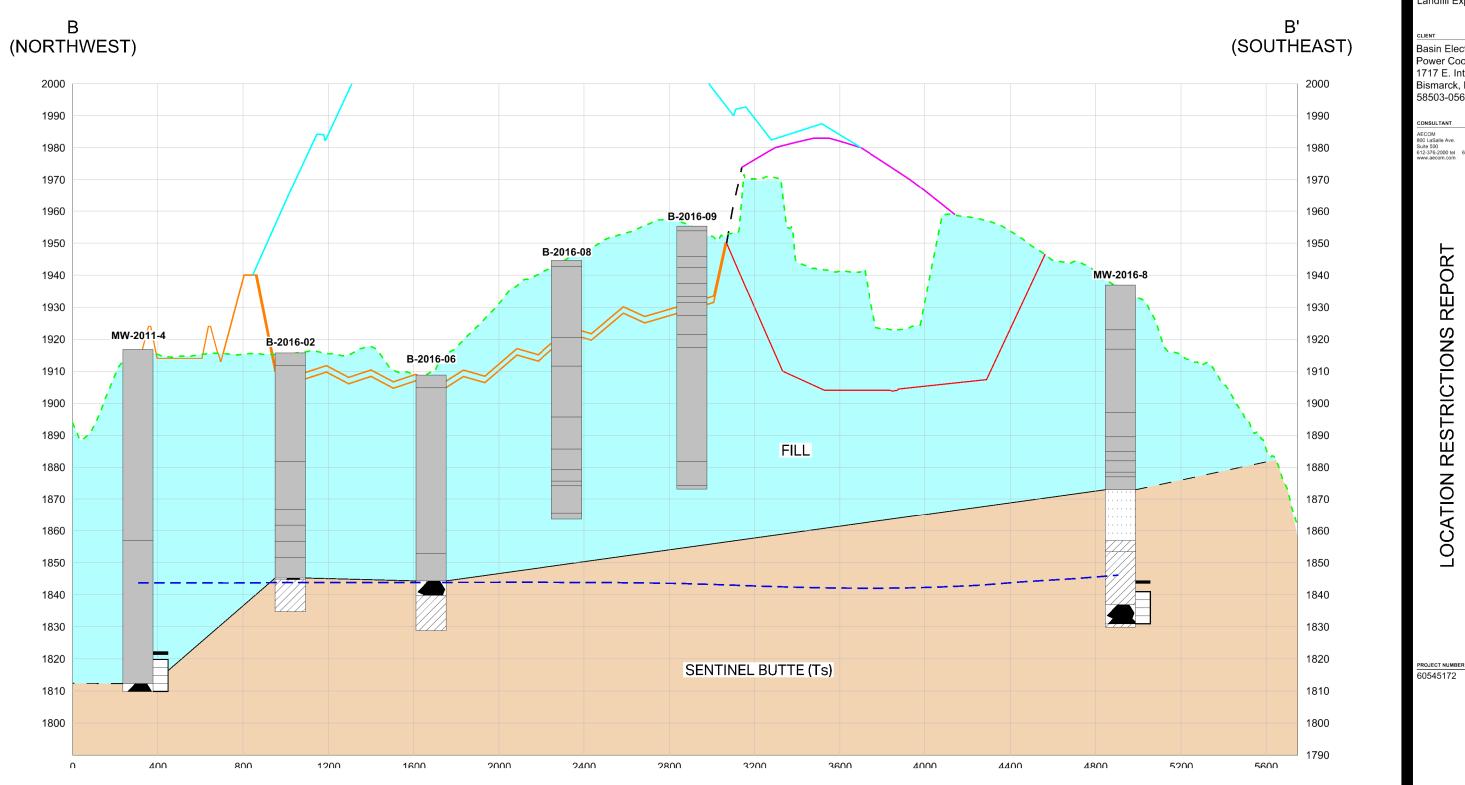
COM AECOM 300 LaSalle Ave. Suite 500 512-376-2000 tel 612-376-2271 fax www.aecom.com

SUPPLEMENTAL SITE CHARACTERIZATION REPORT

PROJECT NUMBER 494667

RAWING NUMBER

3



\$DATE\$

GEOLOGIC CROSS SECTION B - B'

AECOM

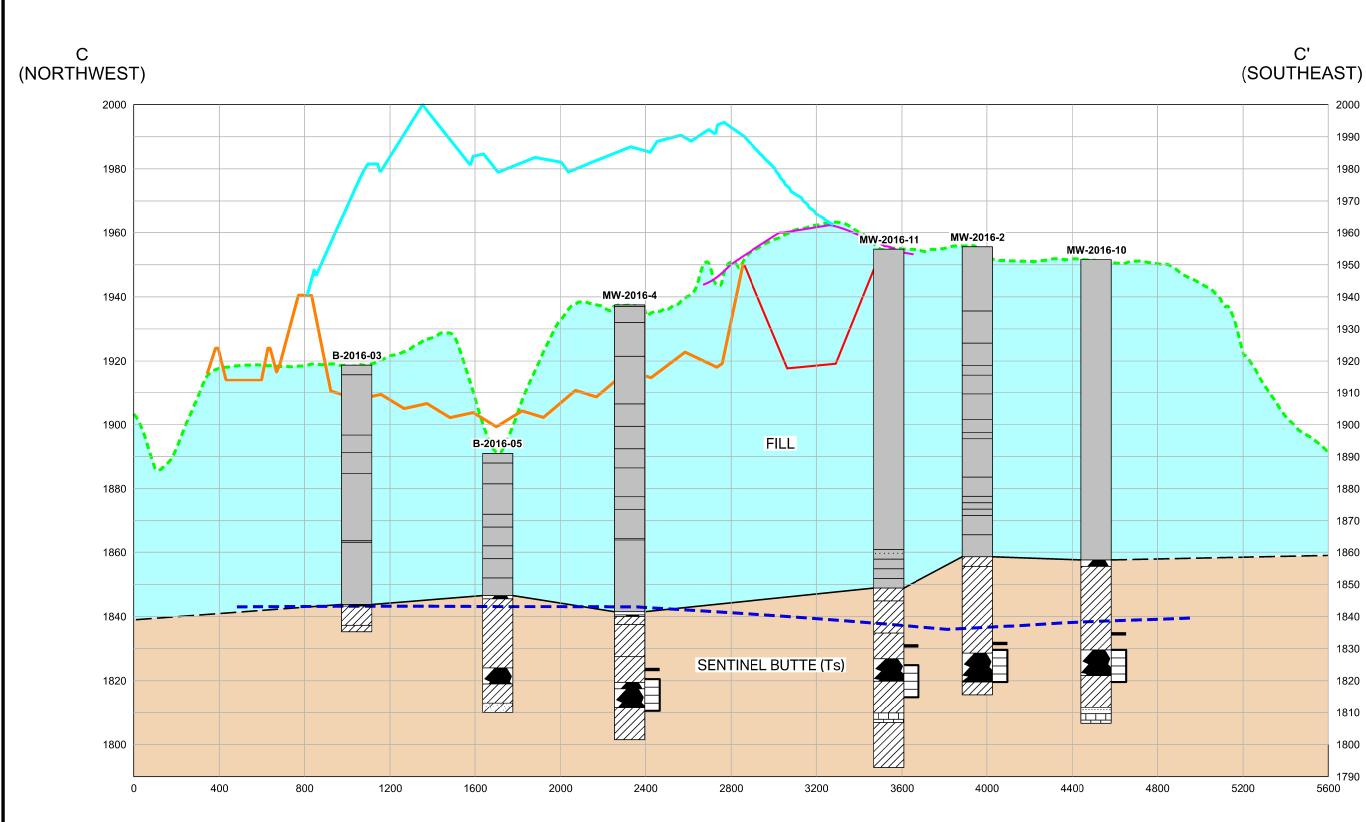
Leland Old Station Glenharold Mine Landfill Expansion

