



# CCR Groundwater Monitoring System Report, Revision 1

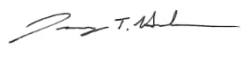


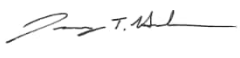
Laramie River Station  
Wheatland, Wyoming

Basin Electric Power Cooperative

Project number: 60506860

January 16, 2025

### Quality information

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Revision	Revision date	Details	Authorized	Name	Position
Revision 1	1/16/2025	Updated well Network		Jeremy Hurshman	Project Manager

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## List of Acronyms

AECOM	AECOM Technical Services, Inc.
ANOVA	analysis of variance
Basin	Basin Electric Power Cooperative
bgs	below ground surface
CCR	Coal Combustion Residuals
CFR	Code of Federal Regulations
EPA	United States Environmental Protection Agency
FGD	Flue Gas Desulfurization
ft	feet
ft/d	feet per day
ID	internal diameter
LRS	Laramie River Station
MW	megawatt
PVC	polyvinyl chloride
RCRA	Resource Conservation and Recovery Act
SSI	statistically significant increase
SU	standard units
U.S.	United States
USGS	U.S. Geological Survey

## Monitoring System Certification

### Basin Electric Power Cooperative Laramie River Station CCR units: Ash Pond 1, Ash Pond 2, Ash Pond 3, Ash Landfill, Emergency Holding Ponds

AECOM Technical Services, Inc. ("Consultant") was retained by Basin Electric Power Cooperative to prepare the attached documentation of the updated groundwater monitoring systems for the above-referenced coal combustion residuals ("CCR") surface impoundments and landfill, and to certify whether they meet the design and construction requirements set out in the CCR Rule under 40 Code of Federal Regulations (CFR) § 257.91. Some of the systems have been modified since the original certification dated October 17, 2017 to account for the results of groundwater monitoring and corrective action at the Site. This current certification applies to the systems as they exist as of December 31, 2024.

## Background

Pursuant to 40 CFR § 257.90(b), owners and operators of new and existing CCR landfills, and new and existing CCR surface impoundments, and all lateral expansions of a CCR unit must install a groundwater monitoring system, compliant with 40 CFR § 257.91, which requires that said system consist of a sufficient number of wells, installed at appropriate locations and depths, to yield groundwater samples from the uppermost aquifer that accurately represent the quality of background groundwater that has not been affected by leakage from the CCR unit and accurately represent the quality of groundwater passing the waste boundary of the CCR unit.

Pursuant to 40 CFR § 257.91(f), the owner or operator must obtain a certification from a qualified professional engineer stating that the groundwater monitoring system has been designed and constructed to meet the requirements of 40 CFR § 257.91, including the performance standards specified in 40 CFR § 257.91(a), based on the site-specific information specified in 40 CFR § 257.91(b). If the groundwater monitoring system includes only the minimum number of monitoring wells specified in 40 CFR § 257.91(c)(1), the certification must document the basis supporting this determination. In support of Consultant's assessment, Consultant completed an evaluation of the groundwater monitoring system for the above-referenced CCR units and determined that sufficient information is available to make the certification required under 40 CFR § 257.91(f).

## Limitations

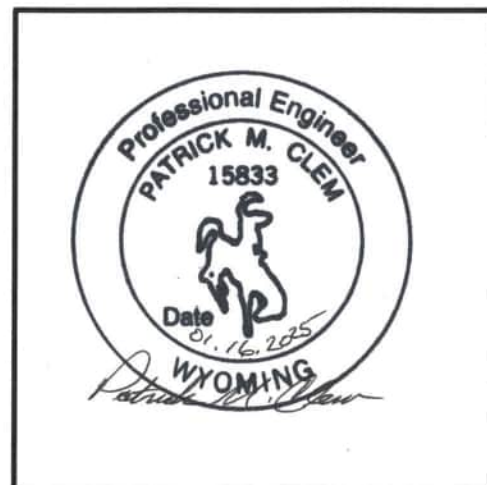
The signature of Consultant's authorized representative on this document represents that to the best of Consultant's knowledge, information, and belief in the exercise of its professional judgment, it is Consultant's professional opinion that the aforementioned information is accurate as of the date of such signature. Any opinion or decisions by Consultant are made on the basis of Consultant's experience, qualifications, and professional judgment and are not to be construed as warranties or guaranties. In addition, opinions relating to environmental, geologic, and geotechnical conditions or other estimates are based on available data, and actual conditions may vary from those encountered at the times and locations where data are obtained, despite the use of due care.

## Certification

I, Patrick Clem, being a Registered Professional Engineer in the State of Wyoming, certify to the best of my knowledge, information, and belief, that the groundwater monitoring system for the CCR units that are the subject of this certification has been designed and constructed to meet the requirements of 40 CFR § 257.91, and that this certification is true and correct and has been prepared in accordance with generally accepted good engineering practices.

SIGNATURE: Patrick M. Clem

DATE: 01.16.2025



## Statistical Method Certification

### Basin Electric Power Cooperative Laramie River Station CCR units: Ash Pond 1, Ash Pond 2, Ash Pond 3, Ash Landfill, Emergency Holding Ponds

AECOM Technical Services, Inc. ("Consultant") was retained by Basin Electric Power Cooperative to prepare the attached documentation of the groundwater monitoring systems for the above-referenced coal combustion residuals ("CCR") surface impoundments and landfill, and to certify the appropriate statistical methods for evaluation of the monitoring systems data. Some of the groundwater monitoring systems have been modified and significant groundwater monitoring data have been generated and evaluated since the original certification dated October 17, 2017. Accordingly, the statistical methods were re-evaluated to account for the results of these modifications and monitoring. This current certification applies to the statistical methods selected for use as of December 31, 2024.

## Background

Pursuant to 40 Code of Federal Regulations (CFR) § 257.90(b), owners and operators of new and existing CCR landfills, and new and existing CCR surface impoundments, and all lateral expansions of a CCR unit must install a groundwater monitoring system, compliant with 40 CFR § 257.91, which requires that said system consist of a sufficient number of wells, installed at appropriate locations and depths, to yield groundwater samples from the uppermost aquifer that accurately represent the quality of background groundwater that has not been affected by leakage from the CCR unit and accurately represent the quality of groundwater passing the waste boundary of the CCR unit.

Pursuant to 40 CFR § 257.93(f), the owner or operator of the CCR unit must select one of the statistical methods specified in paragraphs (f)(1) through (5) of this section to be used in evaluating groundwater monitoring data for each specified constituent. The statistical test chosen shall be conducted separately for each constituent in each monitoring well, and shall comply with the performance standards specified in 40 C.F.R. § 257.93(g). Per 40 CFR § 257.93(f)(6), the owner or operator must obtain a certification from a qualified professional engineer stating that the statistical method for the evaluation of groundwater monitoring data for the groundwater monitoring system meets the requirements of 40 CFR § 257.93(f)(6), including the performance standards specified in 40 CFR § 257.91(a), based on the site-specific information specified in 40 CFR § 257.91(b). In support of Consultant's assessment, Consultant completed an evaluation of the groundwater monitoring system for the above-referenced CCR units and determined that sufficient information is available to make the certification required under 40 CFR § 257.93(f).

## Limitations

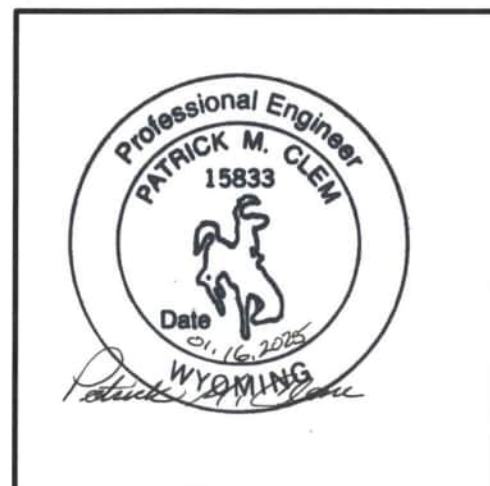
The signature of Consultant's authorized representative on this document represents that to the best of Consultant's knowledge, information, and belief in the exercise of its professional judgment, it is Consultant's professional opinion that the aforementioned information is accurate as of the date of such signature. Any opinion or decisions by Consultant are made on the basis of Consultant's experience, qualifications, and professional judgment and are not to be construed as warranties or guaranties. In addition, opinions relating to environmental, geologic, and geotechnical conditions or other estimates are based on available data, and actual conditions may vary from those encountered at the times and locations where data are obtained, despite the use of due care.

## Certification

I, Patrick Clem, being a Registered Professional Engineer in the State of Wyoming, certify to the best of my knowledge, information, and belief, that the statistical methods selected to evaluate groundwater monitoring data for the CCR units that are the subject of this certification, as identified in **Table 6-1** of this report, are appropriate and comply with the performance standards specified in 40 CFR § 257.93(g), and that this certification is true and correct and has been prepared in accordance with generally accepted good engineering practices.

SIGNATURE: Patrick M. Clem

DATE: 01.16.2025





# 1. Introduction

On behalf of Basin Electric Power Cooperative (Basin), AECOM Technical Services, Inc. (AECOM) prepared this revised report documenting the Coal Combustion Residuals (CCR) groundwater monitoring systems for the CCR units at Basin's Laramie River Station (LRS) located east of Wheatland, Wyoming (see **Figure 1-1**). This report addresses the requirement under Chapter 40 Code of Federal Regulations (CFR) Part 257.105(h) to provide in the Operating Record, as it becomes available, "documentation of the design, installation, development, and decommissioning of any monitoring wells, piezometers and other measurement, sampling, and analytical devices."

Pursuant to 40 CFR § 257.90(b)(1), by October 17, 2017, an owner and operator of a CCR unit must install a groundwater monitoring system that meets the requirements of 40 CFR § 257.91. The groundwater monitoring system must meet the CCR Rule's performance standard, which requires the system to consist of a sufficient number of wells, installed at appropriate locations and depths, to yield groundwater samples from the uppermost aquifer that accurately represent the quality of:

1. Background groundwater that has not been affected by leakage from a CCR unit; and
2. Groundwater passing the waste boundary of the CCR unit—the downgradient monitoring system must be installed at the waste boundary that ensures detection of potential groundwater contamination in the uppermost aquifer and must monitor all potential contaminant pathways.

This report summarizes the procedures and field activities associated with drilling and installation of monitoring wells that comprise the CCR monitoring networks at LRS, as well as the results of testing and monitoring of wells to evaluate the network against the requirements of the Final Rule.

This report is organized as follows:

- Section 1 includes a brief introduction to this report;
- Section 2 provides a brief background with historical information concerning LRS and associated CCR units;
- Section 3 describes the geological and hydrogeological setting of LRS;
- Section 4 describes selection and installation of the CCR monitoring well networks for all CCR units at LRS, including the drilling and installation of monitoring wells to supplement existing monitoring wells at LRS;
- Section 5 presents an evaluation of the LRS CCR monitoring compared to the requirements of the CCR Rule;
- Section 6 describes the statistical methodology that will be used to evaluate CCR groundwater monitoring data;
- Section 7 describes the professional limitations that apply to this report; and
- Section 8 lists the references cited in this report.

Certifications pertaining to the design and construction of the groundwater monitoring system and selection of the statistical method for evaluating data acquired using the groundwater monitoring system, are presented before **Section 1**.

## 2. Background

The LRS is one of the largest consumer-operated, regional, joint power supply ventures in the United States (U.S.). LRS is a coal-based generating station located in Platte County east of Wheatland, Wyoming, and has a total power output capacity of 1,710 megawatts (MW) from three coal-based units:

- Unit 1, with a rating of 570 MW, which began operating in 1980;
- Unit 2, with a rating of 570 net MW, which began operating in 1981; and
- Unit 3, with a rating of 570 net MW, which began operating in 1982.

Coal ash is disposed at LRS in the following CCR units:

- Ash Landfill
- Ash Pond 1
- Ash Pond 2
- Ash Pond 3
- Emergency Storage Ponds

The three ash ponds and the landfill are located west of the generating units and office complex, near the western edge of the Site. The two emergency holding ponds are located north of the generating units in the northeastern part of the Site. The landfill and ash ponds were permitted in 1978 and began receiving coal ash in 1980. The emergency holding ponds were subsequently incorporated due to disposal of flue gas desulfurization (FGD) materials. Basin Electric reported that in 2014 the landfill received 284,119 tons of solid waste, including fly ash, FGD waste, and a minor contribution of solid debris. The landfill is currently accessed via a haul road running generally east to west along the south side of the landfill.

Due to the presence of CCR, the LRS ash ponds, landfill, and emergency holding ponds are regulated by the CCR Rule, promulgated by the U.S. Environmental Protection Agency (EPA) under Chapter 40 CFR Part 257, Subtitle D of the Resource Conservation and Recovery Act (RCRA). The CCR Rule establishes requirements for existing CCR landfills and surface impoundments, including groundwater monitoring and corrective action. The groundwater monitoring provisions of the CCR Rule require the installation of a system of monitoring wells, the specification of procedures for sampling these wells, and analysis of the resulting data to detect the presence of hazardous constituents. A corrective action process is required in the event that hazardous constituents are detected above background concentrations at levels exceeding groundwater protection standards.

### 3. Geological and Hydrogeological Setting

The geological and hydrogeological setting is important to understanding the groundwater environment in the vicinity of the LRS. The geologic history of Platte County is similar to most areas within the Front Range of the Rocky Mountains. Platte County is underlain by marine and continental deposits of limestone, conglomerate, sandstone, siltstone, shale, and unconsolidated sediments. Deposits range in thickness over the Laramie Range, Hartville uplift, and related features up to 10,000 feet (ft) in the east central and southeastern parts of the county. Precambrian rocks generally make up the mountainous (structurally complex) areas, Paleozoic and Mesozoic rocks adjoin the older formations, and Tertiary and Quaternary rocks underlie most of the county east of the Laramie Range (U.S. Geological Survey [USGS] 1960). The Laramide Orogeny was active in the county approximately 70 million years ago marking the beginning the Hartville uplift and Laramie Range. In the Cenozoic, streams eroded the eastern side of the range depositing silts, sands, and gravels of the Brule and Arikaree Formations that underlie the Wheatland area and subsequently Basin Electric LRS.

Precipitation landing on the eastern flank of the Laramie Range supplies surface water to perennial and ephemeral streams that flow east towards the basin. Most surface water west of Wheatland eventually joins with the Laramie River continuing east before discharging into the Platte River near Fort Laramie. Groundwater near Wheatland is recharged primarily through infiltration on the eastern flank of the Laramie Range, and through re-infiltration of irrigation water during the spring, summer, and fall months. Some groundwater in the saturated zones eventually returns to the land surface through seeps and springs, or is discharged by wells and evapotranspiration; however, the majority flows into surface streams. Alluvial drainages bounding the eastern (Wheatland Creek) and western portions (Chugwater Creek) of the facility transport surface water generally northward, discharging to the Laramie River (USGS 1960). Some groundwater within these regions percolates into the Arikaree Formation which holds the uppermost aquifer beneath the facility.

The LRS facility is underlain by a 5- to 30-ft section of Quaternary sediments that overlies the Arikaree Formation. The Arikaree Formation is comprised primarily of loosely- to moderately-cemented very fine- to fine-grained sandstone containing interbeds of silts and clays. A lower unit consists of lenses of loosely to well-cemented red to gray coarse sandstone interbedded with lenses of well-cemented conglomerate. A basal conglomerate lies unconformably upon the underlying Brule Formation in many places throughout Platte County (USGS 1960). The 2016 AECOM drilling investigation did not penetrate to depths great enough to expose the lower portions of the Arikaree; however, a review of the geologic logs generated during the drilling of the on-Site water supply well (Forell-Baumgardner No. 2) suggests the Brule Formation is approximately 820 ft below ground surface (bgs) in the western portions of the Site. Based on this information, the local thickness of the Arikaree Formation on-Site is approximately 790 ft thick.

The lithologic characteristics of the Arikaree Formation beneath the LRS are generally consistent, although there are slight differences in the degree of cementation and induration, and minor variations in grain size. Few fractures were noted in borehole soil cores obtained during monitoring well network installation described in **Section 4**. Interbeds with higher silt and clay content, coupled with greater cementation generate thin discontinuous perched groundwater horizons that are interpreted to hold only seasonal groundwater. The perched groundwater would tend to percolate downward to what is interpreted as the uppermost aquifer based on data obtained during monitoring well installation and aquifer testing. The uppermost aquifer is present at a depth of approximately 95 ft bgs in the southeastern portion of the LRS facility, and slopes generally north towards the Laramie River. The hydraulic gradient for the uppermost aquifer beneath the Site appears to be controlled dominantly through topographic features and enhanced infiltration zones in permeable shallow alluvium.

## 4. Monitoring Well System Selection and Installation

Monitoring well systems have been established at LRS to comply with the requirements of the EPA CCR Rule published in the Federal Register on April 17, 2015. The systems are comprised of several existing monitoring wells that predate the CCR Rule, as well as a number of additional monitoring wells that were installed to complete the systems and fully comply with requirements of the Rule.

### 4.1 Monitoring Well Installation in 2016

Sixteen monitoring wells were installed at LRS during the summer of 2016 to target the uppermost aquifer in the vicinity of the LRS CCR units, including nine monitoring wells (MW-32B through MW-40B) around the landfill and ash ponds west of the main plant area, and seven monitoring wells (MW-41B through MW-47B) surrounding the emergency holding ponds generally north of the main plant area (**Figure 4-1**). The monitoring well locations were selected to evaluate the direction of groundwater flow in the vicinity of the LRS CCR units.

Monitoring well installation involved drilling, well construction, development, and aquifer testing is described below.

### 4.2 Drilling and Well Construction

Subsurface utilities in the vicinity of each planned monitoring well installation location were identified by utility representatives following the One-Call of Wyoming notification system. The uppermost 5 ft of each boring location was excavated using hydro-excavation or hand-auger as an additional precaution against utility strikes.

Monitoring well drilling and construction occurred between July 13 and August 12, 2016. The monitoring wells were installed using sonic drilling methods. Soil cores recovered during drilling operations were photographed and logged by AECOM geologists. Boring logs are included in **Appendix A**. Each boring was drilled 10 to 15 ft below the elevation at which groundwater was encountered. Moist to wet horizons were encountered at multiple depths during drilling. A submersible pump was used to test these zones for water production. If water was not recharging within the test interval, the borehole was advanced deeper until a distinct groundwater horizon was reached, or pump testing yielded significant quantities of groundwater.