Basin Electric Power Cooperative 1717 E. Interstate Ave Bismarck, ND 58503-0564

AECOM 800 LaSalle Ave. Suite 500 612-376-2000 tel 612-376-2271 fax www.aecom.com

RAWING NUMBER

4



:lectric/60494667 LOS Ash LF Expa

GEOLOGIC CROSS SECTION C - C'

AECOM

Leland Old Station Glenharold Mine Landfill Expansion

CLIENT

Basin Electric Power Cooperative 1717 E. Interstate Ave Bismarck, ND 58503-0564

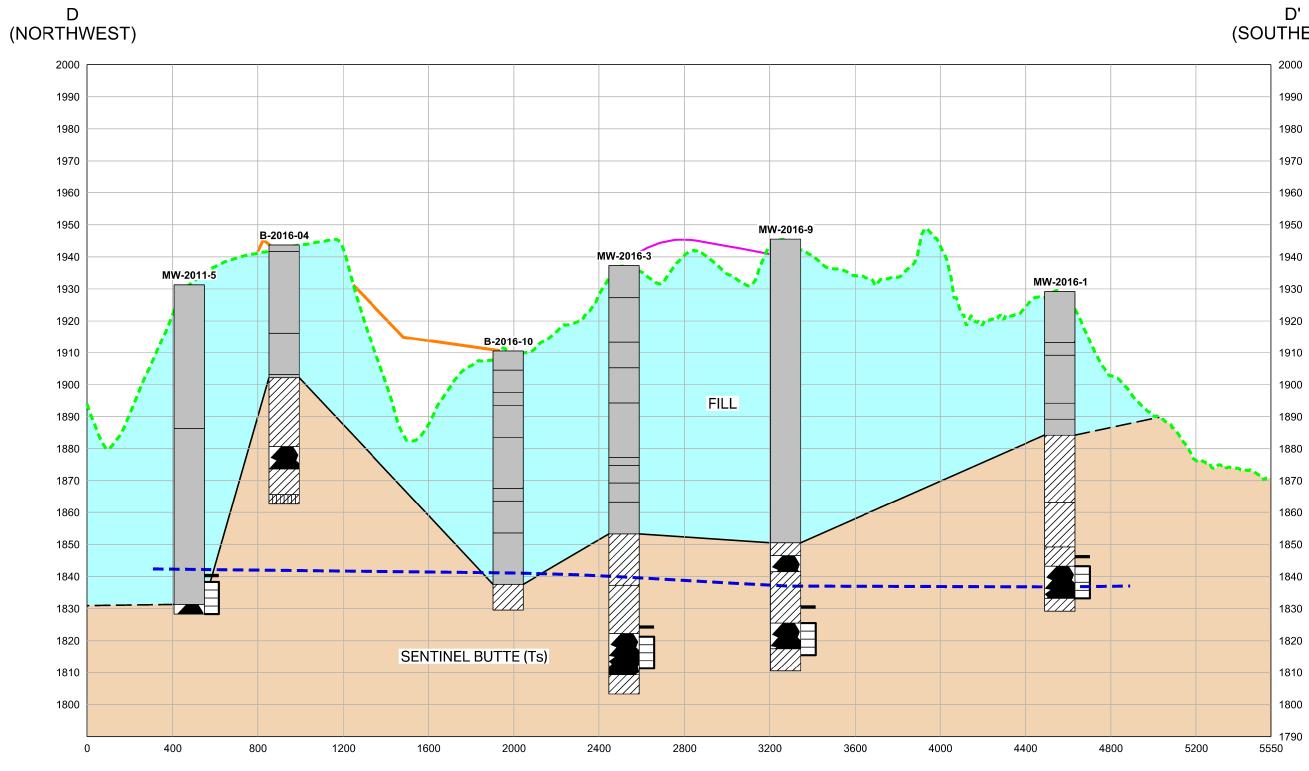
CONSULTANT AECOM 300 LaSalle Ave. Suite 500 512-376-2000 tel 612-376-2271 fax www.aecom.com

SUPPLEMENTAL SITE CHARACTERIZATION REPORT

PROJECT NUMBER

5

AWING NUMBER



GEOLOGIC CROSS SECTION D - D'

D' (SOUTHEAST)



AECOM

Leland Old Station Glenharold Mine Landfill Expansion

Basin Electric Power Cooperative 1717 E. Interstate Ave Bismarck, ND 58503-0564

LIEN

ONSULTANT AECOM 300 LaSalle Ave. Suite 500 512-376-2000 tel 612-376-2271 fax www.aecom.com

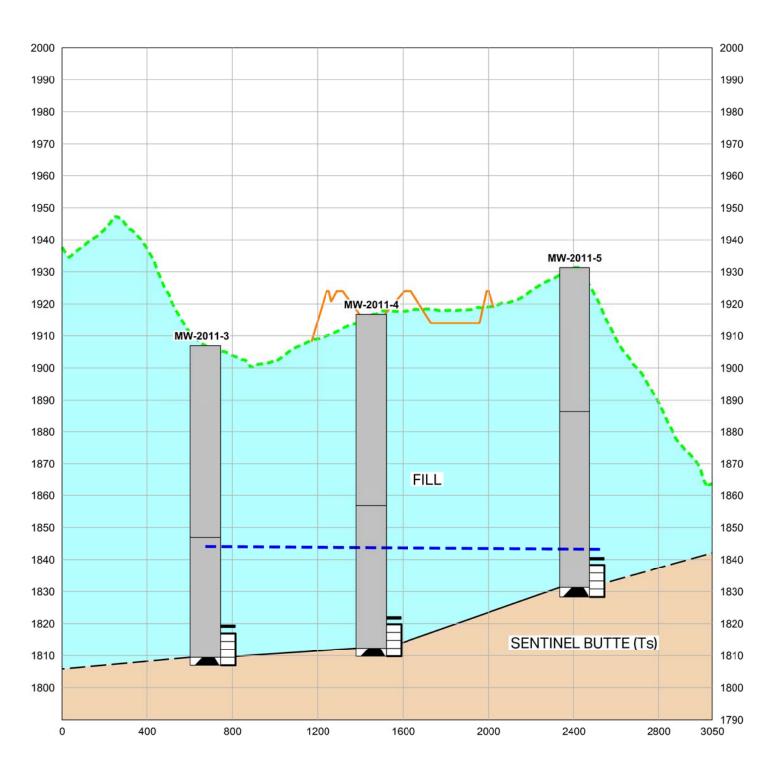
SUPPLEMENTAL SITE CHARACTERIZATION REPORT

PROJECT NUMBER 494667

6

AWING NUMBEI





SDATES FILENAM

E' (NORTHEAST)