Each new monitoring well was constructed of 2-inch-diameter, schedule 40 polyvinyl chloride (PVC) riser pipe and slotted screen. The screen interval was constructed using 20 ft of 0.010-inch factory-slotted PVC screen straddling the water table or groundwater production zone. The annular space within the borehole around the screen was filled with clean 10/20 silica sand filter pack to a minimum of 2 ft above top of screen. Bentonite chips were placed above the filter pack and hydrated with potable water to seal the filter pack from surface influence. The remaining annular space above the bentonite seal was filled with Portland Type I/II grout and allowed to set for a minimum of 24 hours before well development activities were completed. Above-grade stainless steel monuments, lockable J-Plugs, and monument locks were installed to protect and secure the wellhead. Surface monuments were labeled with the well identification number and set within a 2-foot square concrete pad. Steel bollards painted yellow were installed around wells located near traffic areas to enhance visibility and protect the wells. Well construction diagrams are included in **Appendix A**, and construction details are summarized in **Table 4-1**.

### 4.3 Well Development

The newly installed monitoring wells were developed between August 15, 2016, and August 17, 2016. Well development activities included measuring the water level and total depth of the well, surging the well with a PVC surge block, bailing the well with a weighted bailer to remove initial influx of sediment into the well, and finally using a submersible pump to purge the well. After well measurements were taken, a surge block was used to surge water into and out of the screened portion of the well for a minimum of 10 to 15 minutes. Bailers were then used to remove water and sediment from the well prior to pumping using a submersible electric pump. A minimum of ten well volumes of water were removed from each monitoring well during well development. Field parameters (pH, temperature, specific conductance and turbidity) were measured and recorded at regular intervals during pumping. Each well was purged until visibly clear and a minimum ten well casing volumes were removed. Purge water generated during well development was spread on the adjacent ground surface.

## 4.4 Aquifer Testing

A combination of aquifer pumping and slug tests were performed on the 16 new monitoring wells around the emergency ponds and ash ponds to evaluate the hydraulic conductivity of the geologic formation at each well location. The aquifer tests were performed between August 19, 2016 and August 23, 2016, after all wells had been developed.

Slug tests were performed on eight wells (MW-33B, MW-35B, MW-37B, MW-38B, MW-39B, MW-42B, MW-45B, and MW-47B). Wells MW-42B, MW-45B, and MW-47B are located directly adjacent to the Emergency Holding Ponds (**Figure 4-1**). Wells MW-33B, MW-35B, MW-37B, MW-38B, and MW-39B are located around the Ash Ponds to the southwest of the Emergency Holding Ponds. Slug tests were performed by first taking water level and total depth measurements on the well. A transducer was then lowered into each well and set at a depth of approximately 1 to 2 ft off the bottom of the well. The well was then allowed to recover back to the static water level recorded before the transducer was placed in the well. The transducer then began recording data and a slug was lowered into the well. The slug was placed at a depth to be fully submerged in the well above the height of the transducer, making sure that the transducer did not move during placement. The slugs used for the tests at the Basin Electric Laramie River station consisted of a 1-inch by 6-ft long section of PVC capped at both ends and filled with sand. One end of the slug contained an eye hook to allow a nylon rope to be attached to it for placement and retrieval. After slugs were placed in the well, the water level was allowed to return to within 95 percent of the static water level. Once 95 percent of static was achieved, the slug was removed and the water level was once again allowed to return to within 95 percent of static. The transducer in the well recorded the depth of water above the transducer, temperature, and hydraulic head pressure measurements within the well for the entirety of the test. Once a 95 percent static water level was achieved after removing the slug, the test was stopped and equipment was removed and decontaminated before using in the next well to be tested. Manual water level measurements were recorded on field slug test forms (**Appendix B**) and electronic data was removed from the transducer to be used for data evaluation.

Aquifer pumping tests were performed at eight of the newly installed monitoring wells at the Site (MW-32B, MW-34B, MW-36B, MW-40B, MW-41B, MW-43B, MW-44B, and MW-46B). Wells MW-41B, MW-44B, MW-46B, and MW-43B are located around the Emergency Holding Ponds (**Figure 4-1**). MW-32B, MW-34B, MW-36B, and MW-40B are located around the Ash Ponds. The pumping tests were performed in a similar manner to the slug testing (reference AECOM Standard Operating Procedure 18.0, **Appendix B**). Prior to starting each aquifer test, water level and total well depth measurements were taken. After well measurements were taken, a submersible electric pump was lowered into the well and placed at a level approximately 2 to 3 ft off the bottom. A transducer was attached to the pump tubing approximately 1 ft above the top of the pump. The water level was then allowed to stabilize before the test was started. After water level stabilization, the transducer started recording data and the pump was turned on to a flow rate ranging from 0.5 to 1.5 gallons per minute. The pumping rate was held constant during the test and drawdown in the well was recorded using the transducer and periodic manual water level measurements using an electronic water level meter. The pump remained on until drawdown neared the elevation the transducer was placed, or the water level in the well stabilized. The pump was then shut off and recovery of the water level was measured until 95 percent of the static initial water level was reached, at which time the test was stopped and equipment removed from the well and decontaminated prior to testing of the next well. Manual measurements were recorded on field aquifer testing forms (**Appendix B**) and electronic data was removed from the transducer and used for data evaluation.

## 4.5 Slug Test Analysis

Data from the slug tests performed at the Site were processed and analyzed using the software AQTESOLV (Duffield 2007), which provides type curve solutions from published methods corresponding to a range of conceptual models for various well completions and aquifer types (e.g., fully penetrating well in an unconfined aquifer), and simplifying hydrologic assumptions (e.g., infinite aquifer extent). After initial processing and analysis, the most appropriate conceptual model was determined to be the Bouwer and Rice Slug Test Solution for Unconfined Aquifers (Bouwer & Rice 1976). This method uses a straight line fit to the observed water-level displacement and is applicable to wells screened below and across the water table. Graphs of the slug test results are included in **Appendix B**. For wells screened across the water table (all except MW-39B and MW-42B), a double straight line can be observed in the data sets when plotted on a log-normal axes, with a line of a steeper slope in early time representing groundwater entering or exiting the well from the filter pack. The second segment of data with a shallower slope represents the behavior of the geologic formation located immediately outside of the filter pack. In these cases, an effective casing



radius correction factor is applied and the straight line solution is fit to the second slope in the data. Some basic assumptions of the Bouwer-Rice solution include:

- Aquifer has infinite areal extent;
- Aquifer is isotropic and has uniform thickness;
- Aquifer potentiometric surface is initially horizontal;
- Control well is fully or partially penetrating;
- A volume of water,  $V$  (the slug), is injected or discharged instantaneously from the control well;
- Flow is steady; and
- Aquifer is confined or unconfined.

Results from the slug test analyses are summarized in **Table 4-2**. AQTESOLV analyses of the slug test data for each well are presented in **Appendix B**. The average estimated hydraulic conductivity of the completed slug tests was 2.16 ft per day (ft/d) with a geometric mean of 1.65 ft/d. The minimum hydraulic conductivity of 0.45 ft/d was estimated at MW-39B. The maximum of 6.28 ft/d was estimated at MW-37B. Although the software calculates a value for aquifer storage from the slug test data, these values are assumed to represent rough approximations, as both slug tests and single-well pumping tests are considered relatively poor methods to determine aquifer storage.

## 4.6 Pumping Test Analysis

Pumping test data also were analyzed using the software package AQTESOLV. Type curve solutions for pumping tests available in AQTESOLV typically require observation well data. In cases where observations from only the pumping well are available, aquifer storage calculations are not usable; however, hydraulic conductivity calculations are still valid. Data were analyzed as single well pumping tests using the Moench solution for a pumping test in an unconfined aquifer (Moench 1997). The Moench solution is the only available option in AQTESOLV for unconfined aquifers which accounts for wellbore storage. Due to the low flow rate of the pump test, wellbore storage has a clear effect on the data in early time. Although the data most indicative of aquifer behavior is in late time, it is helpful to account for the wellbore storage through derivative plot analysis, ensuring that the conceptual model for the solution is valid. For the pumping test analysis graphs shown in **Appendix B**, the observed data are plotted with black squares, and the Moench solution is plotted with a blue line. The derivative data are plotted with gray crosses and the derivative solution is plotted in a red line.

The Moench solution utilizes the following assumptions:

- Aquifer has infinite areal extent;
- Aquifer is homogeneous, isotropic and of uniform thickness;
- Aquifer is unconfined; and
- Flow is unsteady.

Results from the pumping test analyses are summarized in **Table 4-2**. AQTESOLV analyses of the pump test data for each well are presented in **Appendix B**. The average estimated hydraulic conductivity of the eight pumping tests was 1.40 ft/d with a geometric mean of 1.19 ft/d. The minimum hydraulic conductivity of 0.65 ft/d was estimated at MW-34B. The maximum of 3.12 ft/d was estimated at MW-41B. During the pumping test on MW-44B, the well began to recharge prior to the completion of the test. No significant fluctuations were observed in the flow rate at this time. It is possible that these results were affected by the drawdown cone reaching a recharge boundary, or insufficient well development. Hydraulic conductivity results for well MW-44B yielded similar results to the other wells tested.

## 4.7 Addition of Existing Monitoring Wells in November 2016

The first CCR baseline groundwater monitoring event at LRS was conducted in September 2016. A review of the resulting data concluded that the assessment of baseline groundwater conditions associated with the ash impoundments and landfill could be improved by modifying the list of monitoring wells included in the CCR monitoring system. Therefore, the monitoring system was modified in November 2016, as described below for subsequent baseline monitoring events:

- Existing monitoring wells MW-14BR, MW-20B, and MW-21B were added to the groundwater monitoring program (**Figure 4-1**). These wells are located downgradient of the ash impoundments and eastern portion of the ash landfill, and supplement the downgradient data provided by MW-36B, MW-37B, MW-38B, and MW-48B.
- Monitoring wells MW-33B, MW-34B, and MW-35B were removed from the groundwater sampling program because they were found to be cross-gradient from the ash impoundments, although groundwater elevations continued to be measured in these wells to support interpretation of Site-wide groundwater flow.

#### 4.8 Addition of New and Existing Monitoring Wells in 2017

The LRS CCR groundwater monitoring network was modified in July 2017 based on an evaluation of interim baseline data acquired in 2016 through the spring of 2017. The rationale for expanding the network was to provide greater resolution of baseline groundwater quality and flow in the vicinity of the three ash ponds, and support an evaluation of upgradient and downgradient conditions for Ash Pond 1 and a multi-unit consisting of Ash Pond 2, Ash Pond 3, and the Ash Landfill. The monitoring wells added to the network in July 2017 included two existing wells along the northern edge of the ash ponds: MW-22B and MW-23B. In addition to these wells, six new monitoring wells were installed along the northern edge of the ash ponds and between the ash ponds: MW-48B, MW-49B, MW-50B, MW-51B, MW-52B and MW-53B.

The six new monitoring wells were installed using sonic drilling methods consistent with the methods described above to install the monitoring wells in 2016. Drilling and well construction was performed by O'Keefe Drilling of Butte, Montana. Soil cores recovered during drilling were logged by an AECOM geologist. **Appendix A** contains the borings log for each monitoring well. Construction details for the six monitoring wells installed in July 2017 are presented in **Table 4-1**. Each well was constructed of 2-inch-diameter, schedule 40 PVC riser pipe and slotted screen. The well screen was constructed using 20 ft of 0.010-inch factory-slotted PVC screen positioned to straddle the water table. The annular space between the borehole and screen was filled with clean 10/20 silica sand filter pack to a minimum of 2 ft above top of screen. Bentonite chips were placed above the filter pack and hydrated with potable water to seal the filter pack from potential infiltration of surface water. The annular space above the bentonite seal was filled with Portland Type I/II grout and allowed to set for a minimum of 24 hours. All wells except for MW-48B were completed with flush-mount construction to provide protection from vehicular traffic. MW-48B was constructed with an above-grade outer steel casing. The surface monuments were labeled with the well identification number and anchored in a 2-ft square concrete pad. Construction diagrams for the six monitoring wells are included in **Appendix A**.

The six newly installed monitoring wells were developed by surging with a PVC surge block and pumping using a submersible pump. Each well was purged until visibly clear and after a minimum ten well casing volumes were removed. Purge water generated during development was spread onto the adjacent ground surface. Aquifer testing was not performed on the six new monitoring wells because sufficient data was obtained during testing of the 16 wells installed in 2016 to adequately characterize the hydrogeological characteristics of the uppermost aquifer in the vicinity of the LRS CCR units.

#### 4.9 Addition of New Monitoring Wells in 2019

Because of the detection of Appendix IV constituents at statistically significant levels above groundwater protection standards in monitoring well MW-38B, LRS installed a series of four monitoring wells to fulfill the requirements of 40 CFR 257.95(g)(1)(i) to characterize the nature and extent of the release. Three of the wells (MW-54B, MW-55B, and MW-56B) help delineate the horizontal extent, including the characterization at the downgradient property boundary (**Figure 4-1**). The fourth new monitoring well, MW-38C, was installed near MW-38B to evaluate the vertical extent of potential release of CCR constituents from Bottom Ash Pond 1.

The four new monitoring wells were installed using hollow system auger methods. Drilling and well construction was performed by Inberg Miller located in Riverton, Wyoming. Soil cores recovered during drilling were logged by an AECOM geologist. **Appendix A** contains the borings log for each monitoring well. Construction details for the four monitoring wells installed in 2019 are presented in **Table 4-1**. MW-54B was constructed with a 2-inch internal diameter (ID), Schedule 40, PVC riser. MW-55B, MW-56B, and MW-38C were constructed with 2-inch ID, Schedule 80, PVC risers. The well screen was constructed using 20 ft of 0.010-inch factory-slotted PVC screen positioned to straddle the water table for wells MW-54B, MW-55B, and MW-56B. MW-38C was constructed with an 11-ft long, 2-inch ID, 0.010-inch slotted PVC screen with prepacked sand. A prepacked screen was utilized due to flowing sands entering the borehole due to increased hydrostatic pressure causing the surrounding formation to enter

the borehole before a screen and sand pack could be installed. The annular space between each PVC well casing and boring wall was filled with 10/20 silica sand pack from the bottom of the boring to 2 ft above the top of each screen. The filter pack material was emplaced in a manner to prevent bridging between the borehole and the casing. A 2-foot thick layer of 3/8-inch bentonite chips was installed above the sand pack and hydrated. A hydrated bentonite grout mixture was placed above the interval of hydrated bentonite chips to the surface. Wells were constructed with an above-grade outer steel casing. The surface monuments were labeled with the well identification number and anchored in a 2-ft square concrete pad.

#### 4.10 Replacement of Existing Monitoring Wells in 2024

LRS replaced monitoring well MW-53B with monitoring well MW-53BR in April 2024 due to damage to the screen interval of well MW-53B, which was located on the top edge of a steep berm that supports an access road encircling Pond 3. The old well was drilled to a depth of 120 ft bgs between May 20, 2017 and May 28, 2017, as part of the original CCR network. MW-53B was determined to have a damaged 20-ft screen (100 ft bgs to 120 ft bgs), which allowed silt to infiltrate into the well and completely fill and block the screened interval with silt. The well was abandoned using hydrated bentonite grout in April 2024. Monitoring well MW-53BR was drilled to a depth of 120 ft bgs to match the depth of the original MW-53B. **Appendix A** contains the boring log for MW-53BR. Materials and well completion consisted of the following:

- 100 ft of 2-inch ID, schedule 40 PVC casing;
- 20 ft of 2-inch ID, schedule 40 PVC, 0.010 slotted screen (100 – 120 ft bgs);
- Casing centralizers placed approximately every 25 vertical ft;
- 10/20 silica sand filter pack from 120 to 98 ft bgs;
- Bentonite seal from 98 to 93 ft bgs;
- Bentonite grout from 93 to 10 ft bgs;
- Bentonite seal from 10 to 4 ft bgs; and
- Concrete from 4 ft bgs to surface.

Monitoring wells MW-50B, MW-51B, and MW-52B, which are located on the same berm as MW-53B/BR, required their surface completions be raised between six and 30 inches to be flush with the access road, because the elevation of the access road was modified during Pond 3 retrofit activities. In April 2024, Cascade Drilling removed the original surface completions of the three wells and attached a sufficient length of 2-inch ID schedule 40 PVC casing to the existing well riser to bring them flush with the access road. New traffic rated flush-mount surface completions were added for security and protection. Stockpile soil at the Site was used to fill in the depressions left by the removal of the original surface completions and then a new 2-ft by 2-ft concrete pad was constructed into which a new metal vault was secured for each well location. Construction details for the four monitoring wells installed or modified in April 2024 are presented in **Table 4-1**.

#### 4.11 Recovery Well Installation

There are two wells at the facility that are not currently part of the compliance network. The two recovery wells, RW-1 and RW-2, were installed between November 3, 2021 and November 6, 2021 at Basin LRS. A subcontracted drilling company (Cascade Drilling/Technical Services) mobilized a sonic drilling rig and crew to LRS for the well installation with observation and oversight by an AECOM geologist. Both wells are constructed of 6-inch ID schedule 40 PVC. Each well was temporarily completed with a stick up above ground surface with four safety bollards surrounding. Outer protective casings were not installed at the wells because the surface completions were redone during the final completion phase of the extraction well system completed in 2024. RW-1 and RW-2 were drilled and completed to 80 and 85 ft bgs), respectively. Each well has a screen interval of 20 ft at the bottom of the well with a 0.020-inch PVC slotted screen. The borehole annulus around the screen was filled with 10/20 Colorado silica sand pack that was placed from the bottom of the screen to 2 ft above the top of screen. A minimum of 2 ft of bentonite chips was placed above the sand pack as a seal and allowed to hydrate before the well was grouted. The annulus of the borehole was grouted using a high solids bentonite grout from the top of the seal to approximately 7 to 8 ft bgs. The remaining space to ground surface was initially filled with 10/20 sand, which was later removed during installation of pitless adapters during extraction system installation and startup. Sampling ports were installed on extraction system piping

at each well head to allow for potential compliance monitoring of the system in the future. The recovery wells are not part of the compliance network that is required to be certified in this report.

## 5. System Evaluation

The Final CCR Rule establishes the following general performance standard for CCR groundwater monitoring systems:

- All groundwater monitoring systems must consist of a sufficient number of appropriately located wells (at least one upgradient and three downgradient wells) in order to yield groundwater samples from the uppermost aquifer that represent the quality of background groundwater and the quality of groundwater passing the CCR waste boundary.
- The objective of a groundwater monitoring system is to intercept groundwater to determine whether the groundwater has been contaminated by the CCR disposal unit. The number, spacing, and depths of the monitoring wells must be determined based on a thorough characterization of the Site, including a number of specifically identified factors relating to the hydrogeology of the Site.

The “uppermost aquifer” and “aquifer” are defined in the Final CCR Rule in § 257.53, as follows:

“Uppermost aquifer” means the geologic formation nearest the natural ground surface that is an aquifer, as well as lower aquifers that are hydraulically interconnected with this aquifer within the facility’s property boundary. Upper limit is measured at a point nearest to the natural ground surface to which the aquifer rises during the wet season.

“Aquifer” means a geologic formation, group of formations, or portion of a formation capable of yielding usable quantities of groundwater to wells or springs.

As described in the drilling and well construction discussion in **Section 4**, drilling equipment and procedures were employed to identify the uppermost aquifer and ensure each new monitoring well was installed with appropriate total depth and placement of the well screen to: (1) facilitate collection of representative samples of the uppermost aquifer; and (2) accurately measure water table elevations to support evaluation of groundwater gradient and flow direction.

Also as described in **Section 4**, selection and construction of the CCR monitoring system for LRS evolved and adapted based on the results obtained from baseline groundwater monitoring in 2016 and 2017. The final monitoring system consists of 22 monitoring wells that will be sampled as part of the detection monitoring program. The list of wells selected for sampling background and downgradient groundwater quality for each CCR unit or multi-unit is summarized below:

CCR Unit/Multi-unit	Background Wells	Downgradient Wells
Ash Pond 1	MW-52B, MW-53BR	MW-49B, MW-21B, MW-38B, MW-38C*
Ash Pond 2, Ash Pond 3, Ash Landfill	MW-39B, MW-32B	MW-36B, MW-37B, MW-20B, MW-14BR, MW-40B, MW-52B, MW-53BR
Emergency Holding Ponds	MW-41B, MW-42B, MW-43B	MW-44B, MW-45B, MW-46B, MW-47B

\*MW-38C, installed in April 2019 was added to the assessment monitoring program as a downgradient compliance well for Bottom Ash Pond 1.

The following nine monitoring wells are included in the monitoring system only for the purpose of measuring groundwater elevations and evaluating groundwater flow direction and velocity in the vicinity of the ash ponds and landfill:

- MW-33B, MW-34B, MW-35B, MW-48B, MW-50B, MW-51B, MW-545B, MW-55B, and MW-56B.
- Monitoring wells MW-22B, and MW-23B were removed from the monitoring well network due to damage sustained to the wells during retrofit of Ponds 1 and 2. MW-22B and MW-23B had been used for measuring groundwater elevations only.

Potentiometric surface maps have been constructed using the depth to groundwater measurements obtained during recent groundwater monitoring and monitoring well locations and elevations measured by a licensed professional land surveyor. Maps of the potentiometric surface for June 2024 and September 2024 are presented as **Figures 5-1**

and 5-2, respectively. The associated depth to groundwater measurements and calculated groundwater elevations are presented in **Table 5-1** and **Table 5-2**. Groundwater elevations were calculated at each well by subtracting the measured depth to groundwater from the surveyed top of casing elevation. Groundwater elevations for each monitoring well are posted on the figures, with inferred isoelevation contours of the groundwater potentiometric surface. The direction of groundwater flow is generally to the northeast, perpendicular to the potentiometric contour lines. The groundwater flow maps reflect a relatively consistent pattern of groundwater flow beneath the LRS CCR units, and support the selection of the wells listed above to represent background groundwater quality and the quality of groundwater downgradient of the CCR units.

- The monitoring well system has been established at the CCR Landfill at the Basin Electric Power Cooperative Laramie River Station to comply with the requirements of the EPA CCR Rule. The following factors support the spacing and depth of the monitoring wells of the network. Groundwater flow at the Site is generally to the north-northeast. The majority of the recharge to this aquifer is from irrigation on agricultural lands to the south of the facility, resulting in relatively shallow, predominantly horizontal groundwater flow.
- The wells were screened in the uppermost aquifer, which beneath the LRS facility is the upper unit of the Arikaree Formation. As detailed in **Section 3**, this is a very fine-grained soft- to moderately-hard, generally massive sand and silt. Well screens are 20-ft long for most of the monitoring wells at the facility and the screens range in depth from 55 to 110 ft bgs.
- The Arikaree Formation, which is about 790-ft thick beneath the Site, is the principal water source for agricultural irrigation in the Wheatland Flats. Because of the relatively low permeability of the Arikaree Formation, large yields of water cannot be obtained from its shallower depths. Wells with depths of 500 ft or more are typically required in order to obtain sufficient yields for irrigation (Morris and Babcock 1960). Thus, the CCR program wells are screened a significant vertical distance above the primary water source for the region.
- In 2019, monitoring well MW-38C was installed with a screened interval from 125 to 114 ft bgs to assess for the potential of a downward contaminant migration component from the uppermost aquifer well MW-38B (screened from 75 to 55 ft bgs). Water quality sampling and groundwater level measurements from these two wells have provided the following results:
  - The static water level measured at MW-38C has been higher than at MW-38B, indicating an ambient upward gradient in groundwater flow (i.e., an impediment to downward migration of contaminants) (AECOM 2023).
  - Contaminants detected in the shallow well (MW-38B) were not detected in the deep well (MW-38C) above cleanup criteria (AECOM 2019).

These provide further evidence that groundwater flow is relatively shallow and predominantly horizontal, and that the monitoring wells are screened in the uppermost aquifer and are hydraulically isolated from the regional principal aquifer.

- The Arikaree Formation is largely aeolian in origin, resulting in deposition of relatively homogeneous and isotropic silty fine sand deposits through which groundwater flow can be expected to be relatively consistent and predictable. To determine horizontal well spacing, flow paths were drawn across the units with downstream arrows terminating at monitoring wells downgradient of each unit/multi-unit. This demonstrates that the horizontal spacing of the downgradient wells ranges from approximately 600 ft between MW-14BR and MW-20B to approximately 1,000 ft between MW-36B and MW-37B.
- The unsaturated (vadose) zone between the base of the landfill and the monitored aquifer is approximately 60 to 160 ft thick. Hypothetical vertical contaminant transport from the landfill to the aquifer would be subject to significant lateral diffusion prior to encountering and mingling with groundwater, suggesting that any impacts to groundwater are unlikely to be confined to a discrete flow path as might be expected in a more heterogeneous aquifer and/or vadose zone.

Based on these factors, the spacing of downgradient wells in this aquifer is sufficient to accurately represent the quality of groundwater passing the waste boundary of each CCR unit/multi-unit and potential contaminant pathways are being monitored.

## 6. Statistical Methodology

### 6.1 Regulatory Guidance

Regulatory guidance provided in 40 CFR §257.90 specifies that a CCR groundwater monitoring program include selection of the statistical procedures to be used for evaluating groundwater quality data as required by 40 CFR §257.93. Groundwater quality monitoring data will be collected under the detection or assessment monitoring programs outlined in this plan and will include collection and analysis of samples from each background and downgradient compliance well, for each CCR unit or multi-unit, as required by 40 CFR §257.94(b) or 40 CFR §257(b). The groundwater samples will be analyzed for the constituents listed in 40 CFR §257 Appendices III and IV.

After the eight sets of groundwater samples were collected and analyzed, these data were statistically evaluated to determine if there are any statistically significant increases (SSIs) over background concentrations for the Appendix III and IV constituents. In determining whether an SSI has occurred, the constituent concentrations at the downgradient wells and the background wells for each unit/multi-unit were compared using one or more of the statistical methods discussed below.

40 CFR §257.93(f) outlines the statistical methods available to evaluate groundwater monitoring data. The statistical test(s) chosen will be conducted separately for each constituent in each monitoring well and will be appropriate for the constituent data and their distribution. The available statistical methods include the following:

- A parametric analysis of variance (ANOVA) followed by multiple comparison procedures to identify statistically significant evidence of contamination. The method must include estimation and testing of the contrasts between each compliance well's mean and the background mean levels for each constituent;
- An ANOVA based on ranks followed by multiple comparison procedures to identify statistically significant evidence of impacts. The method must include estimation and testing of the contrasts between each compliance well's median and the background median levels for each constituent;
- A tolerance or prediction interval procedure, in which an interval for each constituent is established from the distribution of the background data and the level of each constituent in each compliance well is compared to the upper tolerance or prediction limit;
- A control chart approach that gives control limits for each constituent; or
- Another statistical test method that meets the performance standards of 40 CFR §257.94(g) outlined in the paragraph below.

The chosen statistical method will comply with the following performance standards, as appropriate, based on the statistical test method used. The performance standards include the following:

- The statistical method used to evaluate groundwater monitoring data will be appropriate for the constituent distribution (i.e., parametric or nonparametric).
- If an individual well comparison procedure is used to compare an individual compliance well constituent concentration with background constituent concentrations or a groundwater protection standard, the test shall be done at a Type I error level no less than 0.01 or 0.05, depending on the method chosen. This performance standard does not apply to tolerance intervals, prediction intervals, or control charts.
- If a control chart approach is used to evaluate groundwater monitoring data, the specific type of control chart and its associated parameter values shall be such that this approach is at least as effective as any of the other statistical analysis approaches specified above.
- If a tolerance interval or a prediction interval is used to evaluate groundwater monitoring data, the levels of confidence and, for tolerance intervals, the percentage of the population that the interval must contain, shall be such that this approach is at least as effective as any of the other statistical analysis approaches specified above.
- The statistical method must account for data below the limit of detection with one or more statistical procedures that shall be at least as effective as any of the other statistical analysis approaches specified above.



- If necessary, the statistical method must include procedures to control or correct for seasonal and spatial variability as well as temporal correlation in the data.

Per 40 CFR §257.93(h)(2), statistical analysis of the first eight rounds of data must be completed within 90 days after completing the initial groundwater sampling and analysis to determine whether there has been an SSI over background for any constituent. The first eight rounds of groundwater sampling and analysis must be completed no later than October 17, 2017. In accordance with 40 CFR §257, LRS must obtain a certification from a qualified professional engineer stating that the selected statistical method is appropriate for evaluating the groundwater monitoring data for the CCR management area. The certification must include a narrative description of the statistical method selected to evaluate the groundwater monitoring data.

Assessment monitoring is required per 40 CFR §257.95 whenever a statistically significant increase over background levels has been detected for one or more of the indicator parameters listed in 40 CFR §257 Appendix III. An assessment monitoring program also includes annual groundwater sampling and analysis for the constituents listed in 40 CFR §257 Appendix IV. The purpose of assessment monitoring is to determine if releases of CCR constituents have occurred.

The facility can return to detection monitoring once assessment monitoring results are at or below background values for two consecutive assessment monitoring events. If the assessment monitoring identifies an Appendix IV constituent at a statistically significant level above the groundwater protection standard established per 40 CFR §257.95(h), groundwater assessment of corrective measures must be initiated.

## 6.2 Statistical Analysis Approach

There is no single method of statistical analysis that is appropriate for each groundwater constituent dataset. It is most prudent to use a suite of statistical methods that are dependent on the data and their distributions. The statistical analyses will be based on an interwell and/or an intrawell approach for the purpose of determining if an LRS CCR unit/multi-unit has impacted groundwater quality. The statistical algorithms used for the interwell and intrawell approaches will be chosen based on the groundwater constituent data and their distributions as well as consideration of natural seasonally- or spatially-varying groundwater constituent concentrations.

Eight rounds of baseline groundwater monitoring data were collected and analyzed for the 40 CFR 257 Appendices III and IV constituents. These data will be used to represent background groundwater quality for the LRS CCR units. The detection monitoring data collected at the downgradient wells will be used to determine if any of the CCR units/multi-unit have impacted groundwater quality. The initial eight rounds of detection monitoring sampling and analysis were completed prior to the October 17, 2017 deadline established in the CCR Rule (40 CFR §257.94).

A preliminary, exploratory statistical analysis was conducted after the eight rounds of baseline data were obtained to initially assess the constituent data and determine the most appropriate statistical approach(es) for the data. The data were examined for outliers and the percentage of non-detect values to verify that the data collected are suitable for statistical analysis. The data were also examined using goodness-of-fit tests to determine the most appropriate statistical distribution and time series plots and areal maps were used to determine if seasonal or spatial variations in constituent concentrations were present. Based on this preliminary evaluation of the data, an interwell statistical approach was selected as appropriate for evaluating groundwater at LRS, as described below.

Per 40 CFR §257.93(h)(2), statistical analysis of all eight rounds of data must be completed within 90 days after completing groundwater sampling and analysis to determine whether there has been a statistically significant increase over background for any Appendix III constituent.

## 6.3 Interwell Statistical Approach

Interwell tests compare the statistical differences between (upgradient) background and downgradient compliance wells. An interwell statistical approach will be used during detection monitoring for the following reasons:

- Sufficient data are available in the upgradient background well to ensure adequate degrees of statistical power to detect real exceedances above background levels, and also reasonable control over the site-wide false positive rate so that spurious exceedances have little chance of being identified.



- Although there is evident spatial variation among most, if not all, of the Appendix III constituents, it is unclear to what extent the similarly evident variation among the downgradient wells is due strictly to natural differences in groundwater quality and/or other factors unrelated to management of the CCR ash. Because of this uncertainty, an interwell comparison strategy appears to be initially more appropriate for LRS.

As a caveat to this approach, for constituents that occur naturally and vary substantially in concentration across LRS due to natural hydrogeologic or geochemical factors — thus, exhibiting significant spatial variability — an interwell testing scheme will not always be helpful. Using an interwell approach, constituent concentrations greater than background might be attributed to anthropogenic contamination, when in fact the differences are actually natural and due to locally varying distributions of groundwater constituents. In such cases, an intrawell approach may be warranted.

Furthermore, there is no requirement either in RCRA or the CCR Rule to use exactly the same statistical method or approach for every constituent. Depending on characteristics of LRS and data that are collected, a mix of interwell and intrawell tests may be warranted. At this Site, the initial statistical screening suggests that interwell comparisons are most appropriate despite evident spatial variability. However, that conclusion could change as additional data are collected during future detection monitoring. If new information indicates that constituent concentrations remain relatively stable and that the existing spatial variation is unrelated to the CCR units, a modification of the statistical approach to intrawell testing may be recommended for one or more constituents.

Under an interwell statistical approach in detection monitoring, the actual statistical method(s) chosen will be determined based on the constituent data distribution (as outlined below), which in turn is influenced both by the percentage and pattern of non-detect measurements as well as the temporal stability of the concentration levels.

When (1) the percentage of non-detects is low to moderate (i.e., less than 50-60 percent); (2) the background data can be normalized (perhaps via a standard transformation); and (3) the results are stationary (i.e., stable over time), the following statistical methods are highly recommended by USEPA (2009):

- Interwell control charts with retesting; or
- Parametric interwell prediction limit methods with retesting.

When the background data cannot be normalized (perhaps due to a large percentage of non-detects), but the data are stationary (i.e., stable over time), the following statistical method is recommended by USEPA (2009):

- Non-parametric interwell prediction limits with retesting.

Note that the specific retesting method in each of these options will be chosen to account for the size of the well network, the amount of background data available, the number of constituents being monitored, the site-specific mix of intrawell and interwell tests, and the impact of these factors on the statistical power and accuracy of the test. At this Site, the upgradient background wells relative to the number of downgradient wells to be tested on a semi-annual basis will enable use of a 1-of-2 retesting plan. This necessitates collection of a single independent resample at any location in which the initial routine measurement exceeds its respective statistical limit. A confirmed statistical exceedance will not be recorded unless both the initial measurement and resample value both exceed the statistical limit.

If the upgradient background data are non-stationary and thus exhibit a clear trend, it will suggest that factors unrelated to the CCR unit are impacting upgradient groundwater quality. Three general scenarios will be considered:

- Older background data may no longer be representative of current Site conditions and may need to be excluded from statistical calculations. In this case, the interwell statistical limits will be updated to include only the most representative background data.
- The compliance wells will be examined to see if similar trends are occurring downgradient. If so, a common trend component will be estimated across the Site and removed from every well. The residual data will then be used to construct revised statistical limits and tested, as described above.
- If the trend in upgradient background wells is not reflected in downgradient wells, further investigation may be needed to determine if the upgradient data still serve as a reasonable background with which to compare

downgradient compliance measurements. If not, the statistical approach will be modified to an appropriate intrawell strategy.

Because of the decision matrix needed to establish the correct statistical approach, the background data for each constituent will be periodically screened prior to construction of new or revised statistical limits. This screening will examine the proportion and pattern of outliers and potential data anomalies (perhaps due to laboratory or field sampling factors), the presence or absence of statistically significant trends over time, the presence or absence of statistically significant outliers, and the identification of an appropriate statistical distribution. In particular, any confirmed background outliers will be excluded from statistical calculations, so as not to unduly bias the statistical limits.

## 6.4 Proposed Statistical Methods for Appendix III Analytes

**Table 6-1** provides a summary of the proposed statistical method by well for Appendix III analytes. This table is based on a screening of the background and downgradient well data collected to date. The proposed statistical method is subject to review and potential change in the future, as necessary, to address significant changes in conditions.

## 7. Limitations

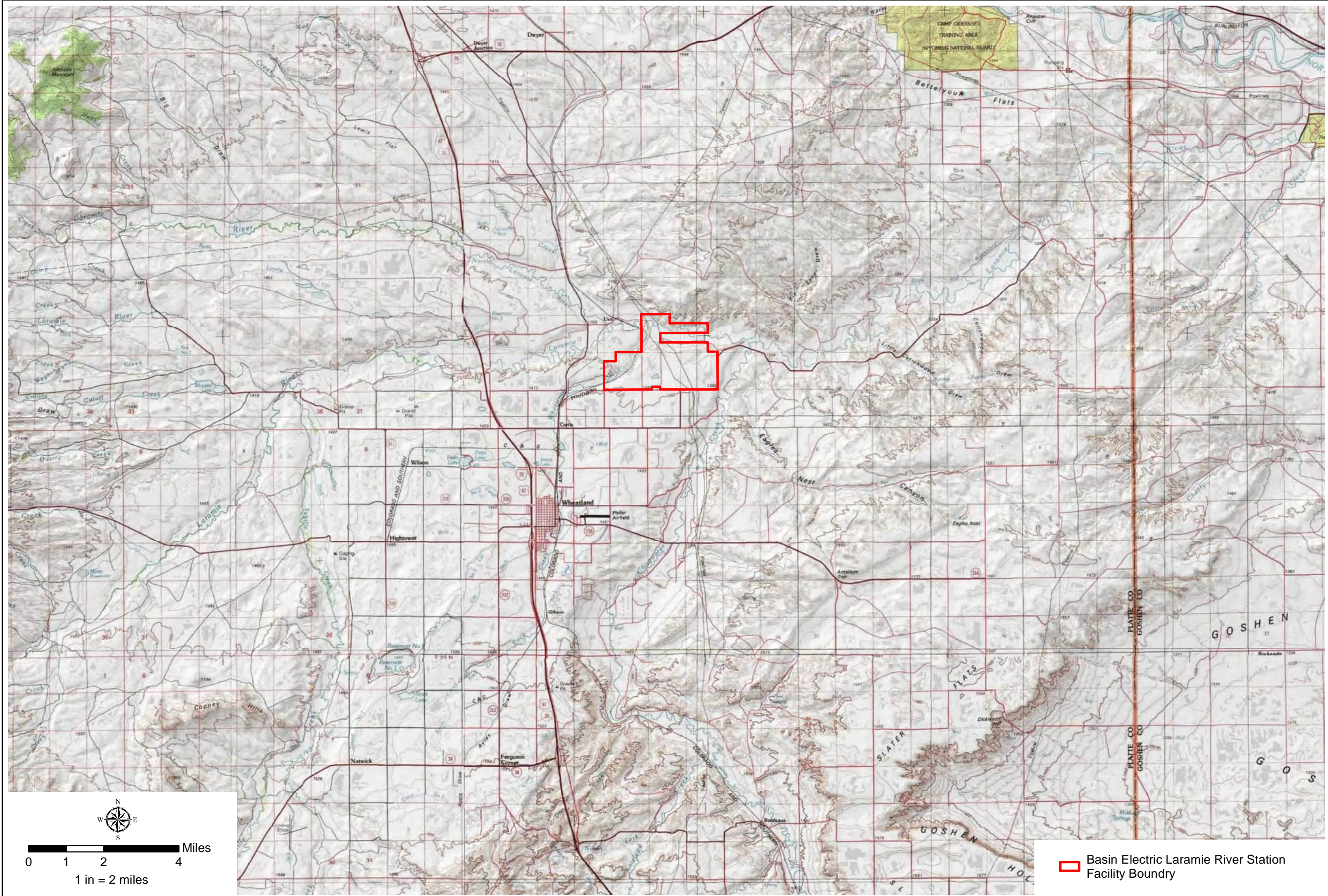
The signature of AECOM's (Consultant's) authorized representative on this document represents that, to the best of Consultant's knowledge, information, and belief in the exercise of its professional judgment, it is Consultant's professional opinion that the aforementioned information is accurate as of the date of such signature. Any opinion or decisions by Consultant are made on the basis of Consultant's experience, qualifications, and professional judgment and are not to be construed as warranties or guaranties. In addition, opinions relating to environmental, geologic, and geotechnical conditions or other estimates are based on available data, and actual conditions may vary from those encountered at the times and locations where data are obtained, despite the use of due care.