Leland Old Station Glenharold Mine Landfill Expansion

CLIENT

Basin Electric Power Cooperative 1717 E. Interstate Ave Bismarck, ND 58503-0564

CONSULTANT

ECOM 300 LaSalle Ave. Suite 500 612-376-2000 tel 612-376-2271 fax www.aecom.com

LOCATION RESTRICTIONS REPORT

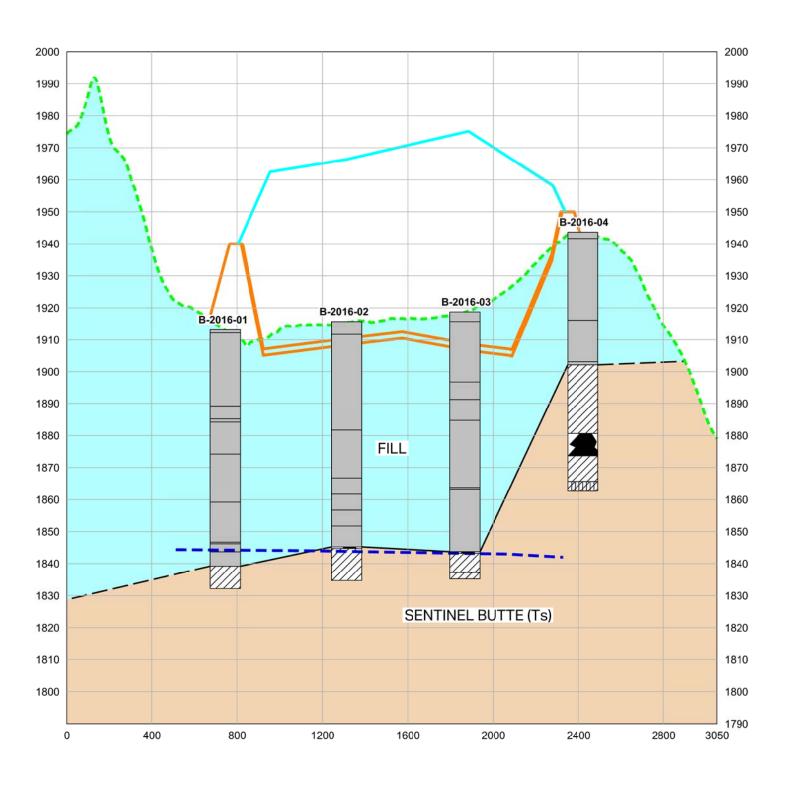
PROJECT NUMBER 60545172

GEOLOGIC CROSS SECTION E - E'

7

WING NUMBE

F (SOUTHWEST)



SDATES FILENAN

F' (NORTHEAST)



Leland Old Station Glenharold Mine Landfill Expansion

CLIENT

Basin Electric Power Cooperative 1717 E. Interstate Ave Bismarck, ND 58503-0564

CONSULTANT

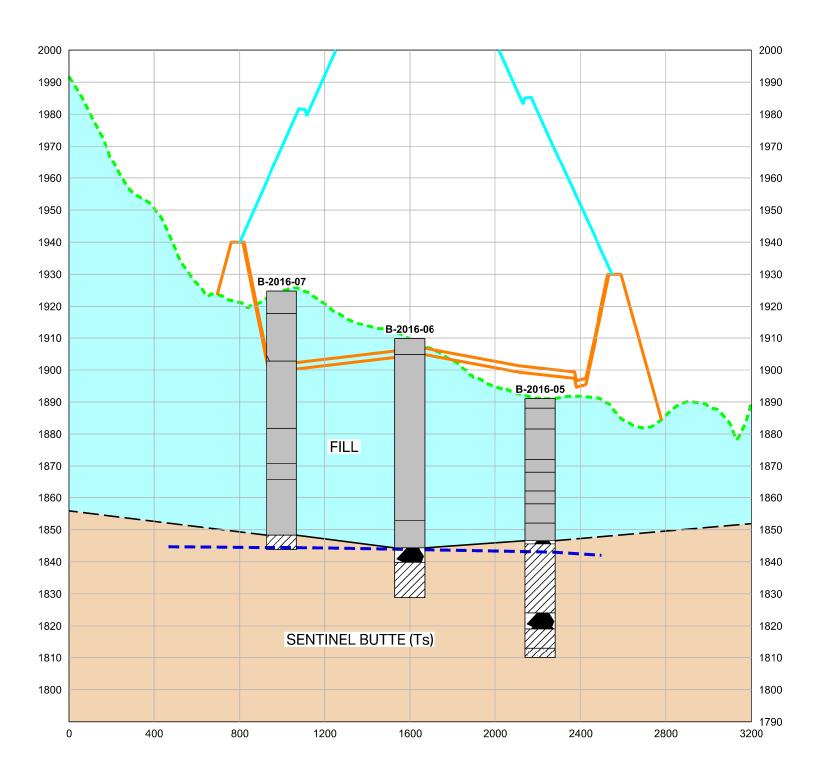
AECOM 000 LaSalle Ave. Suite 500 1312-376-2000 tel 612-376-2271 fax www.aecom.com

LOCATION RESTRICTIONS REPORT

PROJECT NUMBER 60545172

GEOLOGIC CROSS SECTION F - F' RAWING NUMBER

G (SOUTHWEST)



SDATES

G' (NORTHEAST)



Leland Old Station Glenharold Mine Landfill Expansion

CLIENT

Basin Electric Power Cooperative 1717 E. Interstate Ave Bismarck, ND 58503-0564

CONSULTANT AECOM 800 LaSalle Ave. Suite 500 612-376-2000 tel 612-376-2271 fax www.aecom.com

LOCATION RESTRICTIONS REPORT

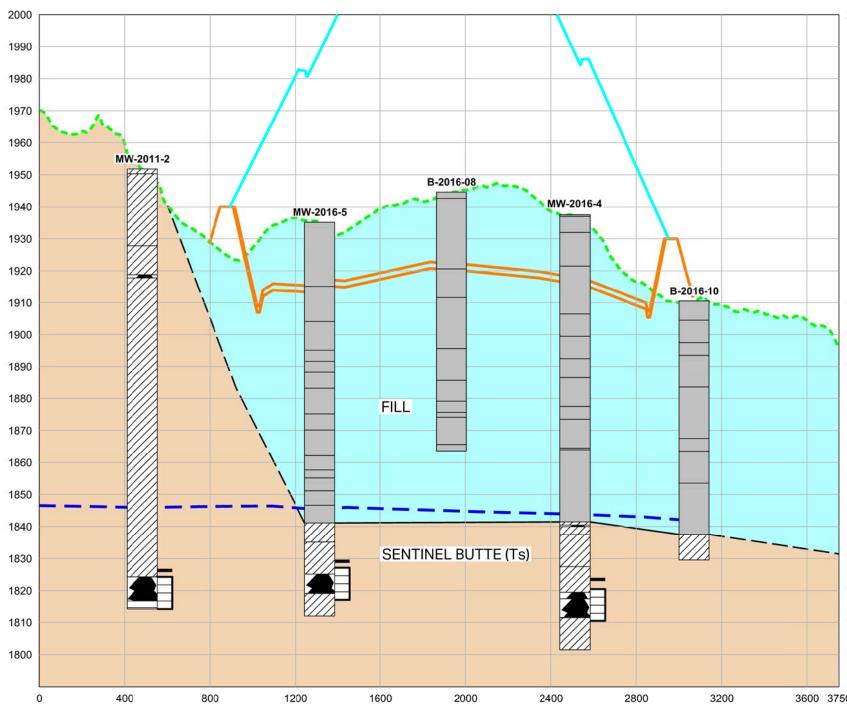
PROJECT NUMBER

GEOLOGIC CROSS SECTION G - G'

9

DRAWING NUMBER

H (SOUTHWEST)

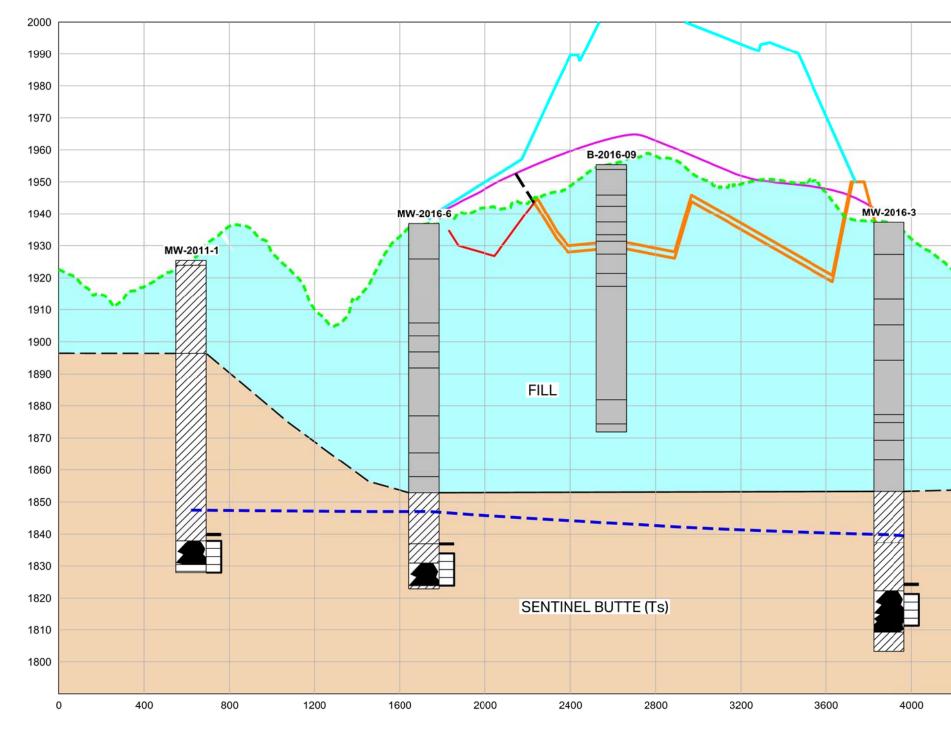


DATES

GEOLOGIC	CROSS
SECTION	

		PROJECT Leland Old Station Glenharold Mine Landfill Expansion
	H' (NORTHEAST)	CLIENT Basin Electric
2000		Power Cooperative 1717 E. Interstate Av Bismarck, ND
1990		58503-0564 consultant
1980		AECOM 800 LaSalle Ave. Sulte 500 612-376-2020 tel 612-376-2271 fax
1970		www.aecom.com
1960		
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1840		
1830		
1820		PROJECT NUMBER
1810		60545172
1800		
1790 50		
		DRAWING NUMBER





GEOLOGIC CROSS SECTION I - I'



DRAWING NUMBER

PROJECT NUMBER 60545172



l' (NORTHEAST)

CLIENT **Basin Electric**

COM

1717 E. Interstate Ave Bismarck, ND

Power Cooperative 58503-0564

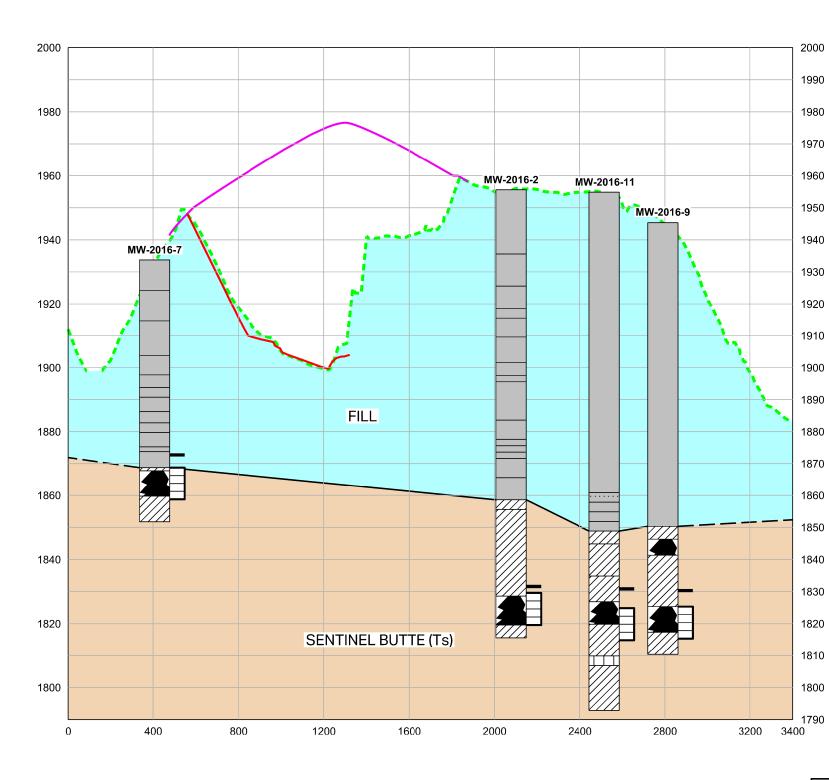
AECOM 800 LaSalle Ave. Suite 500 612-376-2000 tel 612-376-2271 fax www.aecom.com

LOCATION RESTRICTIONS REPORT

Leland Old Station Glenharold Mine Landfill Expansion

AECOM

J (SOUTH)



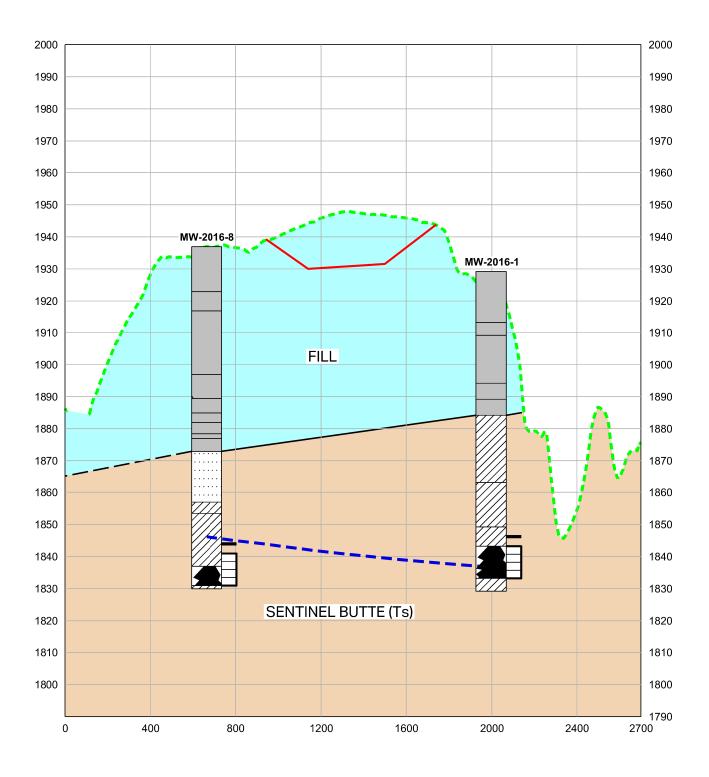
GEOLOGIC CROSS
SECTION J - J'