## 8. References

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## Figures



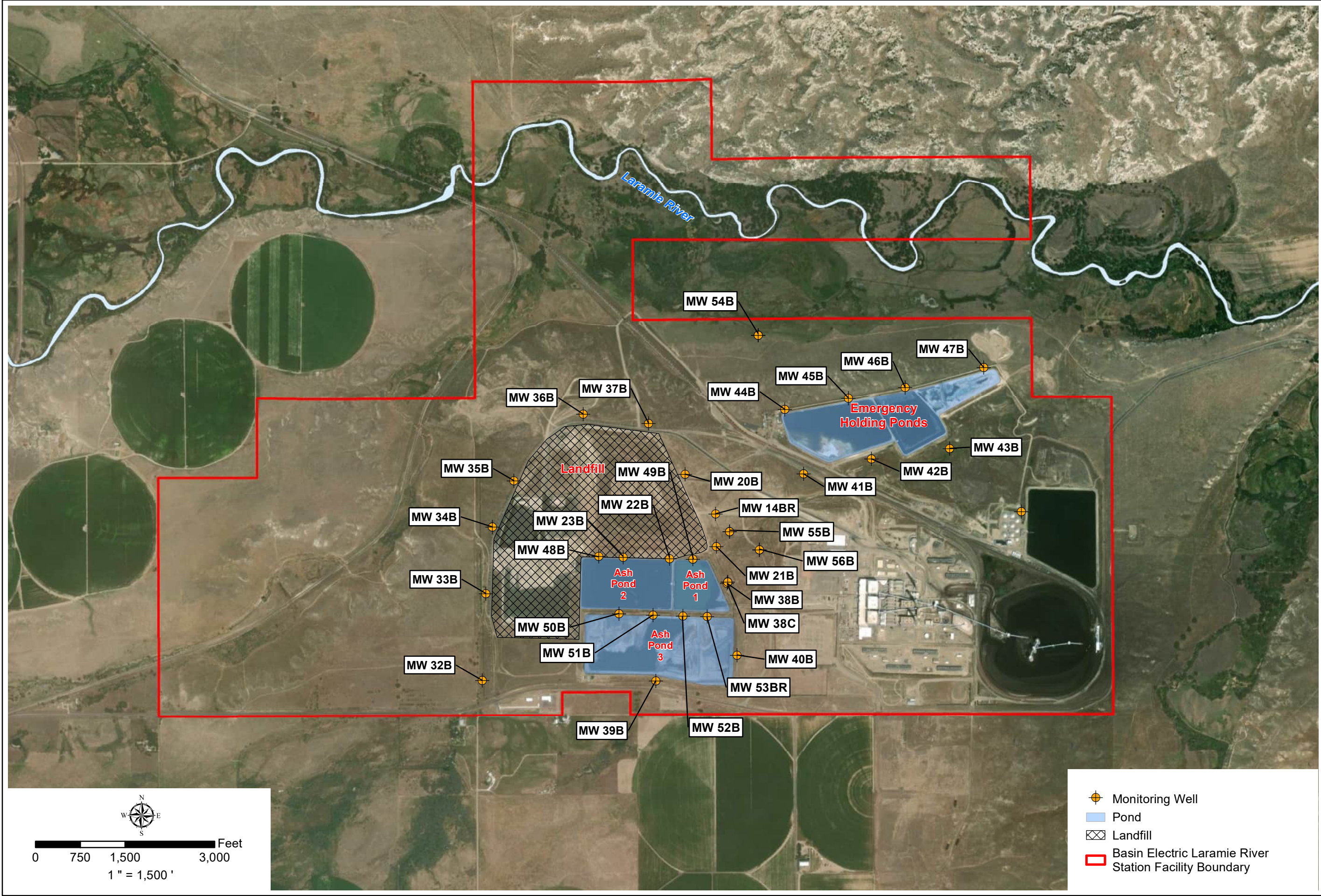


 Basin Electric Laramie River Station Facility Boundary

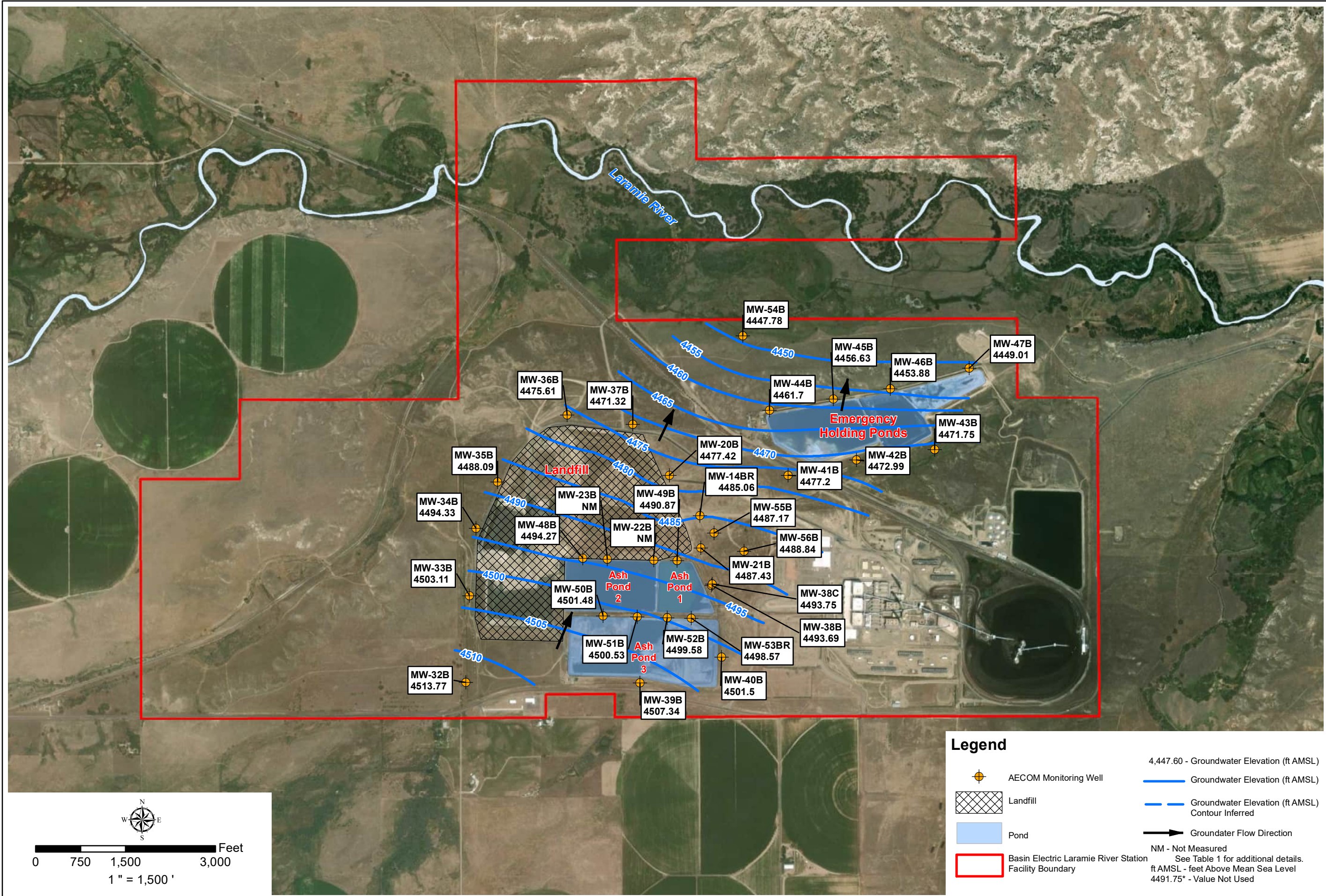
Site Location Map





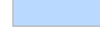




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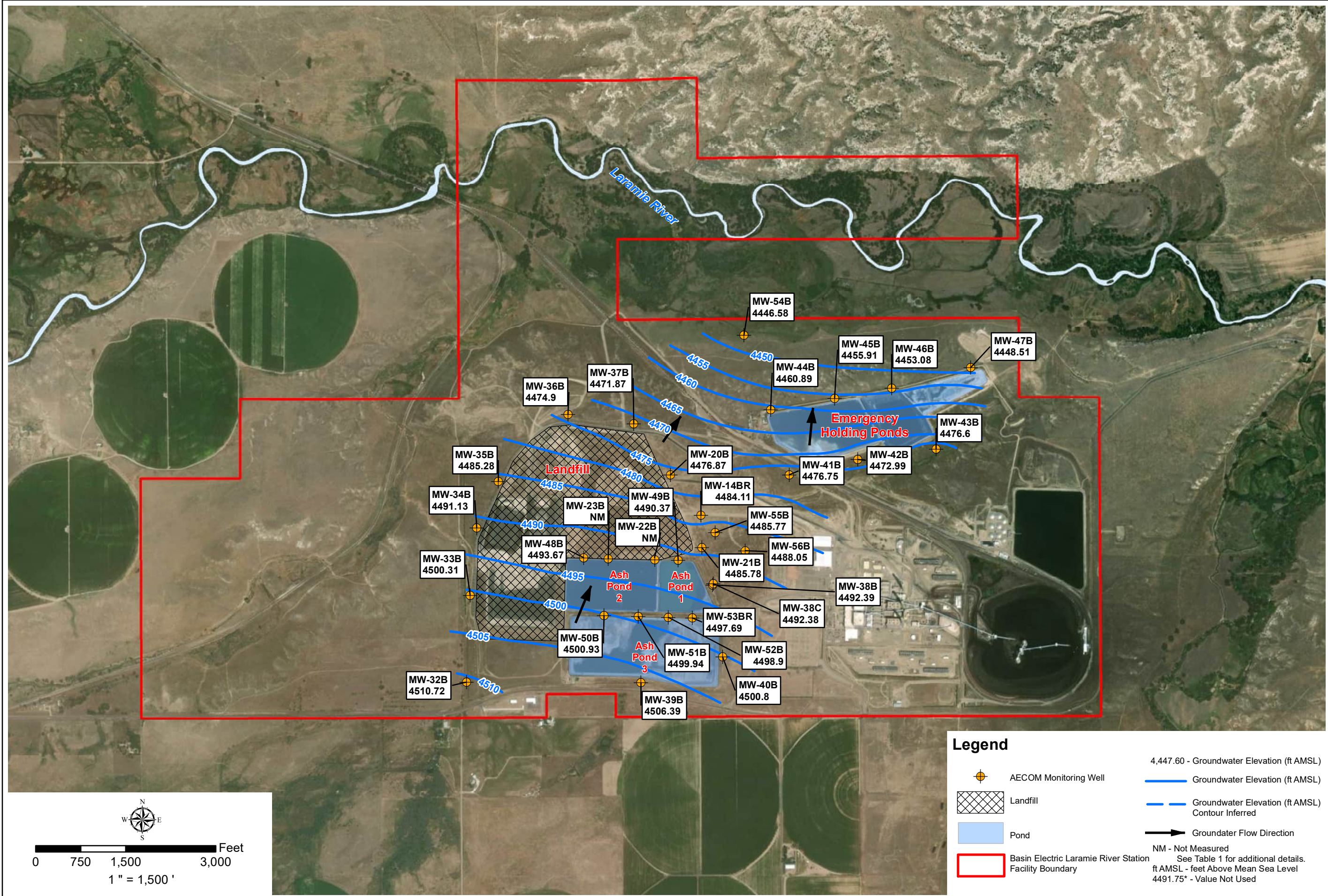
**Legend**

-  AECOM Monitoring Well
-  Landfill
-  Pond
-  Basin Electric Laramie River Station Facility Boundary
-  4,447.60 - Groundwater Elevation (ft AMSL)
-  Groundwater Elevation (ft AMSL) Contour Inferred
-  Groundwater Flow Direction
- NM - Not Measured  
See Table 1 for additional details.
- ft AMSL - feet Above Mean Sea Level  
4491.75\* - Value Not Used

Potentiometric Surface Map  
June 4-5, 2024



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0 750 1,500 3,000 Feet  
1" = 1,500'

- Legend**
- AECOM Monitoring Well
  - Landfill
  - Pond
  - Basin Electric Laramie River Station Facility Boundary
  - 4,447.60 - Groundwater Elevation (ft AMSL)
  - Groundwater Elevation (ft AMSL)
  - Groundwater Elevation (ft AMSL) Contour Inferred
  - Groundwater Flow Direction
  - NM - Not Measured  
See Table 1 for additional details.
  - ft AMSL - feet Above Mean Sea Level
  - 4491.75\* - Value Not Used



## Tables

**Table 4-1: Monitoring Well Construction Details**

Well Name	Year of Construction	State Plane WY East Zone Coordinates		Top of Casing Elevation <sup>1</sup> (ft amsl)	Ground Surface Elevation (ft amsl)	Total Depth (ft bgs)	Well Screen Interval (ft bgs)	Well Screen Lithology	Coordinate System (Elevation)
		Northing	Easting						
<i>Ash Ponds/Landfill</i>									
MW-14BR	2001	587906.6	730355.4	4540.51	4537.14	72.0	62-72	Silty Sandstone	NAVD88
MW-20B	1982	587906.6	729846.4	4535.47	4534.41	73.0	43.3-73	Silty Sandstone	NGVD29
MW-21B	1982	587358.2	730371.0	4539.58	4538.54	80.0	39.3-79	Sandstone	NGVD29
MW-22B**	1982	587159.1	729587.2	4569.21	4565.87	96.0	66.3-96	Sandstone	NGVD29
MW-23B**	1982	587179.9	728811.2	4569.11	4565.07	90.0	60.2-90	Silty Sandstone	NGVD29
MW-32B	2016	585117.1	726449.5	4569.72	4567.54	75.0	55-75	Sand with Silt	NAVD88
MW-33B	2016	586570.9	726509.5	4569.22	4581.97	89.0	65-85	Sand with Silt	NAVD88
MW-34B	2016	587689.7	726621.3	4557.33	4566.91	89.0	66-86	Sand with Silt	NAVD88
MW-35B	2016	588465.4	726979.2	4551.28	4554.76	90.0	66-86	Silty Sand	NAVD88
MW-36B	2016	589573.8	728145.6	4535.05	4548.80	79.0	58-78	Sand with Silt	NAVD88
MW-37B	2016	589424.0	729236.4	4532.98	4532.87	79.0	57.5-77.5	Sand with Silt	NAVD88
MW-38B	2016	586742.1	730549.7	4550.09	4530.69	88.0	55-75	Sand with Silt	NAVD88
MW-38C	2019	586762.0	730563.0	4549.45	4547.31	130.0	114-125	Sand with Silt	NAVD88
MW-39B	2016	585111.6	729357.3	4584.06	4546.54	109.3	89.3-109.3	Sand with Silt	NAVD88
MW-40B	2016	585540.5	730716.8	4592.20	4590.01	108.0	87.9-107.9	Sand with Silt	NAVD88
MW-48B	2017	587197.1	728402.3	4571.27	4569.39	100.0	80-100	Sand with Silt	NAVD88
MW-49B	2017	587153.4	729978.4	4566.97	NM	100.0	80-100	Sand and Sandstone	NAVD88
MW-50B*	2017/2024	586231.9	728742.5	4593.48	4593.84	120.0	100-120	Sand with Silt	NAVD88
MW-51B*	2017/2024	586215.1	729312.9	4593.14	4393.51	120.0	100-120	Sand with Silt	NAVD88
MW-52B*	2017/2024	586198.0	729809.7	4593.30	4393.65	125.0	104.6-124.6	Sand with Silt	NAVD88
MW-53BR	2024	586183.8	730230.5	4592.89	4593.523	120.0	100-120	Sandstone	NAVD88
MW-54B	2019	590900.5	731071.9	4454.80	4452.16	25.0	12.5-24.5	Sand with Silt	NAVD88
MW-55B	2019	587609.3	730593.4	4532.37	4529.77	70.0	50-70	Sand with Silt	NAVD88
MW-56B	2019	587310.4	731092.3	4541.95	4539.57	79.0	59-79	Sand with Silt	NAVD88
<i>Emergency Holding Ponds</i>									
MW-41B	2016	588577.1	731829.2	4532.25	4529.99	79.0	53-73	Sand with Silt	NAVD88
MW-42B	2016	588829.6	732965.3	4518.44	4515.91	69.0	48.5-68.5	Sand with Silt	NAVD88
MW-43B	2016	589002.8	734274.6	4504.05	4500.61	79.0	58.5-78.5	Sand with Silt	NAVD88
MW-44B	2016	589659.8	731518.4	4532.00	4529.93	99.0	72.1-92.1	Sand with Silt	NAVD88
MW-45B	2016	589851.3	732581.2	4533.53	4531.27	89.0	69-89	Silty Sand	NAVD88
MW-46B	2016	590022.2	733532.2	4530.33	4527.94	94.0	73-93	Sand with Silt	NAVD88
MW-47B	2016	590358.4	734848.3	4525.21	4523.04	89.0	69-89	Silty Sand	NAVD88

Notes:

ft amsl = feet above mean sea level

ft bgs = feet below ground surface

NM = not measured

WY = Wyoming

\* = new surface completions installed in 2024. wells were resurveyed. Ground surface elevation equals top of concrete pad elevation.