1	2

	Leland Old Station Glenharold Mine Landfill Expansion
J' (NORTHEAST)	CLIENT Basin Electric Power Cooperative 1717 E. Interstate Ave Bismarck, ND 58503-0564
	CONSULTANT AECOM 800 LaSalla Are. 500 (12:375-2000 tel 612:375-2000 tel www.aecom.com 612:376-2271 fax
	PROJECT NUMBER 60494667
	DRAWING NUMBER

AECOM

K (SOUTH)



K' (NORTHEAST)



Leland Old Station Glenharold Mine Landfill Expansion

CLIENT

Basin Electric Power Cooperative 1717 E. Interstate Ave Bismarck, ND 58503-0564

CONSULTANT

AECOM 300 LaSalle Ave. Suite 500 312-376-2000 tel 612-376-2271 fax www.aecom.com

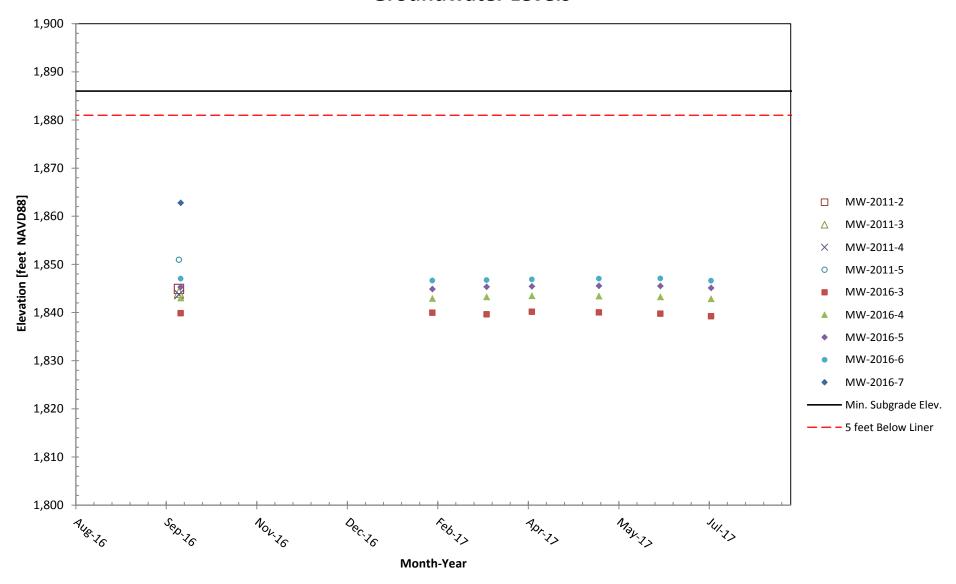
SUPPLEMENTAL SITE CHARACTERIZATION REPORT

PROJECT NUMBER

GEOLOGIC CROSS SECTION K - K' AWING NUMBER

Appendix E – Groundwater Data

LOS Ash Landfill Expansion Groundwater Levels



Groundwater Level Data Collected Since 2012

2011 Wells - Groundwater Data

Well ID	MW	/-2011-1	MW-2	2011-2	MW-2	2011-3	MW-2011-4		MW-2011-5	
Reference Elevation Top of Casing* (ft, NAVD88)	1928.39		1954.80		1910.09		1919.80		1934.26	
Date	DTW (feet)	GW Elev. (ft, NAVD88)	DTW (feet)	GW Elev. (ft, NAVD88)	DTW (feet)	GW Elev. (ft, NAVD88)	DTW (feet) GW Elev. (ft, NAVD88)		DTW (feet)	GW Elev. (ft, NAVD88)
2/21/2012	77.88	1850.51	106.23	1848.57	62.3	1847.79	72.33	1847.47	81.44	1852.82
4/17/2012	78.42	1849.97	106.94	1847.86	62.9	1847.19	73.99	1845.81	82.23	1852.03
7/31/2012	79.06	1849.33	107.7	1847.10	63.68	1846.41	73.78	1846.02	82.13	1852.13
10/8/2012	79.27	1849.12	108.06	1846.74	64.03	1846.06	74.15	1845.65	82.01	1852.25
1/9/2013	79.64	1848.75	108.44	1846.36	64.48	1845.61	74.58	1845.22	82.6	1851.66
5/6/2013	80.04	1848.35	108.75	1846.05	64.84	1845.25	74.97	1844.83	82.77	1851.49
7/29/2013	79.48	1848.91	108.25	1846.55	64.3	1845.79	74.42	1845.38	82.55	1851.71
10/7/2013	79.14	1849.25	107.95	1846.85	63.94	1846.15	74.01	1845.79	82.42	1851.84
5/12/2014	80.14	1848.25	108.69	1846.11	64.77	1845.32	74.85	1844.95	82.64	1851.62
9/22/2014	79.3	1849.09	108.17	1846.63	64.16	1845.93	74.2	1845.60	82.05	1852.21
4/13/2015	80.17	1848.22	109.4	1845.40	64.69	1845.40	74.72	1845.08	82.34	1851.92
9/27/2016	80.95	1847.44	109.89	1844.91	65.98	1844.11	76.05	1843.75	83.29	1850.97

2016 Wells - Groundwater Data

Well ID	MW	MW-2016-1		MW-2016-2		MW-2016-3		MW-2016-4		MW-2016-5		MW-2016-6	
Reference Elevation Top of Casing* (ft, NAVD88)	1931.73		1957.98		1939.88		1939.97		1937.54		1939.31		
Date	DTW (feet)	GW Elev. (ft, NAVD88)											
9/28/2016	94.97	1836.76	121.99	1835.99	100.04	1839.84	96.96	1843.01	92.24	1845.30	92.29	1847.02	
1/25/2017	NM	NM											
2/14/2017	95.59	1836.14	115.22	1842.76	99.92	1839.96	97.05	1842.92	92.65	1844.89	92.69	1846.62	
3/16/2017	93.04	1838.69	123.02	1834.96	100.27	1839.61	96.72	1843.25	92.20	1845.34	92.58	1846.73	
4/10/2017	92.94	1838.79	118.36	1839.62	99.73	1840.15	96.50	1843.47	92.10	1845.44	92.45	1846.86	
5/17/2017	92.55	1839.18	116.32	1841.66	99.85	1840.03	96.57	1843.40	91.99	1845.55	92.26	1847.05	
6/20/2017	92.70	1839.03	116.26	1841.72	100.13	1839.75	96.71	1843.26	92.03	1845.51	92.24	1847.07	
7/18/2017	93.20	1838.53	118.18	1839.80	100.66	1839.22	97.12	1842.85	92.44	1845.10	92.70	1846.61	