\*\* = removed from well network, well damaged during Pond retrofit activities.

1 = Ground surface elevations re-evaluated and updated in 2024.

**Table 4-2: Aquifer Test Results**

Well ID	Test Type	Aquifer Thickness (ft)	Hydraulic Conductivity (ft/day)	Transmissivity (ft <sup>2</sup> /d)
MW-33B	Slug In	16.36	3.80	62.17
	Slug Out		2.27	37.14
MW-35B	Slug In	19.96	3.50	69.86
	Slug Out		1.72	34.33
MW-37B	Slug In	16.14	6.04	97.49
	Slug Out		6.28	101.36
MW-38B	Slug In	15.83	0.99	15.67
	Slug Out		1.09	17.25
MW-39B	Slug In	25.17	0.45	11.33
	Slug Out		0.55	13.84
MW-42B	Slug In	21.62	1.23	26.59
	Slug Out		1.28	27.67
MW-45B	Slug In	12.80	1.27	16.26
	Slug Out		2.35	30.08
MW-47B	Slug In	12.53	1.11	13.91
	Slug Out		1.36	17.04
MW-32B	Pumping	12.59	1.29	16.21
MW-34B	Pumping	16.62	0.65	10.88
MW-36B	Pumping	14.97	2.42	36.22
MW-40B	Pumping	11.39	0.79	8.99
MW-41B	Pumping	15.03	3.12	46.84
MW-43B	Pumping	20.00	0.75	14.90
MW-44B	Pumping	19.69	1.40	27.59
MW-46B	Pumping	17.10	0.76	13.00

## Notes:

ft = feet

ft/day = feet per day

ft<sup>2</sup>/d = squared feet per day

ID = Identification

**Table 5-1: Groundwater Elevations - June 4-5, 2024**

Location ID	Date Gauged	TOC Elevation (ft amsl)	Depth to Water (TOC ft)	Water Level Elevation (ft amsl)
MW-14BR	6/5/2024	4540.51	55.45	4,485.06
MW-20B	6/5/2024	4535.47	58.05	4,477.42
MW-21B	6/5/2024	4539.58	52.15	4,487.430
MW-32B	6/5/2024	4569.72	55.95	4,513.77
MW-33B	6/5/2024	4569.22	66.11	4,503.11
MW-34B	6/5/2024	4557.33	63.00	4,494.33
MW-35B	6/5/2024	4551.28	63.19	4,488.09
MW-36B	6/5/2024	4535.05	59.44	4,475.61
MW-37B	6/5/2024	4532.98	61.66	4,471.32
MW-38B	6/5/2024	4550.09	56.40	4,493.69
MW-38C	6/5/2024	4549.45	55.70	4,493.75
MW-39B	6/5/2024	4584.06	76.72	4,507.34
MW-40B	6/5/2024	4592.20	90.70	4,501.50
MW-41B	6/4/2024	4532.25	55.05	4,477.20
MW-42B	6/4/2024	4518.44	45.45	4,472.99
MW-43B	6/4/2024	4504.05	32.30	4,471.75
MW-44B	6/4/2024	4532.00	70.30	4,461.70
MW-45B	6/4/2024	4533.53	76.90	4,456.63
MW-46B	6/5/2024	4530.33	76.45	4,453.88
MW-47B	6/4/2024	4525.21	76.20	4,449.01
MW-48B	6/5/2024	4571.27	77.00	4,494.27
MW-49B	6/5/2024	4566.97	76.10	4,490.87
MW-50B	6/5/2024	4593.48	92.00	4,501.48
MW-51B	6/5/2024	4593.14	92.61	4,500.53
MW-52B	6/5/2024	4593.30	93.72	4,499.58
MW-53BR*	6/5/2024	4592.89	94.32	4,498.57
MW-54B	6/5/2024	4454.80	7.02	4,447.78
MW-55B	6/5/2024	4532.37	45.20	4,487.17
MW-56B	6/5/2024	4541.95	53.11	4,488.84

**Notes:**

TOC = top of casing

ft amsl = feet above mean sea level

ID = Identification

NM<sup>1</sup> = Not Measured - Well Not Found

NM = Not Measured

\* = MW-53B replaced with MW-53BR in April 2024

Vertical Datum: North American Vertical Datum of 1988 (NAVD 88)

**Table 5-2: Groundwater Elevations - September 26-27, 2024**

Location ID	Date Gauged	TOC Elevation (ft amsl)	Depth to Water (TOC ft)	Water Level Elevation (ft amsl)
MW-14BR	9/26/24 - 9/27/24	4540.51	56.40	4,484.11
MW-20B	9/26/24 - 9/27/24	4535.47	58.60	4,476.87
MW-21B	9/26/24 - 9/27/24	4539.58	53.80	4,485.780
MW-32B	9/26/24 - 9/27/24	4569.72	59.00	4,510.72
MW-33B	9/26/24 - 9/27/24	4569.22	68.91	4,500.31
MW-34B	9/26/24 - 9/27/24	4557.33	66.20	4,491.13
MW-35B	9/26/24 - 9/27/24	4551.28	66.00	4,485.28
MW-36B	9/26/24 - 9/27/24	4535.05	60.15	4,474.90
MW-37B	9/26/24 - 9/27/24	4532.98	61.11	4,471.87
MW-38B	9/26/24 - 9/27/24	4550.09	57.70	4,492.39
MW-38C	9/26/24 - 9/27/24	4549.45	57.07	4,492.38
MW-39B	9/26/24 - 9/27/24	4584.06	77.67	4,506.39
MW-40B	9/26/24 - 9/27/24	4592.20	91.40	4,500.80
MW-41B	9/26/24 - 9/27/24	4532.25	55.50	4,476.75
MW-42B	9/26/24 - 9/27/24	4518.44	45.45	4,472.99
MW-43B	9/26/24 - 9/27/24	4504.05	27.45	4,476.60
MW-44B	9/26/24 - 9/27/24	4532.00	71.11	4,460.89
MW-45B	9/26/24 - 9/27/24	4533.53	77.62	4,455.91
MW-46B	9/26/24 - 9/27/24	4530.33	77.25	4,453.08
MW-47B	9/26/24 - 9/27/24	4525.21	76.70	4,448.51
MW-48B	9/26/24 - 9/27/24	4571.27	77.60	4,493.67
MW-49B	9/26/24 - 9/27/24	4566.97	76.60	4,490.37
MW-50B	9/26/24 - 9/27/24	4593.48	92.55	4,500.93
MW-51B	9/26/24 - 9/27/24	4593.14	93.20	4,499.94
MW-52B	9/26/24 - 9/27/24	4593.30	94.40	4,498.90
MW-53BR*	9/26/24 - 9/27/24	4592.89	95.20	4,497.69
MW-54B	9/26/24 - 9/27/24	4454.80	8.22	4,446.58
MW-55B	9/26/24 - 9/27/24	4532.37	46.60	4,485.77
MW-56B	9/26/24 - 9/27/24	4541.95	53.90	4,488.05

Notes:

TOC = top of casing

ft amsl = feet above mean sea level

ID = Identification

NM<sup>1</sup> = Not Measured - Well Not Found

NM = Not Measured

\* = MW-53B replaced with MW-53BR in April 2024

Vertical Datum: North American Vertical Datum of 1988 (NAVD 88)

**Table 6-1: Proposed Statistical Methods for Appendix III Constituents in Background Wells**

CCR Unit/Multi-unit	Background Wells	Statistical Method	Constituents
Ash Pond 1	MW-52B, MW-53B	Parametric Prediction Interval	Boron, Calcium, Fluoride, pH
	MW-52B, MW-53B	Nonparametric Prediction Interval	Chloride, Sulfate, Total Dissolved Solids
Ash Pond 2, Ash Pond 3, Ash Landfill Multi-unit	MW-32B, MW-39B	Parametric Prediction Interval	Boron, Calcium, Fluoride, pH
	MW-32B, MW-39B	Nonparametric Prediction Interval	Chloride, Sulfate, Total Dissolved Solids
Emergency Holding Ponds Multi-unit	MW-41B, MW-42B, MW-43B	Parametric Prediction Interval	Calcium
	MW-41B, MW-42B, MW-43B	Nonparametric Prediction Interval	Boron, Chloride, Fluoride, pH, Sulfate, Total Dissolved Solids

Note:  
CCR = Coal Combustion Residuals

# Appendix A

## Boring Logs and Well Construction Diagrams



**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 7/19/2016 **COMPLETED** 7/20/2016 **GROUND ELEVATION** 4564.93 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** ---  
**LOGGED BY** Matt Hartz **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 4567.106 N 4564.93 E **12hrs AFTER DRILLING** 58.35 ft / Elev 4506.58 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 2.176 (ft) Casing Type: 2" PVC Pipe
0 - 6.0	N/A	0				Hand potholed until 6' bgs	Top of Casing (2.176' ags)
6.0 - 13.0	SONIC 1	100		SW		SAND, very fine to coarse-grained, some silt, some gravel and pebble, lightly weathered to weathered; loose, dry, light gray-brown Minerology consists primarily of granite clasts (qtz, k-spar, lithies)	Grout (0' - 47' bgs)
13.0 - 20.0	SONIC 2	100		SW		S.A.A., moist	PVC Pipe (2.176' ags - 75' bgs)

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 10/10/16 15:00 - C:\BISMARCK GINTLRS - 60506860 2.01\LRS\_091516.GPJ

CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
20							
20.5				SW		20.5 4544.4 SAND, very fine to fine-grained, subround, some silt, massive/no apparent bedding; firm to stiff, predominantly dry with moist intervals (typically on top of SS Caliche horizons), light brown	
25	SONIC 3	100		SP		@28-29' bgs: light gray SS Caliche, hard, well cemented	
30	SONIC 4	100				@30-33' bgs: intervals of very stiff (nearly SS), intervals contained calcium carbonate stringers and nodules (cemented sands)	Grout (0' - 47' bgs)
33.0						33.0 4531.9 SANDSTONE, very fine to fine-grained, some silt, well indurated, laminae of Caliche silts and clays, interbeds of dense unconsolidated sands (same as 30-33' bgs interval); hard, moist, light gray-brown	
35	SONIC 5	100		SANDSTONE			
38.0						38.0 4526.9 SAND, very fine to fine-grained, subround, some silt, trace clay, very thin beds (appear as chips in core) of calcareous, cemented sands; loose, dry to moist, light gray-brown	PVC Pipe (2.176' ags - 75' bgs)
40	SONIC 6	100		SP		@39-42' bgs: color change from light gray-brown to brown	

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 10/10/16 15:00 - C:\BISMARCK GINTLRS - 60506860 2.01\LRS\_091516.GPJ

CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
45	SONIC 7	100				SAND, poorly graded, subround, some silt, trace clay, very thin beds (appear as chips in core) of calcareous, cemented sands; loose, dry to moist, brown @43-49' bgs: dry	
50						@49-56' bgs: moist	
55	SONIC 8	100		SP			
60	SONIC 9	100				@56.5-57.5' bgs: 1' of SS Caliche, well cemented; very dense, moist on top and bottom of interval	
65	SONIC 10	100				▼ @59-60' bgs: wet to saturated	

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 10/10/16 15:00 - C:\BISMARCK GINTLRS - 60506860 2.01\LRS\_091516.GPJ

CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
70	SONIC 11	100				SAND, poorly graded, subround, some silt, trace clay, very thin beds (appear as chips in core) of calcareous, cemented sands; loose, wet to saturated, brown  @71-75' bgs: medium-grained sand, interbedded zones (<6"); saturated	<p>10/20 Silica Sandpack (52' - 75' bgs)</p> <p>0.010 Slotted Pipe (55' - 75' bgs)</p>
75	SONIC 12	100		SP	75.0		

Bottom of borehole at 75.0 feet.

4489.9  
 Total Depth of Well 75' bgs

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 7/20/2016 **COMPLETED** 7/20/2016 **GROUND ELEVATION** 4579.362 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** ---  
**LOGGED BY** Matt Hartz **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 4566.607 N 4564.303 E **▼ AFTER DRILLING** 68.21 ft / Elev 4511.15 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 2.304 (ft) Casing Type: 2" PVC Pipe
0 - 6.0	N/A	0				Hand potholed until 6' bgs	Top of Casing (2.304' ags)
6.0 - 15.0	SONIC 1 SONIC 2	100 100		SM		6.0 4573.4 SILTY SAND, very fine to medium-grained, subround to subangular, some gravel and pebbles, lightly weathered; loose, dry  Pebbles consist primarily of granite clasts; sand composed of weathered granite fragments	Grout (0' - 57.7' bgs) PVC Pipe (2.304' ags - 85' bgs)
15.0 - 21.0	SONIC 3	100		SP		15.0 4564.4 SAND, fine to medium-grained, subround, some silt, lenses (<1") of coarse-grained sand, lightly to moderately weathered; loose, dry to moist, brown	
21.0 - 25.0	SONIC 4	100		SP		21.0 4558.4 SAND, very fine to fine-grained, subround, some silt, unweathered, laminae or concretions (<.5") of calcium carbonate, trace small (5 mm) clasts of clay and SS Caliche; firm to stiff, moist, brown	

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
25							
25 - 30	SONIC 5	100		SP		SAND, very fine to fine-grained, subround, some silt, unweathered, laminae or concretions (<.5") of calcium carbonate, trace small (5 mm) clasts of clay and SS Caliche; firm to stiff, moist, brown	<p>Grout (0' - 57.7' bgs)</p> <p>PVC Pipe (2.304' ags - 85' bgs)</p>
30 - 35	SONIC 6	100		CALICHE		31.0 CALICHE SAND, very fine to fine-grained, well cemented, well indurated, calcarious; very hard, dry, light gray to white 4548.4	
35 - 40	SONIC 7	100		SP		35.5 SAND, poorly graded, subround, some silt, trace clay, no apparent bedding but tends to break along irregular planes (horizontal), small pockets of weathered silt and sand; loose to firm, dry, brown 4543.9	
40 - 45	SONIC 8	100		SP		40.0 SAND, poorly graded, subround, some silt, trace clay, no apparent bedding but tends to break along irregular planes (horizontal), small pockets of weathered silt and sand; loose to firm, dry, brown 4539.4	
45 - 50	SONIC 9	100		SP		@43' bgs: moist on top of thin Caliche interbed (<1") @44-47' bgs: interbeds of uncemented, well indurated SS (same description as formation interbeds, no thicker than 1"); hard	
50 - 55	SONIC 10	100				@53-54' bgs: Caliche SS, well cemented and indurated; very hard, light gray	

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
55	SONIC 11	100		SP		SAND, poorly graded, subround, some silt, trace clay, no apparent bedding but tends to break along irregular planes (horizontal), small pockets of weathered silt and sand; loose to firm, dry, brown @55-58' bgs: increase in SS interbeds (not Caliche), well indurated; hard, brown	<p>Grout (0' - 57.7' bgs)                      PVC Pipe (2.304' ags - 85' bgs)</p>
60	SONIC 12	80				SAND, poorly graded, subround, some silt, contains thin beds (<2") of SS and zones (1" - 1' thick) of SS Caliche; loose, dry to moist  @63-64' bgs: just below a Caliche horizon, moist @64-69' bgs: firm, moist	<p>3/8" Bentonite Chips (55.4' - 61.5' bgs)</p>
65	SONIC 13	100				@69-77.5' bgs: wet to saturated (moisture decreases just below 77.5' bgs)	<p>10/20 Silica Sandpack (62' - 85' bgs)</p>
70				SP		@79-89' bgs: wet	<p>0.010 Slotted Pipe (65' - 85' bgs)</p>
75	SONIC 14	100					
80							

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
85	SONIC 15	100		SP		SAND, poorly graded, subround, some silt, contains thin beds (<2") of SS and zones (1" - 1' thick) of SS Caliche; loose, wet	<ul style="list-style-type: none"> <li>10/20 Silica Sandpack (62' - 85' bgs)</li> <li>0.010 Slotted Pipe (65' - 85' bgs)</li> <li>Total Depth of Well 85' bgs</li> <li>Native Clay Below Well - Natural Collapse</li> </ul>
					89.0	Bottom of borehole at 89.0 feet.	4490.4

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 7/24/2016 **COMPLETED** 7/24/2016 **GROUND ELEVATION** 4564.303 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** ---  
**LOGGED BY** Matt Hartz **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 4554.72 N 4552.152 E **▼ AFTER DRILLING** 68.71 ft / Elev 4495.59 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 2.568 (ft) Casing Type: 2" PVC Pipe
0 - 6.0	N/A	0				Hand potholed until 6' bgs	Top of Casing (2.568' ags)
6.0 - 9.0	SONIC 1	100		SP		SAND, very fine to fine-grained, subround, some silt, trace gravel and pebbles; loose, dry, light brown	
9.0 - 16.0	SONIC 2	100		FILL		FILL, sand, gravel, pebbles, and cobbles, angular to subangular; loose, dry, light gray	Grout (0' - 55.4' bgs) PVC Pipe (2.568' ags - 86' bgs)
16.0 - 25.5	SONIC 3	100		SP		SAND, very fine to fine-grained, subround, some silt, no apparent bedding, interbedded SS (<1"), unweathered; loose to firm and firm to stiff at depth, dry, light brown @17-18' bgs: silt interbed, light gray	
25.5 - 25	SONIC 4	100		SP		@24-25.5' bgs: slight moisture increase just above SS interbed (perched, not holding significant water year-round)	

(Continued Next Page)

CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
25	SONIC 5	100				SAND, very fine to fine-grained, subround, some silt, no apparent bedding, interbedded SS (<1"), unweathered; loose to firm and firm to stiff at depth, dry, light brown	<p>Grout (0' - 55.4' bgs)</p> <p>PVC Pipe (2.568' ags - 86' bgs)</p>
30	SONIC 6	100				@30-36' bgs: SS beds increase in frequency; firm to stiff	
35	SONIC 7	100					
40	SONIC 8	100		SP		@39-44' bgs: moisture content increases above stiff sand interval	
45	SONIC 9	100				@46-50' bgs: thin SS interbed above zone of saturation; wet to saturated	
50	SONIC 10	100				@53-54' bgs: SS interbed, cemented, possibly Caliche; hard, dry, light gray	

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 10/10/16 15:02 - C:\BISMARCK GINTLRS - 60506860 2.01\LRS\_091516.GPJ




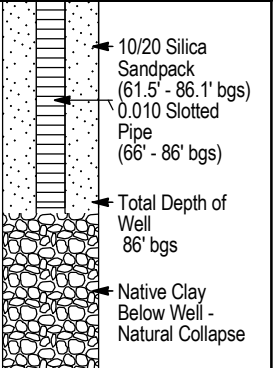
CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
55	SONIC 11	100		SP		SAND, fine-grained, subround, some silt, no SS beds; loose, moist, light brown to brown	<ul style="list-style-type: none"> <li>Grout (0' - 55.4' bgs)</li> <li>PVC Pipe (2.568' ags - 86' bgs)</li> <li>3/8" Bentonite Chips (55.4' - 61.5' bgs)</li> <li>10/20 Silica Sandpack (61.5' - 86.1' bgs)</li> <li>0.010 Slotted Pipe (66' - 86' bgs)</li> </ul>
60	SONIC 12	80		SP		SAND, fine-grained, subround, some silt, no SS beds; loose, moist, light brown to brown tends to break along irregular bedding planes (<1")	
65	SONIC 13	100		SP		@69-79' bgs: lightly weathered between bedding panes; zones of saturation  @74-76' bgs: laminae of well compacted, dense, stiff SS	
70	SONIC 14	100		SP		@79-89' bgs: saturated	
75	SONIC 15	100		SP			
80							

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CLIENT Basin Electric PROJECT NAME Laramie River Station

PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
85	SONIC 16	100		SP		SAND, fine-grained, subround, some silt, no SS beds; loose, saturated, light brown to brown tends to break along irregular bedding planes (<1")	 <ul style="list-style-type: none"> <li>← 10/20 Silica Sandpack (61.5' - 86.1' bgs)</li> <li>← 0.010 Slotted Pipe (66' - 86' bgs)</li> <li>← Total Depth of Well 86' bgs</li> <li>← Native Clay Below Well - Natural Collapse</li> </ul>

89.0

4475.3

Bottom of borehole at 89.0 feet.

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 7/31/2016 **COMPLETED** 8/1/2016 **GROUND ELEVATION** 4552.152 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** ---  
**LOGGED BY** Chris Ahrendt **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 4548.665 N 4546.185 E **▼ AFTER DRILLING** 63.70 ft / Elev 4488.45 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 2.48 (ft) Casing Type: 2" PVC Pipe
						Hand potholed until 6' bgs	Top of Casing (2.480' ags)
5	N/A	0					
	SONIC 1	100		SP-GP		6.0 4546.2	
	SONIC 2	75		SP-GP		9.0 4543.2	
	SONIC 3	80		SP-GP		11.0 4541.2	
				SP		14.4 4537.8	
				SW		15.1 4537.1	
	SONIC 4	76				19.0 4533.2	Grout (0' - 59.5' bgs)
				SM		20.4 4531.8	
	SONIC 5	100		ML		24.0 4528.2	PVC Pipe (2.480' ags - 86' bgs)
25				ML			

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

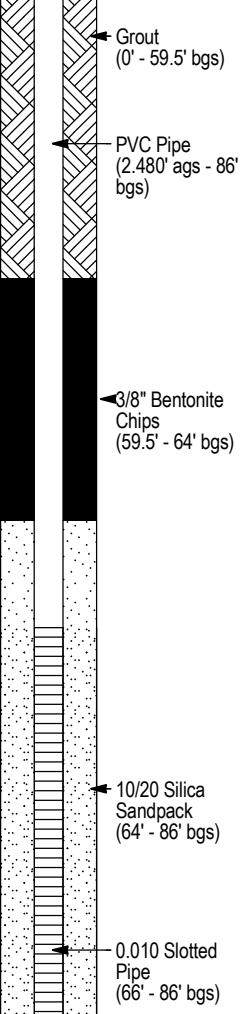
DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
25							
	SONIC 6	100		ML		SILT, noncohesive, nonplastic, no oxidation or staining or odor; very soft, moist, pale brown (10YR 6/3)	
						27.0 4525.2	
				ML		SILT, trace very fine sand, noncohesive, nonplastic, no oxidation or staining or odor, blocky structures (1") that break in hand; very stiff, moist, dark gray (10YR 4/1)	
30						30.0 4522.2	
	SONIC 7	100		SM		SILTY SAND, very fine to fine-grained, slow dilatancy, no odor or staining; soft, wet, dark yellowish brown @30-35' bgs: perched aquifer	
35						34.7 4517.5	
						35.0 SANDSTONE, no odor or staining; hard, dry	
				ML		SANDY SILT, with gravel, slow dilatancy, noncohesive, nonplastic, no odor or staining; very soft, wet, gray (10YR 5/1)	
	SONIC 8	100		ML		SILT, with gravel (15% subangular sandstone), noncohesive, nonplastic; loose, dry, white (10YR 6/1)	
						36.2 4516.0	
						38.3 4513.9	
				SP		SAND, poorly graded, little fines, with thinly bedded sandstone lenses (.5"-1"), no odor or staining; loose, dry, pale brown (10YR 6/3)	
40						39.0 4513.2	
				SM		SILTY SAND, very fine to fine-grained, slow dilatancy, no odor or staining; medium dense, wet (perched aquifer), brown (10YR 5/3)	
	SONIC 9	100				41.5 4510.7	
				SM		S.A.A., 10% of 3/4"-1" blocky sandstone; moist, light gray (10YR 7/2)	
						44.0 4508.2	
45						SAND, very fine to fine-grained, with silt, with 3/4"-1" hard sandstone, no odor or staining; loose, moist, brown	
				SP-SM		46.1 4506.1	
	SONIC 10	100		SM		SILTY SAND, very fine to fine-grained; very hard, moist, dark gray	
						46.4 4505.8	
						SAND, very fine to fine-grained, with silt, with 3/4"-1" hard sandstone, no odor or staining; loose, moist, brown	
50						@49-50.1' bgs: 1" hard fragments of sandstone; wet (due to drilling waters)	
	SONIC 11	94		SP			

Grout (0' - 59.5' bgs)  
 PVC Pipe (2.480' ags - 86' bgs)

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 10/10/16 15:41 - C:\BISMARCK\GINTLRS - 60506860 2.01\LRS\_091516.GPJ

CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
55	SONIC 12	100		SP		54.0 SAND, very fine to fine-grained, with silt, no odor or staining; medium dense, wet, yellowish brown (10YR 5/4), mottled dark gray (10YR 4/1)	4498.2
				55.7 SAND, very fine to fine-grained; medium dense, moist, light brownish gray (10YR 6/1)		4496.5	
				57.1 SANDY SILT, slow dilatancy, noncohesive, nonplastic; soft, wet, grayish brown, mottled very dark gray (10YR 5/1)		4494.2	
60	SONIC 13	70		ML		58.0 SILTY SAND, very fine to fine-grained; medium dense, wet, grayish brown (10YR 5/2)	4491.7
				60.5 S.A.A., soft, decreasing in moisture		4488.2	
65	SONIC 14	100		SP-SM		64.0 SAND, very fine to fine-grained, with silt; soft, wet, brown (10YR 5/3)	4486.5
				65.7 SILTSTONE, massive, blocky; hard, moist, brown (10YR 4/3)		4485.2	
				67.0 S.A.A., brown (10YR 5/3)		4481.2	
70	SONIC 15	100		SILTSTONE		71.0 SAND, very fine to fine-grained, with silt; soft, wet, brown (10YR 5/3)	4480.2
				72.0 SILTY SAND; stiff, moist, brown		4479.7	
75	SONIC 16	100		SANDSTONE		72.5 SANDSTONE, some hard sand; loose, white and tan	4478.2
				74.0 SILTY SAND, very fine to fine-grained; medium dense, moist, brown		4477.2	
				75.0 S.A.A., moist		4475.2	
				77.0 SILTY SAND, very fine to fine-grained, slow dilatancy; soft, wet, brown		4473.9	
				78.3 S.A.A., medium dense, moist		4473.2	
80	SONIC 17	74		SM		79.0 S.A.A., stiff	4473.2
				ML		SANDY SILT, noncohesive, nonplastic, massive, slow dilatancy; very soft, wet, grayish brown	



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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
85	SONIC 18	75		ML		SANDY SILT, noncohesive, nonplastic, massive, slow dilatancy; very soft, wet, grayish brown	
90				SM		SILTY SAND, very fine to fine-grained, slow dilatancy, no odor or staining; loose, wet, brown  Note: drillers drilled to 89', but all of it fell back into the hole because outer casing was not used.	

Bottom of borehole at 90.0 feet.

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 8/1/2016 **COMPLETED** 8/2/2016 **GROUND ELEVATION** 4546.185 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** 35.96 ft / Elev 4510.23 ft  
**LOGGED BY** Chris Ahrendt **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 4532.438 N 4530.256 E **AFTER DRILLING** 59.35 ft / Elev 4486.84 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0						Hand potholed until 5' bgs	Casing Top Elev: 2.182 (ft) Casing Type: 2" PVC Pipe
5	N/A	0					Top of Casing (2.182' aqs)
5.0	SONIC 1	100		SW-GP		SAND, fine to coarse-grained, with gravel, no odor or staining; loose, moist brown	
9.0						S.A.A., increasing gravel content, subround; too hot for sleeves	Grout (0' - 51.5' bgs)
9.0	SONIC 2	100		SW-GP			
14.0						SILTY SAND, very fine to fine-grained, no odor or staining; loose, moist, brown (10YR 5/3)	PVC Pipe (2.182' aqs - 78' bgs)
14.0	SONIC 3	96		SM			
17.8						GRAVEL, poorly graded, subround (1-2"), little clay, little sand, no odor or staining; loose, moist to wet, brown	
17.8				GP			
19.0						SILTY SAND, very fine to fine-grained, trace gravel, no odor or staining; loose, moist, brown (10YR 5/3)	
19.0				SM			
20							

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
20							
	SONIC 4	94		SM		SILTY SAND, very fine to fine-grained, trace gravel, no odor or staining; loose, moist, brown (10YR 5/3)	
						24.0	4522.2
						S.A.A., little gravel	
25							
	SONIC 5	98		SM			
						29.0	4517.2
						SANDY SILT, noncohesive, nonplastic, blocky, no staining; very soft, moist, dark grayish brown (10YR 4/2)	
30							
	SONIC 6	100		ML			
						32.0	4514.2
						SANDSTONE, broken; dry to moist, white and tan	
						32.8	4513.4
						SILTY SAND, very fine to fine-grained, little gravel, no odor or staining; medium dense, moist, pale brown (10YR 6/3)	
						34.0	4512.2
						SANDY SILT, noncohesive, nonplastic, massive; medium dense, moist, brown (10YR 4/3)	
35							
	SONIC 7	100	0.75	ML			
						35.2	4511.0
						SILTY SAND, very fine to fine-grained, no odor or staining; loose, moist, brown	
						37.2	4509.0
						37.4	4508.8
						SILT, with sand, trace gravel, noncohesive, nonplastic, no odor or staining; soft, wet, brown	
						SANDSTONE, with wet silt in between bedding, noncohesive, nonplastic; hard, moist to wet, brownish gray	
						39.0	4507.2
						SILT, noncohesive, nonplastic, blocky, no oxidation; hard, moist, brown	
40							
	SONIC 8	69		ML			
						40.0	4506.2
						SILTY SAND, very fine to fine-grained, trace gravel; hard, moist, brown	

Grout (0' - 51.5' bgs)  
 PVC Pipe (2.182' ags - 78' bgs)

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM	
45	SONIC 9	100		SM		SILTY SAND, very fine to fine-grained, trace gravel; hard, moist, brown		
				44.0		4502.2		S.A.A., increasing in moisture
50	SONIC 10	100	2.5	SM		SAND, very fine to fine-grained, with silt, no odor or staining; very stiff, moist, grayish brown (10YR 5/2)		
				49.0		4497.2		S.A.A., loose, pale brown (10YR 4/3)
				50.7		4495.5		S.A.A., loose, pale brown (10YR 4/3)
55	SONIC 11	0	>4.0	SP-SM		SAND, very fine to fine-grained, with silt; moist, light brown @57.6' bgs: increasing in moisture and fines		
				53.0		4493.2		S.A.A., blocky; hard, grayish brown (10YR 5/2)
60	SONIC 12	100		SP-SM		SAND, very fine to fine-grained, with silt; soft, wet, yellowish brown		
				55.7		4490.5		SAND, very fine to fine-grained, with silt; moist, light brown @57.6' bgs: increasing in moisture and fines
65	SONIC 12	100		SP-SM		SAND, very fine to fine-grained, with silt; soft, wet, yellowish brown		
				59.0		4487.2		10/20 Silica Sandpack (56' - 78' bgs)
				61.3		4484.9		0.010 Slotted Pipe (58' - 78' bgs)
				62.3		4483.9		SANDY SILT, noncohesive, nonplastic, massive; hard, moist, brown
65	SONIC 12	100		SM		SILTY SAND, very fine-grained; soft, moist to wet, yellowish brown		
				64.0		4482.2		SAND, very fine to fine-grained, some silt, slow dilatancy; medium dense, wet, yellowish brown

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM	
70	SONIC 13	98		SP		SAND, very fine to fine-grained, some silt, slow dilatancy; medium dense, wet, yellowish brown	<p>10/20 Silica Sandpack (56' - 78' bgs)</p> <p>0.010 Slotted Pipe (58' - 78' bgs)</p>	
72.3				4473.9	ML			SILT, noncohesive, nonplastic; soft, wet, gray
73.1				4473.1	SP			SAND, very fine to fine-grained, some silt, slow dilatancy; medium soft, wet, grayish brown
74.0				4472.2	SP			S.A.A., little silt; yellowish brown
75				SP		S.A.A., little silt; yellowish brown	<p>Total Depth of Well 78' bgs</p> <p>Native Clay Below Well - Natural Collapse</p>	
79.0						4467.2		

Bottom of borehole at 79.0 feet.

LGE GHENT SOIL-WELL LOG - GHENT\_GDT - 10/10/16 15:04 - C:\BISMARCK GINTLRS - 60506860 2.01\LRS\_091516.GPJ

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 8/2/2016 **COMPLETED** 8/3/2016 **GROUND ELEVATION** 4530.256 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** 68.00 ft / Elev 4462.26 ft  
**LOGGED BY** Chris Ahrendt **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 4530.367 N 4528.075 E **AFTER DRILLING** ---

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 2.292 (ft) Casing Type: 2" PVC Pipe
						Hand potholed until 5.5' bgs	Top of Casing (2.292' aqs)
5	N/A	0					
	SONIC 1	100		SP-GP		5.5 4524.8 SAND, very fine to medium-grained, with gravel, no odor or staining; loose, moist, brown	
10	SONIC 2	98		SW-GP		9.0 4521.3 SAND, very fine to coarse-grained, with subround gravel, no odor or staining; loose, moist, brown	Grout (0' - 50' bgs)
				GP		11.8 4518.5 GRAVEL, poorly graded, subangular, with fine to coarse-grained sand, trace fines, no odor or staining; loose, moist, tan	PVC Pipe (2.292' aqs - 77.5' bgs)
				ML		12.6 4517.7 SANDY SILT, noncohesive, nonplastic, no odor or staining; loose, moist, light brown	
15	SONIC 3	98		SM		14.0 4516.3 SILTY SAND, very fine-grained, trace fine grained sand, no odor or staining; loose, moist, light brown	
20						20.0 4510.3	

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
20							
	SONIC 4	100		SM		SILTY SAND, very fine-grained; loose, moist, brown	<p>Grout (0' - 50' bgs)</p> <p>PVC Pipe (2.292' ags - 77.5' bgs)</p>
					21.7	4508.6	
				ML		SILT, little sand, noncohesive, nonplastic, blocky, no odor or staining; hard, moist, pale brown	
					24.0	4506.3	
25				ML		SANDY SILT, noncohesive, nonplastic, no odor or staining, blocky; soft, moist, brown	
	SONIC 5	100			27.0	4503.3	
				ML		S.A.A., slow dilatancy; wet (perched)	
					29.0	4501.3	
30				SM		SILTY SAND, very fine to fine-grained, no odor or staining; loose, wet (due to drilling waters), brown	
					30.0	4500.3	
	SONIC 6	94		SM		S.A.A., moist	
					32.9	4497.4	
				SM		S.A.A., blocky; hard	
					34.0	4496.3	
35				ML		SILT, with sand, noncohesive, nonplastic, slow dilatancy; soft, wet, grayish brown (10YR 5/2), mottled gray (10YR 5/1)	
					35.5	4494.8	
	SONIC 7	100		SM		SILTY SAND, very fine to fine-grained, no odor or staining; soft, wet, brown	
					37.3	4493.0	
				SM		S.A.A., decreasing moisture	
					39.0	4491.3	
40				SM		SILTY SAND, very fine to fine-grained, no staining; loose, moist, brown	
	SONIC 8	100					

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
45	SONIC 9	100		SM		SILTY SAND, very fine to fine-grained, no staining; loose, moist, brown	Grout (0' - 50' bgs)
				SW	45.0 - 45.4	SAND, very fine to coarse-grained, with round gravel, no odor or staining; loose, wet (due to drilling waters), brown	
	SONIC 10	100	1.25	SM		SILTY SAND, very fine to fine-grained, no odor or staining; loose, moist, brown	PVC Pipe (2.292' ags - 77.5' bgs)
				SP	49.0 - 51.0	SAND, very fine to fine-grained, little silt; stiff, moist, brown S.A.A., loose	
50	SONIC 11	88		SP		SAND, very fine to fine-grained, with silt, no odor or staining; loose, moist, brown	3/8" Bentonite Chips (50' - 54' bgs)
				SP-SM	51.0 - 54.0	S.A.A., moist	
55	SONIC 12	48		SM		SAND, very fine to fine-grained, with silt; loose, moist, yellowish brown	10/20 Silica Sandpack (54' - 77.5' bgs)
				SM	56.0 - 56.9	S.A.A., slow dilatancy; wet	
60				SP-SM		SAND, very fine to fine-grained, with silt; loose, moist, yellowish brown	0.010 Slotted Pipe (57.5' - 77.5' bgs)
				SP-SM	59.6 - 62.0	S.A.A., slow dilatancy; wet	
65							

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
			2.0			66.2 - 4464.1 SILTY SAND, very fine to fine-grained; stiff, moist, yellowish brown	<p>10/20 Silica Sandpack (54' - 77.5' bgs)</p> <p>0.010 Slotted Pipe (57.5' - 77.5' bgs)</p> <p>Total Depth of Well 77.5' bgs</p> <p>Native Clay Below Well - Natural Collapse</p>
				SM		68.0 ▽ - 4462.3 SAND, very fine to fine-grained, with silt, slow dilatancy; loose, wet, yellowish brown	
				SP-SM		69.0 - 4461.3 No recovery	
70							
	SONIC 13	43					
75							
						76.3 - 4454.0 SAND, very fine to fine-grained, with silt; loose, wet, grayish brown	
				SP-SM			
						77.9 - 4452.4	
				ML		78.4 - 4451.9 SANDY SILT, noncohesive, nonplastic, no odor or staining; soft, wet, gray	
				SM		79.0 - 4451.3 SILTY SAND, very fine-grained, no odor or staining; soft, wet, gray	
						Bottom of borehole at 79.0 feet.	