Well ID	MW	-2016-7	MW-2	2016-8	MW-2	2016-9	MW-2016-10		MW-2016-11	
Reference Elevation Top of Casing* (ft, NAVD88)	1936.11		1939.36		1947.39		195	3.32	1956.73	
Date	DTW (feet)	GW Elev. (ft, NAVD88)								
9/28/2016	73.31	1862.80	93.21	1846.15	NM	NM	NM	NM	NM	NM
1/25/2017	NM	NM	NM	NM	109.22	1838.17	112.1	1841.22	117.26	1839.47
2/14/2017	NM	NM	92.77	1846.59	116.77	1830.62	112.12	1841.20	124.68	1832.05
3/16/2017	NM	NM	92.66	1846.70	113.65	1833.74	111.60	1841.72	123.05	1833.68
4/10/2017	NM	NM	92.36	1847.00	113.57	1833.82	111.20	1842.12	122.60	1834.13
5/17/2017	NM	NM	92.62	1846.74	111.30	1836.09	111.56	1841.76	119.91	1836.82
6/20/2017	NM	NM	92.71	1846.65	113.43	1833.96	111.69	1841.63	121.12	1835.61
7/18/2017	NM	NM	92.97	1846.39	115.69	1831.70	112.03	1841.29	123.09	1833.64

NAVD = North American Vertical Datum of 1988 (NAVD 88)

NM = Not Measured (Well did not exist or no longer sampled)

DTW = Depth To Water

GW = Groundwater

Appendix F – Environmental and Wetland Delineation Report (Excerpt)

EXECUTIVE SUMMARY

Basin Electric Power Cooperative (BEPC) contracted AECOM to conduct wetland delineations within the ash landfill expansion (Project) near Stanton, North Dakota in Mercer County. The purpose of this report is to provide a summary of the available desktop data and wetland delineations conducted on August 19, 2016 and an evaluation of potential waters of the U.S. (WOTUS). A desktop analysis and literature search were also conducted to identify federally listed species of concern with the potential to occur within the proposed Project area.

One soil type was found within the Project area, mined land complex with 0 to 60 percent slopes (Figure 4-1). The mined land complex soils are not characterized as having hydric characteristics. Hydrology of the Project area is influenced by drainages and creeks contributing to the Missouri River, and the Project area is entirely within the Missouri River Basin. Historically, the dominant natural vegetation type of the Project area is shortgrass prairie (Dyke, S.R., S.K. Johnson, and P.T. Isakson. 2015. North Dakota State Wildlife Action Plan. North Dakota Game and Fish Department, Bismarck, ND). Found mostly in the Missouri Slope ecoregion of North Dakota, this vegetation type is dominated by warm season species that can survive on little rainfall (Figure 4-2).

A desktop analysis and literature search were conducted to identify federally listed species of concern with the potential to occur within the proposed Project area. Using the United States Fish and Wildlife Service's (USFWS's) Information for Planning and Conservation tool, AECOM identified seven threatened and endangered (T&E) species of concern and assigned each a determination of affect. North Dakota does not have a state endangered or threatened species list; only those species listed by the Endangered Species Act are considered threatened or endangered in North Dakota, and the USFWS has primary oversight over these species.

A no effect determination was given to the least tern (*Sterna antillarum*), piping plover (*Charadrius melodus*), red knot (*Calidris canutus rufa*), whooping crane (*Grus Americana*), pallid sturgeon (*Scaphirhynchus albus*), gray wolf (*Canis lupus*), and northern long-eared bat (*Myotis septentrionalis*). Additionally, no T&E species were observed during the field survey on August 19, 2016.

AECOM conducted a desktop evaluation of wetlands to determine potential United States Army Corps of Engineers (USACE) jurisdictional waters. Potential impacts to WOTUS are subject to USACE permitting under Section 404 of the Clean Water Act. The Project area lies entirely within the Omaha District of the USACE. The Project area evaluated by AECOM contains two mapped National Wetlands Inventory (NWI) features and one National Hydrography Dataset (NHD) tributary (Figure 4-3). The two NWI features did not meet wetland criteria in the field. The NHD-mapped creek appeared to be an upland drainage that flowed into Alderin Creek. This drainageway did not contain hydrophytic vegetation or an ordinary high water mark.

Four wetlands were delineated within the Project area (Figures 4-4, 4-5 and 4-6). AECOM has evaluated the characteristics of Wetland-1, Wetland-2, Wetland-3, and Wetland-4 and has come to the conclusion that these wetlands appear to be non-relatively permanent waters (non-RPW) that are formed by geomorphic position, are isolated from jurisdictional waters, and appear to be without significant nexus. Wetlands-1-3 formed following the mineland reclamation when soils settled forming small basins. Wetland-4 is a depressional wetland formed within a ditch created during the construction of the adjacent road.

However, these are the recommendations of AECOM based on our experience, observations and data collected in the field, and best professional judgement. The final authority over wetland jurisdiction is the responsibility of the USACE. AECOM recommends that an official jurisdictional determination (JD) is obtained from the USACE for the wetlands and drainageway in question.

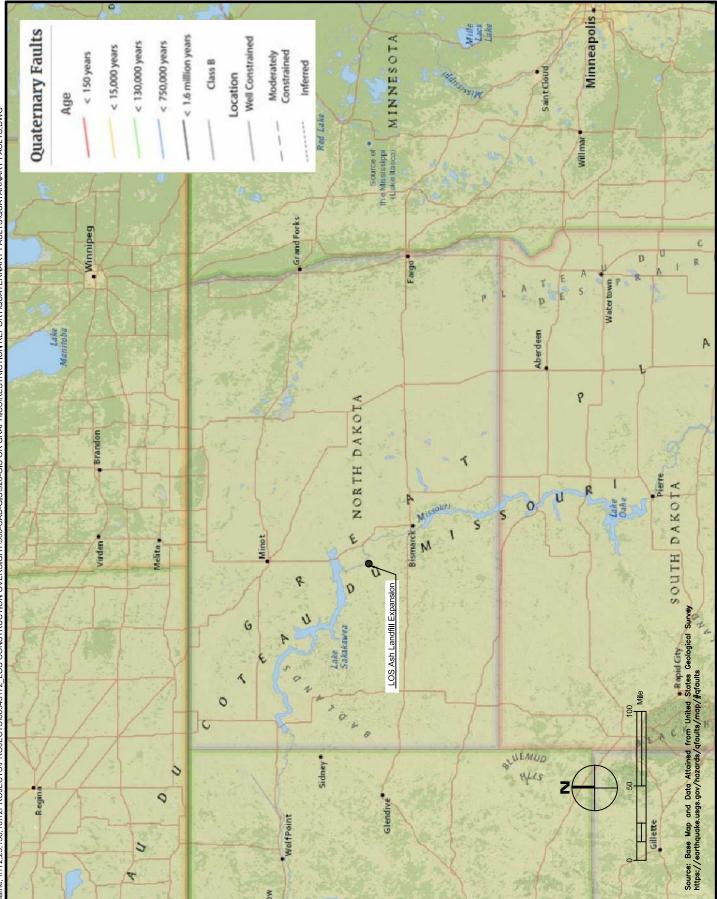
STATEMENT OF LIMITATIONS

This report was prepared by the staff of AECOM under the supervision of experienced professionals. The data interpretation, conclusions, and recommendations presented in the report were governed by AECOM's experience and professional judgment. This report has been prepared based on data current at

the time of preparation. Assumptions based on this data, although believed reasonable and appropriate based on the data provided herein, may not prove to be true in the future as new data are collected. The conclusions and recommendations of AECOM are conditioned upon these assumptions.

Appendix G – Geologic Maps

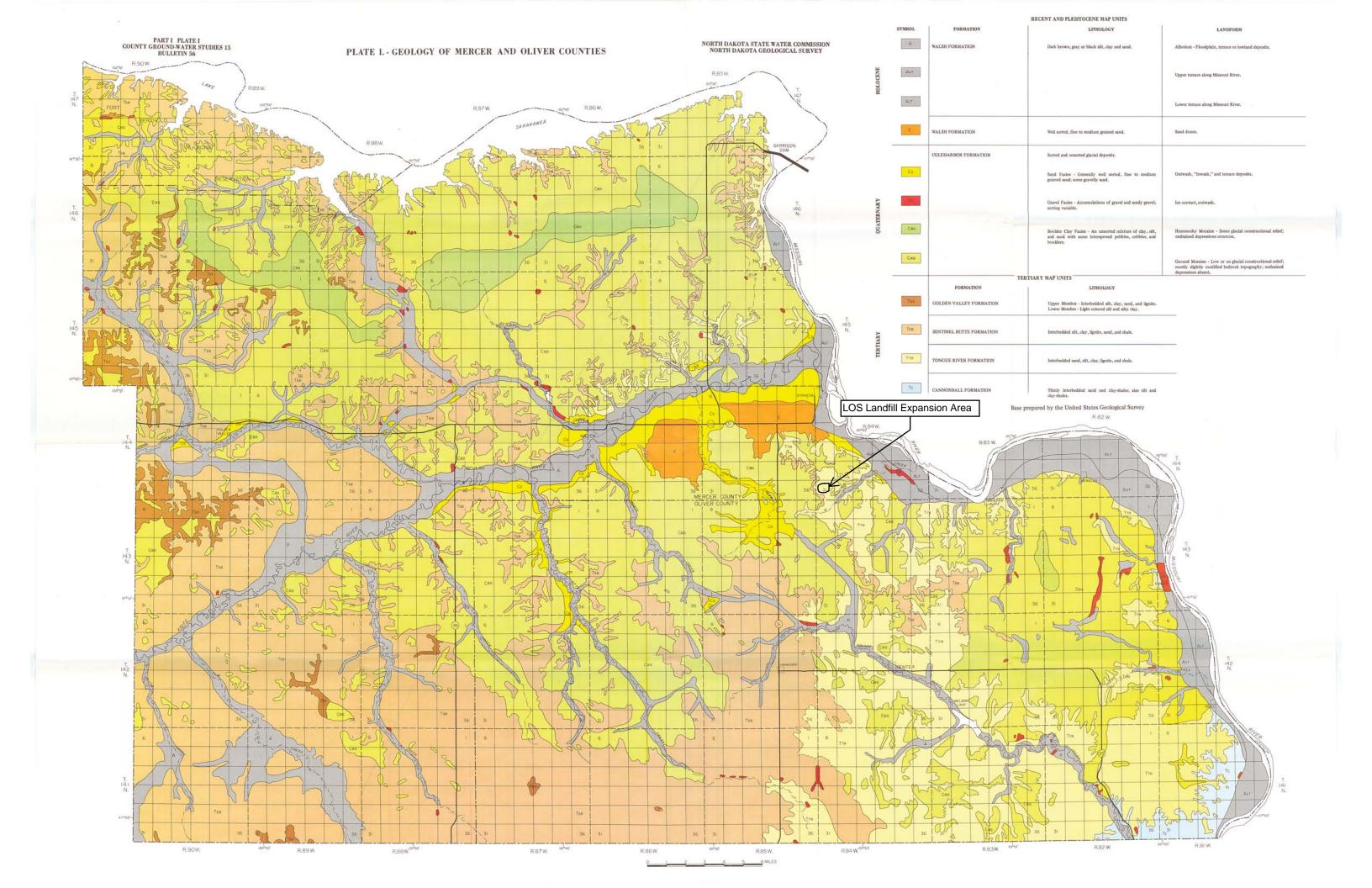
Last saved by: BLOECHERM(2017-11-02) Last Plotted: 2017-11-02 Filename: \\172.25.156.10\12PROJECTS\PROJECTS\60545172_LOS CONSTRUCTION OVERSIGHT\900-CAD-GIS\920-GIS OR GRAPHICS\RESTRICTION REPORT\QUATERNARY FAULTS\QUATARNARY FAULTS.DWG

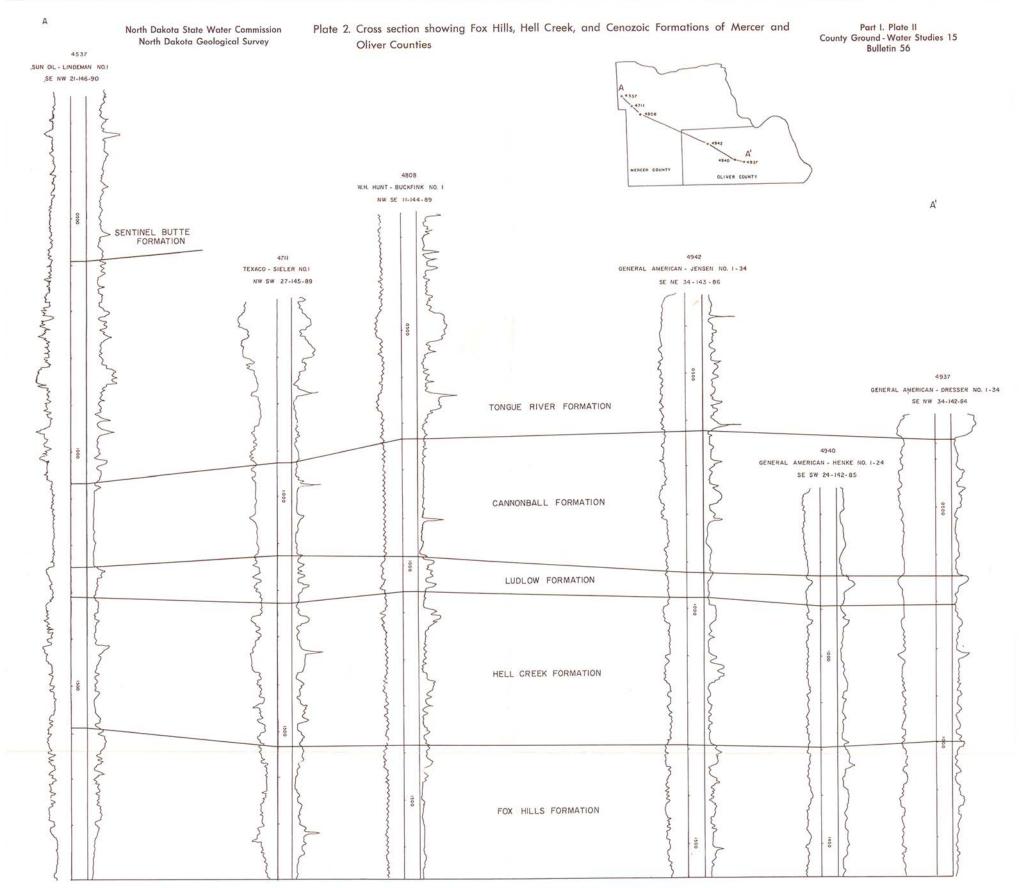


Location Restrictions Report LOS Ash Landfill Expansion Basin Electric Power Cooperative Project No.: 60545172 2017-03-14