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 7/14/2016 **COMPLETED** 7/14/2016 **GROUND ELEVATION** 4528.075 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** ---  
**LOGGED BY** Matt Hartz **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 4547.479 N 4544.695 E **▼ AFTER DRILLING** 56.90 ft / Elev 4471.18 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 2.784 (ft) Casing Type: 2" PVC Pipe
0 - 5	N/A	0				Hand potholed until 5' bgs	Top of Casing (2.784' ags)
5.0						4523.1	
5 - 9				SP		SAND, very fine to fine-grained, subround, some silt, trace clay; loose, moist, light brown Thin beds of medium to coarse-grained sand (k-spar, qtz, minor lithies) loosely cemented	
9.0						4519.1	
9 - 15	SONIC 1	100		FILL		FILL, fine to coarse grained sand, with gravel and cobbles Mixed lithologies throughout	Grout (0' - 62' bgs) PVC Pipe (2.874' ags - 75' bgs)
15						4511.1	
15 - 17	SONIC 2	100					
17.0				SM		SILTY SAND, very fine to fine-grained, round; loose, moist to dry, light brown	
20.0						4508.1	
20 - 25	SONIC 3	100		SM		SILTY SAND, very fine to fine-grained, round; loose, moist to dry, light brown @21.5-25' bgs: thinly bedded sandstone with sand matrix, loosely cemented	
25							

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
25							
30							
35	SONIC 4	100					
40				SM			
45	SONIC 5	100					
50							
	SONIC 6	100					

SILTY SAND, very fine to fine-grained, round; loose, moist to dry, light brown

@40-47' bgs: increase in overall competency of sand, thin beds of loosely consolidated sandstone

Grout (0' - 49.6' bgs)

PVC Pipe (2.874' ags - 75' bgs)

3/8" Bentonite Chips (49.6' - 52.9' bgs)

10/20 Silica Sandpack

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
55				SM		SILTY SAND, very fine to fine-grained, round; loose, moist to dry, light brown  @56' bgs: increase in moisture content  @57-57.5': well-graded, competent SS, cemented (likely calcareous); dense, white	<p>(52.9' - 76.4' bgs)</p> <p>10/20 Silica Sandpack (52.9' - 76.4' bgs) 0.010 Slotted Pipe (55' - 75' bgs)</p> <p>Total Depth of Well 75' bgs</p> <p>Bentonite Chip Fill Below Well</p>
60					60.0	SILTY SAND, very fine to fine-grained, round, slightly more competent zones/beds of moderately cemented SS; loose, moist, light brown to brown  intervals with increasing moisture	
65	SONIC 7	100					
70				SM			
75	SONIC 8	100					
80							

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
85	SONIC 9	100		SM		SILTY SAND, very fine to fine-grained, round, slightly more competent zones/beds of moderately cemented SS; loose, moist, light brown to brown  intervals with increasing moisture	
					88.0		4440.1

Bentonite Chip Fill Below Well

Bottom of borehole at 88.0 feet.

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 7/17/2016 **COMPLETED** 7/18/2016 **GROUND ELEVATION** 4544.695 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** ---  
**LOGGED BY** Matt Hartz **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 4581.452 N 4579.362 E **▼ AFTER DRILLING** 78.30 ft / Elev 4466.40 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 2.09 (ft) Casing Type: 2" PVC Pipe
0 - 6.0	N/A	0				Hand potholed until 6' bgs	Top of Casing (2.09' ags)
6.0 - 9.0	SONIC 1	100		SP		SAND (possibly fill), fine to medium-grained, some silt, trace gravel and cobbles; dry, light brown	
9.0 - 19.0	SONIC 2	100		SM		SILTY SAND, very fine to fine-grained, subround, trace clay, no apparent bedding; loose, dry, light brown to brown with light gray intervals Lithology is granite (qtz, k-spar, trace lithies)	Grout (0' - 74' bgs)
16.0 - 17.0	SONIC 3	100				@16-17' bgs: thin beds (<2") of well indurated and cemented SS, possibly Caliche; light gray	
19.0 - 30.0	SONIC 4	100		SP		SAND, very fine to fine-grained, subround, some silt; firm to stiff, moist, brown with trace white sand stringers visible within laminae	PVC Pipe (2.090' ags - 109.3 bgs)
30.0							

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
30							
30 - 35	SONIC 5	100		SP		SAND, very fine to fine-grained, subround, some silt; firm to stiff, moist, brown with trace white sand stringers visible within laminae @33-34' bgs: well indurated SS (possibly Caliche); light brown with light gray	 Grout (0' - 74' bgs) PVC Pipe (2.090' ags - 109.3 bgs)
35 - 40	SONIC 6	100				SAND, very fine to fine-grained, subround, some silt, trace clay, irregular, thin bedding planes (0.5"); loose, dry @36-38' bgs: weathered zone: occurs predominantly between bedding planes within clays; brown, red, and gray @36-49' bgs: interbedded hard, light gray planes, well cemented (likely Caliche)	
40 - 45	SONIC 7	100					
45 - 50	SONIC 8	100		SP			
50 - 55	SONIC 9	100				@51.5-52.5' bgs: moist (perched moisture interval, not water-bearing)  @54-56.5: firm to dense, moist (perched moisture interval, not water-bearing)	
55 - 60	SONIC 10	100					
60 - 60.0	SONIC 11	100		SP		SAND, very fine to fine-grained, subround, some silt, trace clay, irregular, thin bedding planes (1"); loose, dry with moist intervals	


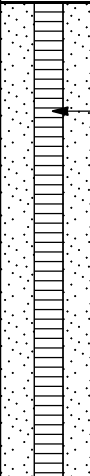
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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
65	SONIC 12	100			SP	SAND, very fine to fine-grained, subround, some silt, trace clay, irregular, thin bedding planes (1"); loose, dry with moist intervals  @75-78' bgs: moist (perched moisture interval, not water-bearing)  @82-88' bgs: moist (due to drilling waters)  @91-99' bgs: moist to wet  @96-98' bgs: increase in well consolidated SS interbedding (2"), siliceous cementation; hard	
70	SONIC 13	100					
75	SONIC 14	100					
80	SONIC 15	100					
85	SONIC 16	100					
90							
95							

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
100	SONIC 17	100		SP		SAND, very fine to fine-grained, subround, some silt, trace clay, irregular, thin bedding planes (1"); loose, dry with moist intervals @101-107' bgs: moist to wet intervals within medium-grained sand interbeds (<2") within native formation, potentially water-bearing	
105							
					109.3		4435.4

Bottom of borehole at 109.3 feet.

Total Depth of Well 109.3' bgs



**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 7/15/2016 **COMPLETED** 7/16/2016 **GROUND ELEVATION** 4587.399 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** ---  
**LOGGED BY** Matt Hartz **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 4589.593 N 4587.399 E **▼ AFTER DRILLING** 38.11 ft / Elev 4549.29 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 2.194 (ft) Casing Type: 2" PVC Pipe
0 - 5	N/A	0				Hand potholed until 5' bgs	Top of Casing (2.194' ags)
5 - 12	SONIC 1	100		FILL	[Cross-hatched pattern]	FILL, sand and silt matrix with gravel to large cobbles Varying lithologies	
12 - 15	SONIC 2	100					Grout (0' - 81' bgs)
15 - 28	SONIC 3	100		SM	[Dotted pattern]	SILTY SAND, fine to medium-grained, trace clay, unconsolidated, irregular thin beds, silts and clays within bedding planes; soft to firm, moist, light brown	PVC Pipe (2.194' ags - 107.9 bgs)
28 - 30	SONIC 4	100				23' bgs: firm, moist to wet  28' bgs: firm, moist to wet 28-30' bgs: moderately consolidated, firm to stiff, moist (on the verge of SS)	
30							

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
30							
30 - 35	SONIC 5	100		SM		<p>SILTY SAND, fine to medium-grained, trace clay, unconsolidated, irregular thin beds, silts and clays within bedding planes; soft to firm, moist, light brown</p> <p>30-35' bgs: moderately consolidated, firm to stiff, moist (on the verge of SS)</p> <p>35-36' bgs: interbeds (&lt;6") of consolidated SS (primarily qtz), very fine to fine-grained, siliceous cementation; dry, white</p>	<p>Grout (0' - 81' bgs)</p> <p>PVC Pipe (2.194' ags - 107.9 bgs)</p>
38.0					<p>4549.4</p> <p>SAND, very fine to fine-grained, subround, some silt, trace clay, minimal weathering, interbeds (&lt;6") of sandstones; firm, moist, light brown to brown</p>		
40 - 45	SONIC 6	100		SP			
45 - 50	SONIC 7	100					
50 - 55							
55 - 60	SONIC 8	100				<p>@57-60' bgs: wet (water-bearing)</p> <p>@60-64' bgs: wet (water-bearing)</p>	
60 - 65							

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
65						SAND, very fine to fine-grained, subround, some silt, trace clay, minimal weathering, interbeds (<6") of sandstones; firm, moist, light brown to brown  @68-78' bgs: moist  @80-82' bgs: increase in moisture above SS unit  @82' bgs: SS horizon (2"), well indurated and silified; hard, dry, gray with white clay at top and bottom @83-85' bgs: increase in moisture below SS unit  @87-96' bgs: increase in grain size to fine to medium-grained; saturated (not water-bearing zone, either perched or due to drilling waters)	<p>Grout (0' - 81' bgs)                      PVC Pipe (2.194' ags - 107.9 bgs)                      3/8" Bentonite Chips (81' - 85.1' bgs)                      10/20 Silica Sandpack (85.1' - 18' bgs)                      0.010 Slotted Pipe (87.9' - 107.9' bgs)</p>
70	SONIC 9	100					
75							
80	SONIC 10	100		SP			
85							
90	SONIC 11	100					
95							
					SANDSTONE	SANDSTONE, fine to medium-grained, subround to subangular, well indurated, well-cemented (siliceous); moist, brown	
					SP	See next page	

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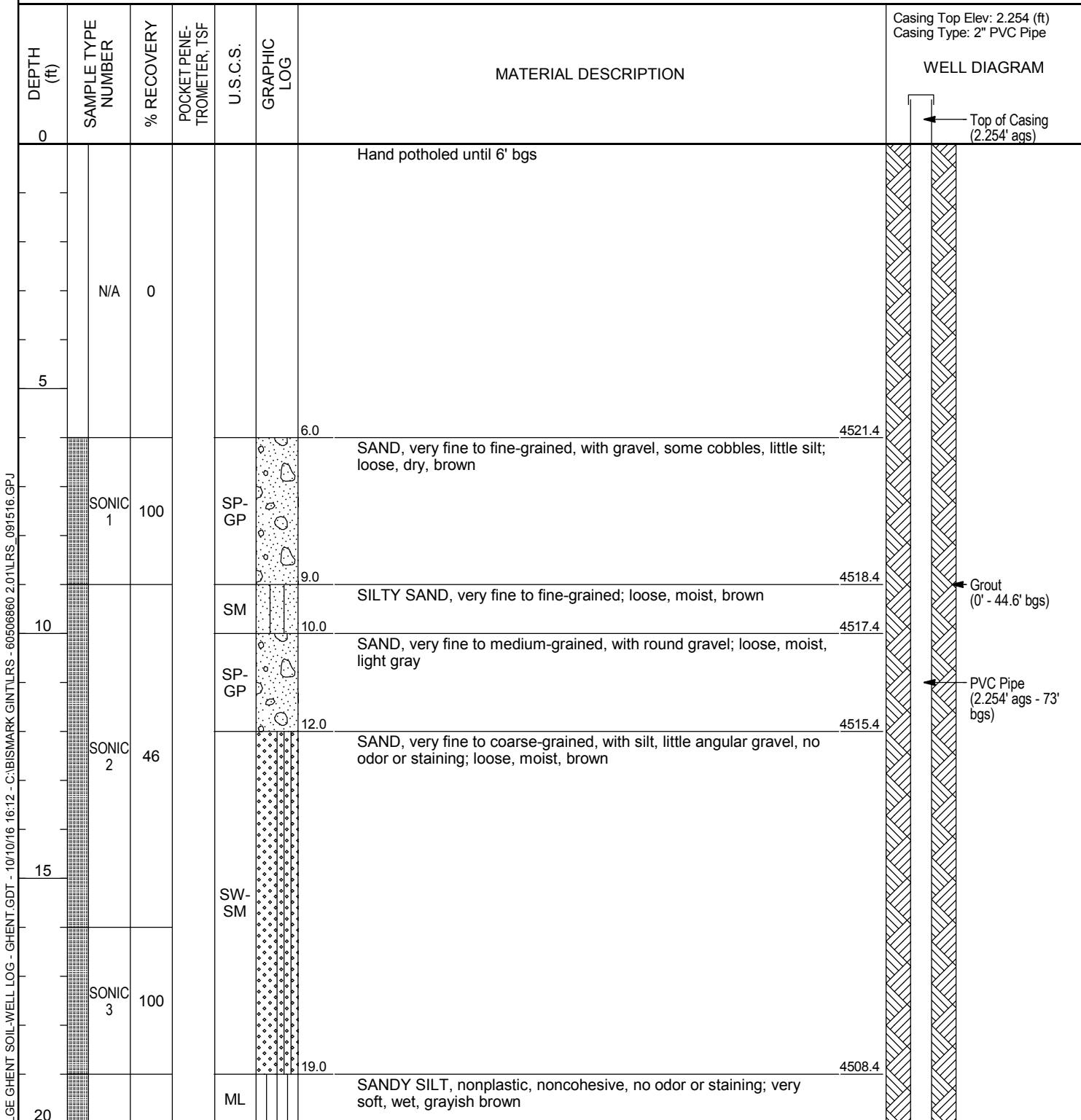
CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
100	SONIC 12	100		SP		SAND, very fine to medium-grained, subround to subangular, some silt, slight zones of weathered, dark brown, oxidized beds; firm to stiff, wet, light brown to brown	
105							
108.0							10/20 Silica Sandpack (85.1' - 18' bgs) 0.010 Slotted Pipe (87.9' - 107.9' bgs) Total Depth of Well 107.9' bgs

Bottom of borehole at 108.0 feet.

4479.4

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 8/3/2016 **COMPLETED** 8/3/2016 **GROUND ELEVATION** 4527.383 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** 69.00 ft / Elev 4458.38 ft  
**LOGGED BY** Chris Ahrendt **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 588577.1 N 731829.2 E **AFTER DRILLING** ---



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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
20							
21.0				ML		SANDY SILT, nonplastic, noncohesive, no odor or staining; very soft, wet, grayish brown	
21.8			SM		SILTY SAND; soft, moist, gray		
23.0			ML		SILT, nonplastic, noncohesive; medium, moist, gray and mottled brown and gray		
27.0			SM		SILTY SAND, very fine to fine-grained, no staining; loose, moist, brown, no mottling		
29.0			ML		SILT, with sand, nonplastic, noncohesive, no odor or staining; very soft, wet, brownish gray		
30.4			SM		SILTY SAND, very fine to fine-grained; loose, wet, grayish brown wetness due to drilling waters		
31.5			SM		SILTY SAND, very fine to fine-grained, little subangular gravel; loose, moist, grayish brown (10YR 5/2)		
32.2			SP		SAND, very fine to fine-grained, trace silt, no odor or staining; loose, moist, light brownish gray		
34.0			SP		S.A.A., light gray (10YR 7/1)		
34.5			SP		SAND, very fine to medium-grained, little silt; medium dense, moist, dark grayish brown (10YR 4/2)		
37.0			SP		S.A.A., little subangular gravel; light brownish gray (10YR 6/2)		
39.0			SP		S.A.A., no gravel; light gray (10YR 7/1)		
40			SM		SILTY SAND, very fine to fine-grained, no odor or staining; loose, wet, yellowish brown		

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SONIC 4 77  
 SONIC 5 80  
 SONIC 6 100

CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
45	SONIC 7	76		SM		SILTY SAND, very fine to fine-grained, no odor or staining; loose, wet, yellowish brown	<p>Grout (0' - 44.6' bgs)</p> <p>PVC Pipe (2.254' ags - 73' bgs)</p> <p>3/8" Bentonite Chips (44.6' - 50.6' bgs)</p> <p>0.010 Slotted Pipe (53' - 73' bgs)</p> <p>10/20 Silica Sandpack (50.6' - 73' bgs)</p>
48.5					4478.9		
50				SP-SM		SAND, very fine to fine-grained, with silt, no odor or staining; loose, moist, pale brown (10YR 6/3)	
50.3					4477.1		
	SONIC 8	69		SP-SM		S.A.A., brown (10YR 5/3)	
54.0					4473.4		
55				ML		SILT, with gravel, nonplastic, noncohesive, massive, no odor or staining; very stiff, moist, grayish brown (10YR 5/2)	
56.0					4471.4		
	SONIC 9	100	3.0	SM		SILTY SAND, very fine-grained; medium dense, moist, grayish brown (10YR 5/2)	
58.0					4469.4		
				SM		S.A.A., with gravel (sandstone); moist	
59.0					4468.4		
60				SM		SILTY SAND, very fine to fine-grained, no odor or staining; loose, wet, grayish brown (10YR 5/2)	
62.0					4465.4		
				SM		S.A.A., medium dense, wet	
65	SONIC 10	85	4.0	ML		See next page	4462.3

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
				ML		SILT, nonplastic, noncohesive, blocky, no odor or staining; stiff, moist, light brownish gray (10YR 6/2), no mottling	
69.0				SP-GW		SAND, poorly graded, with gravel; very loose, wet, grayish brown	
70.0				ML		SILT, nonplastic, noncohesive; soft, wet, grayish brown and mottled gray (10YR 6/1) and light brownish gray (10YR 6/2)	
71.0				SM		SILTY SAND, very fine to fine-grained, no odor or staining; loose, wet, grayish brown	
74.0	SONIC 11	78		SM		S.A.A., decreasing in moisture	
79.0							

Bottom of borehole at 79.0 feet.