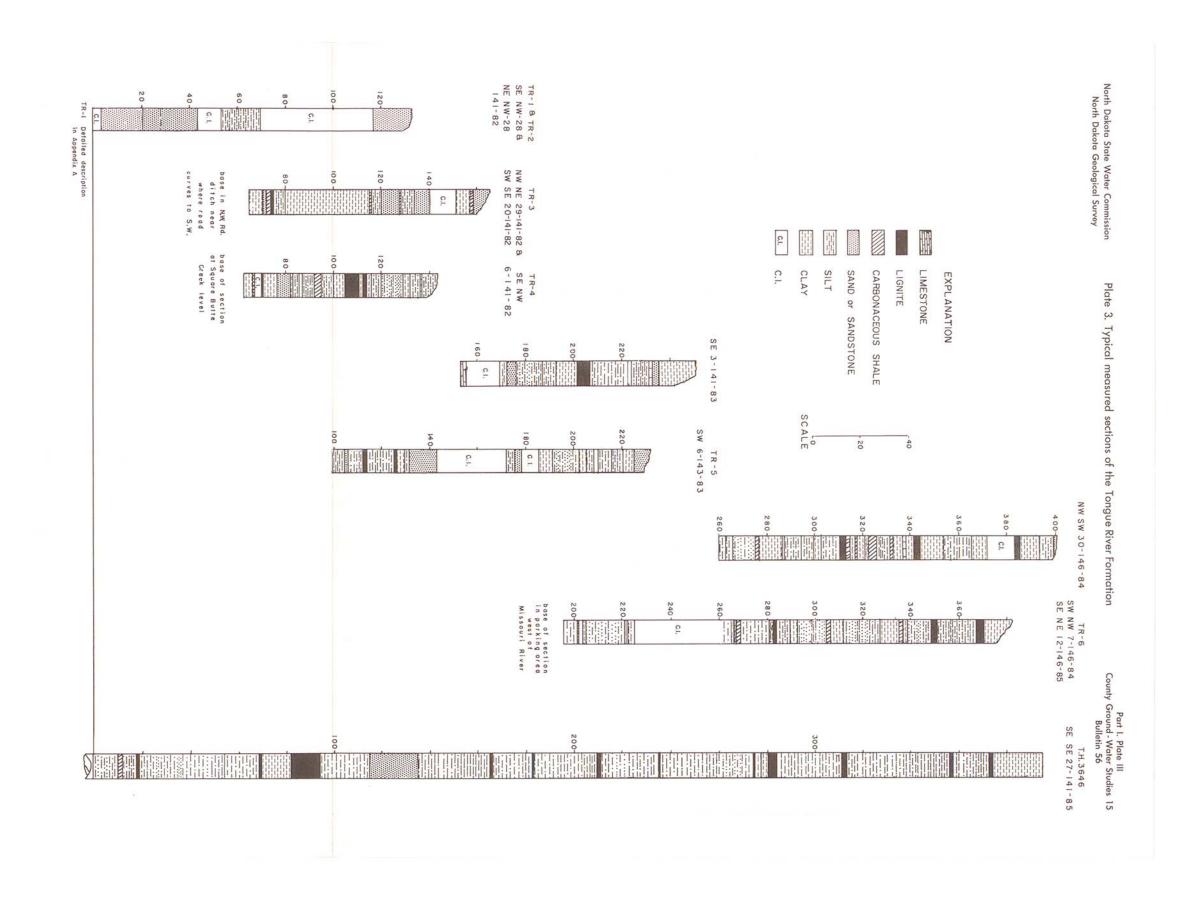
Quaternary Faults in Proximity to Leland Olds Station Mercer County, North Dakota

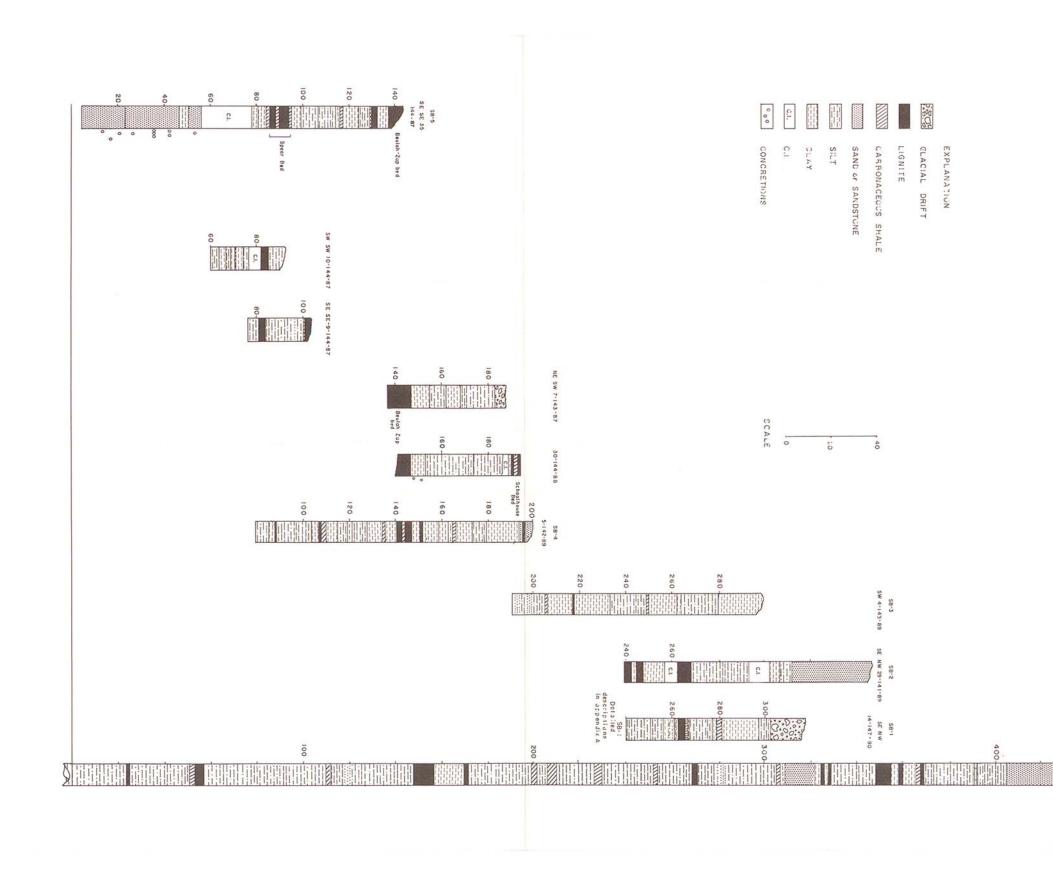






Top of Pierre Formation





North Dakota State Water Commission North Dakota Geological Survey

Plate 4. Typical measured sections of the Sentinel Butte Formation

Part I. Plate IV County Ground - Water Studies 15 Bulletin 56 Trk 3375 58 SW 20-14C-90