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 8/9/2016 **COMPLETED** 8/9/2016 **GROUND ELEVATION** 4513.297 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** ---  
**LOGGED BY** Jeremy Hurshman **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 588829.6 N 732965.3 E **▼ AFTER DRILLING** 40.00 ft / Elev 4473.30 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0						Hand potholed until 5.5' bgs	Casing Top Elev: 2.534 (ft) Casing Type: 2" PVC Pipe
5	N/A	0					Top of Casing (2.534' aqs)
5.5						4507.8 SILTY SAND, fine-grained; loose, dry, medium brown to tan	
9.0	SONIC 1	100		SM		4504.3 SILTY SAND, fine-grained, poorly cemented sandstone lenses, no odor or staining; moist to wet, light tan	Grout (0' - 42' bgs)
14.0	SONIC 2	100		SM		4499.3 SILTY SAND; dry, light tan 14-16' bgs: poorly cemented sandstone lenses, lenses broken by drilling	PVC Pipe (2.534' aqs - 68.5' bgs)
15	SONIC 3	100		SM			
20							

CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
20							
	SONIC 4	100		SM		SILTY SAND; dry, light tan	<p>Grout (0' - 42' bgs)</p> <p>PVC Pipe (2.534' ags - 68.5' bgs)</p>
				SM		22.0 SILTY SAND, fine-grained, subround, trace sandstone lenses; moist, light brown 4491.3	
25				SM		27.0 SAND, fine-grained; loose with hard sections (breaks in hand), moist 4486.3	
	SONIC 5	100		SP		29.0 SAND, fine-grained, few poorly cemented sandstone lenses, minor clay, no odor or staining, crumbles; dry to moist, brown 4484.3	
	SONIC 6	100		SP		34.0 SAND, fine-grained, subround to round; loose, moist to wet (due to drilling waters), brown 4479.3	
35	SONIC 7	100		SM		38.0 SILTY SAND, subround to round; loose, moist to wet (due to drilling waters), brown 4475.3	
				SP		39.0 SAND, fine-grained; dry, light tan @38' bgs: 1 inch of hard zone of visible thin channel, brown silt deposits 4474.3	
40				SP		SAND, fine-grained, round, little silt, tight and compact; stiff, wet	

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 10/10/16 15:07 - C:\BISMARK GINTLRS - 60506860 2.01\LRS\_091516.GPJ

CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_


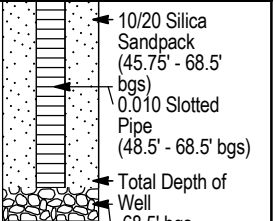
DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
45	SONIC 8	100		SP		SAND, fine-grained, round, little silt, tight and compact; stiff, wet  @45' bgs: gradational contact: increasing silt and decreasing sand	
				ML		SILT, with fine-grained sand, few interbedded clay nodules, low to medium plasticity; stiff, wet, brown	
						46.0 4467.3	
50						SILTY SAND, fine-grained, no visible structures; medium dense, wet, brown	
				SM			
55	SONIC 9	100					
				SANDSTONE		SANDSTONE, fine-grained, fractured from drilling; hard, light gray to tan	
60							
				SP		SAND, fine-grained, little silt; medium dense, wet, brown	
65	SONIC 10	100					
						59.0 4454.3	
						60.0 4453.3	

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CLIENT Basin Electric PROJECT NAME Laramie River Station

PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
				SP		SAND, fine-grained, little silt; medium dense, wet, brown	

69.0

4444.3

Bottom of borehole at 69.0 feet.

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 8/10/2016 **COMPLETED** 8/10/2016 **GROUND ELEVATION** 4498.003 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** 69.00 ft / Elev 4429.00 ft  
**LOGGED BY** Jeremy Hurshman **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 589002.8 N 734274.6 E **AFTER DRILLING** ---

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 3.441 (ft) Casing Type: 2" PVC Pipe
0						Hand potholed until 5' bgs	Top of Casing (3.441' aqs)
5	N/A	0					
5	SONIC 1	100		ML		SILT, with fine-grained, subround to round, sand, trace clay, no odor or staining; dry, moist @7-9' bgs: moist increasing sand with depth	
9.0						4493.0	
9.0						SILTY SAND, fine-grained; moist to dry @9-10' bgs: minor round gravel (0.4-0.8" in size) little recovery due to bit being blocked	Grout (0' - 50' bgs)
10							
10	SONIC 2	50		SM			PVC Pipe (3.441' aqs - 78.5' bgs)
15							
19.0						4489.0	
19.0				GW		SANDY GRAVEL, well graded, fine to coarse-grained, subround to round, little silt, no odor or staining; wet, brown to light tan increasing silt with depth	
20.0						4479.0	
20.0						4478.0	

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
20							
24.0	SONIC 3	90		GW		SANDY GRAVEL, well graded, fine to coarse-grained, subround to round, little silt, no odor or staining; dry, brown to light tan increasing silt with depth	<p>Grout (0' - 50' bgs)</p> <p>PVC Pipe (3.44' ags - 78.5' bgs)</p>
26.0			ML		SILT, with fine-grained sand, minor clay, low plasticity; moist, brown (gradiational contact)		
29.0	SONIC 4	100		SM		SILTY SAND, fine-grained sand, trace clay, no plasticity; moist to wet, brown	
34.0			ML		SILT, with minor sand, trace clay; dense, moist, brown		
39.0	SONIC 5	100		ML		S.A.A, increasing sand; moist to wet	
40.0	SONIC 6	100		ML		SANDSTONE, fine-grained sand, poorly cemented; hard, dry, light gray	
44.0				ML		SILT, with fine-grained sand, little clay, low plasticity; medium dense, moist, brown	

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
45	SONIC 7	100		ML		SILT, with fine-grained sand, little clay, low plasticity; medium dense, moist, brown	
49.0						4449.0	
50				SANDSTONE		SANDSTONE or SILTSTONE, fine-grained, fractured from drilling; hard, wet in fractures and at bottom (may be due to drilling waters), light tan to light gray	
52.0						4446.0	
55	SONIC 8	100		ML		SILT, with fine-grained sand, low to no plasticity, crumbles when crushed with hands, no odor or staining; moist, brown	
59.0						4439.0	
60				SP		SAND, fine-grained, little silt; wet (may be due to drilling waters)	
60.0						4438.0	
				SM		SILTY SAND, fine-grained sand, hard sand nodules interbedded; moist to wet (water in and around sand), brown increasing silt with depth	
64.0	SONIC 9	100				4434.0	
65				ML		SILT, minor fine-grained sand, little clay, crumbles in hand; moderately stiff, moist, brown decreasing sand with depth	



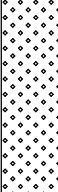

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
				ML		SILT, minor fine-grained sand, little clay, crumbles in hand; moderately stiff, moist, brown decreasing sand with depth	<p>10/20 Silica Sandpack (55' - 79' bgs)</p> <p>0.010 Slotted Pipe (58.5' - 78.5' bgs)</p> <p>Total Depth of Well 78.5' bgs</p>
				SP	69.0 ▽	SAND, fine-grained, minor silt; wet, tan	
70				SP	70.0	S.A.A., brown	
				SP			
75	SONIC 10	100		ML	74.0	SILT, with fine-grained sand, crumbles; wet in fractures and sand zones, brown	
				ML	76.0	S.A.A., decreasing sand with depth; moist	
					79.0	4419.0	

Bottom of borehole at 79.0 feet.

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 8/4/2016 **COMPLETED** 8/5/2016 **GROUND ELEVATION** 4527.324 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** 74.00 ft / Elev 4453.32 ft  
**LOGGED BY** Chris Ahrendt **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 589659.8 N 731518.4 E **AFTER DRILLING** ---

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 2.065 (ft) Casing Type: 2" PVC Pipe
0 - 14.0	SONIC 1	100		FILL		SAND (FILL), fine to coarse-grained, with round gravel, no odor or staining; loose, moist, brown	Top of Casing (2.065' ags)
14.0 - 15.0				SW-GP		SAND, very fine to coarse-grained, with subangular gravel, no odor or staining; loose, wet, grayish brown (10YR 5/2)	Grout (0' - 67.11' bgs)
15.0 - 18.0	SONIC 2	28		SW		S.A.A., no gravel; moist, very pale brown (10YR 7/3)	PVC Pipe (2.065' ags - 92.1' bgs)
18.0 - 20.0	SONIC 3	100		SW		S.A.A., little subangular gravel	
						@9' bgs: rock prevented 3.6' of recovery	

(Continued Next Page)



CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
20							
	SONIC 4	94		SW		SAND, very fine to coarse-grained, little subangular gravel, no odor or staining; loose, moist, very pale brown (10YR 7/3)	<p>Grout (0' - 67.11' bgs)</p> <p>PVC Pipe (2.065' ags - 92.1' bgs)</p>
				SW		21.6 21.9 S.A.A., light gray (10YR 7/1) S.A.A., little silt; light brownish gray (10YR 6/2)	
				SW			
25			1.5	SM		25.7 SILTY SAND, very fine to fine-grained, no odor staining; stiff, moist, gray (10YR 5/1)	
	SONIC 5	100		SP-SM		26.9 SAND, very fine to fine-grained, with silt; stiff, moist, gray (10YR 6/1)	
				SP-SM		30.4 S.A.A., wet	
				SP-SM		33.4 S.A.A., moist	
	SONIC 6	99		SP-SM		34.0 S.A.A., moist to wet, light brownish gray (10YR 6/2)	
				SP-SM		36.5 S.A.A., medium stiff, moist	
				SP-SM		36.7 S.A.A., loose, decreasing moisture	
				SP-SM			
40				SM		40.0 SILTY SAND, very fine to medium-grained, no odor or staining; loose (broken up by rig), moist, light yellowish brown (10YR 6/4)	
	SONIC 7	90					

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
45	SONIC 8	98		SM		SILTY SAND, very fine to medium-grained, no odor or staining; loose (broken up by rig), moist, light yellowish brown (10YR 6/4)	
47.4						4479.9	
						CALICHE, 1" thick, with sand; hard, dry, white	
						48.3	4479.0
50	SONIC 9	86		SM		SILTY SAND, very fine-grained; loose (broken up by rig), moist, light yellowish brown (10YR 6/4)	
50.5						4476.8	
						SAND, very fine to fine-grained, with silt, no odor or staining; loose, moist, brown (10YR 5/3)	
55	SONIC 10	96		SP-SM		59.0	
60							
						61.8	4465.5
						62.0	4465.3
						S.A.A., wet	
						S.A.A., moist	
	SONIC 11	97	>4.0	SM		64.0	4463.3
65							

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
66.5				SM		SILTY SAND, very fine to fine-grained; hard, moist, brown (10YR 4/3)	
						S.A.A., medium dense, moist	
68.8				SM			
						S.A.A., soft, moist	
69.0				SM		No recovery due to rock	
74.0	SONIC 12	50				SILTY SAND, very fine to fine-grained; loose, wet, grayish brown (10YR 5/2)	
77.6				SM		S.A.A., decreasing moisture	
79.0				SM			
84.0	SONIC 13	60		ML		SILT, with sand, noncohesive, nonplastic, no odor or staining; medium dense, moist to wet, dark grayish brown (10YR 4/2)	
88.0	SONIC 14	98		SP		SAND, very fine to fine-grained; loose, moist to wet, brown	
				SP		S.A.A., fine to medium-grained	

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

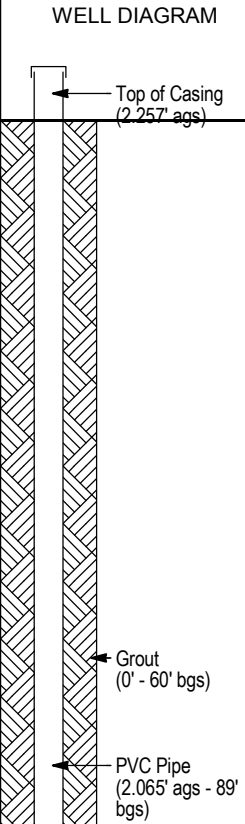
DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
90				SP		89.0	4438.3
						SILTY SAND, very fine to fine-grained; loose, wet, brown (10YR 4/3)	<ul style="list-style-type: none"> <li>10/20 Silica Sandpack (69.1' - 92.1' bgs)</li> <li>0.010 Slotted Pipe (72.1' - 92.1' bgs)</li> <li>Total Depth of Well 92.1' bgs</li> </ul>
95	SONIC 15	80		SM			
						99.0	4428.3

Bottom of borehole at 99.0 feet.

Native Clay Below Well - Natural Collapse

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 8/6/2016 **COMPLETED** 8/7/2016 **GROUND ELEVATION** 4528.664 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** ---  
**LOGGED BY** Chris Ahrendt **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 589851.3 N 732581.2 E **▼ AFTER DRILLING** 73.85 ft / Elev 4454.81 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 2.257 (ft) Casing Type: 2" PVC Pipe
0							Top of Casing (2.257' ags)
5	SONIC 1	100		SW-GP		SAND, very fine to medium-grained, with gravel, little silt, little organic material; loose, moist, brown	
6.0						4522.7	
9.0				SP-SM		S.A.A., with silt, less gravel	
10.9				ML		SILT, with gravel and sand, noncohesive, nonplastic; soft, wet (due to drilling waters), grayish brown (10YR 5/2)	
10.9						4519.7	
11.8				SW-GP		SAND, fine to coarse-grained, with subround gravel, little silt; loose, moist, brown	
11.8						4516.9	
12.6				SW-GP		S.A.A., some silt	
12.6						4516.1	
15	SONIC 2	53		SW-GP		S.A.A., no silt	
19.0						4509.7	
20	SONIC 3	100		SM		SILTY SAND, very fine-grained, no odor or staining; soft, moist, light brownish gray (10YR 6/2)	
23.0						4505.7	
23.0			>4.0	SM		S.A.A., hard	
24.0						4504.7	
24.0				SM		S.A.A., medium	
25							



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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
25							
29.0	SONIC 4	88		SM		SILTY SAND, very fine-grained, no odor or staining; medium dense, moist, light brownish gray (10YR 6/2)	<p>Grout (0' - 60' bgs)</p> <p>PVC Pipe (2.065' ags - 89' bgs)</p>
30			2.0	SP-SM		SAND, very fine to medium-grained, with silt, little gravel; loose, wet (perched aquifer), brown (10YR 5/3)	
32.0				SP-SM		S.A.A., stiff, moist, dark gray (10YR 4/1)	
33.5	SONIC 5	79		SP-SM		S.A.A., loose, light brownish gray (10YR 6/2)	
35				SP-SM			
40	SONIC 6	100		SM		SILTY SAND, very fine-grained, little fine-grained sand; stiff, moist, light brownish gray (10YR 6/2)	
43.0				SM		S.A.A., dark gray (10YR 4/1)	
44.0				SM		S.A.A., light brownish gray (10YR 6/2)	
45				SM			
46.0	SONIC 7	100		SP-SM		SAND, very fine to fine-grained, with silt, no odor or staining; loose, moist, pale brown (10YR 6/3)	
47.2				SP-SM		S.A.A., grayish brown (10YR 5/2)	
48.5			1.0	SP-SM		S.A.A., stiff	
50				SP-SM			
50.7	SONIC 8	100		SP-SM		S.A.A., loose, light brownish gray (10YR 6/2)	
53.0				SP-SM		S.A.A., stiff, grayish brown (110YR 5/3)	

(Continued Next Page)



CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
55	SONIC 9	84		SP-SM	54.0	SILTY SAND, very fine-grained, little fine-grained sand; medium dense, moist, light brownish gray (10YR 6/2)	Grout (0' - 60' bgs)
				SM			
					58.5		
					59.0	S.A.A., blocky; very stiff	
60	SONIC 10	100	1.75	SP-SM	60.4	SAND, very fine to fine-grained, with silt; stiff, moist, grayish brown (10YR 5/2)	PVC Pipe (2.065' ags - 89' bgs)
					60.4	S.A.A., loose, pale brown (10YR 6/3)	
65	SONIC 11	86	1.5	SP-SM	65.7	S.A.A., loose, moist, light brownish gray (10YR 6/2)	3/8" Bentonite Chips (60' - 64.9' bgs)
					65.7		
					69.0		
70	SONIC 12	64		SM	70.0	SILTY SAND, very fine to medium-grained; soft, wet, dark grayish brown (10YR 4/2)	10/20 Silica Sandpack (64.9' - 89' bgs)
					70.0	S.A.A., slow dilatancy; medium stiff, wet	
					78.0		
					79.0	S.A.A., moist	
80				SM		SILTY SAND; soft, wet, dark yellowish brown (10YR 4/4)	0.010 Slotted Pipe (69' - 89' bgs)
				SM	81.5		
					81.5	S.A.A., mottled dark yellowish brown and gray (10YR 5/1)	

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
85	SONIC 13	32				No recovery	<p>10/20 Silica Sandpack (64.9' - 89' bgs)                      0.010 Slotted Pipe (69' - 89' bgs)</p>
89.0						Bottom of borehole at 89.0 feet.	<p>Total Depth of Well 89' bgs</p>

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 8/7/2016 **COMPLETED** 8/8/2016 **GROUND ELEVATION** 4525.334 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** 82.00 ft / Elev 4443.33 ft  
**LOGGED BY** Chris Ahrendt **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 590022.2 N 733532.2 E **AFTER DRILLING** ---

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 2.383 (ft) Casing Type: 2" PVC Pipe
0						SAND, very fine to medium-grained, with gravel and silt, no odor or staining; loose, dry to moist, brown @0-3' bgs: organic material (roots, etc)	Top of Casing (2.383' ags)
5	1	100		SP			
10	2	100		SM		11.5 4513.8 SILTY SAND, very fine to fine-grained; loose, moist, yellowish brown	Grout (0' - 66' bgs)
15	3	100		SW-GP		14.0 4511.3 SAND, very fine to coarse-grained, with subround gravel (qtz, granite); loose, brown	PVC Pipe (2.383' ags - 93' bgs)
20	4	100		ML		17.4 4507.9 SILT, noncohesive, nonplastic, blocky; stiff, moist, brown, mottled with gray	
				ML		19.0 4506.3 SILT, some fine to medium-grained sand, little white qtz fragments, noncohesive, nonplastic, blocky; medium stiff, moist, grayish brown (10YR 5/2)	
				ML		21.4 4503.9 SILT, some fine to coarse-grained sand, little angular gravel, noncohesive, nonplastic, blocky; medium stiff, wet, grayish brown (10YR 5/2)	
				ML		23.0 4502.3 S.A.A., moist	
25							

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 10/10/16 15:10 - C:\BISMARCK GINTLRS - 60506860 2.01\LRS\_091516.GPJ

CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
25	5	100		ML	26.5	SILT, some fine to coarse-grained sand, little angular gravel, noncohesive, nonplastic, blocky; medium, moist, grayish brown (10YR 5/2)	4498.8
				SM	29.0	SILTY SAND, very fine to fine-grained; loose, moist, yellowish brown	
30	6	97	3.5	SM	31.0	SILTY SAND, very fine-grained; loose, moist, gray (10YR 5/1)	4496.3
				SM	32.8	S.A.A., very loose	4494.3
				SM	33.1	S.A.A., very stiff	4492.5
				SM	33.1	S.A.A., very stiff	4492.2
				SM	34.0	S.A.A., very loose	4491.3
35				SP-SM	35.8	SAND, poorly graded, with silt; loose, moist, grayish brown (10YR 5/2)	4489.5
				CALICHE	36.6	CALICHE, laminated; hard, dry, white	4488.7
				ML	41.0	SANDY SILT, noncohesive, nonplastic; medium stiff, moist, brown	4484.3
				ML	42.9	S.A.A., increasing sand content	4482.4
45	7	100		SP-SM	47.5	SAND, very fine to fine-grained, with silt, no odor or staining; loose, moist, light brownish gray (10YR 6/2)	4477.8
				CALICHE	48.1	CALICHE; hard, moist, white	4477.2
	8	100		SP-GP	48.5	SAND, poorly graded, with gravel	4476.8
				SP-GP	48.7	SAND, poorly graded, with gravel	4476.6
				CALICHE	49.0	CALICHE; hard, moist, white	4476.3
50	9	62		SP-GP	50.4	SAND, poorly graded, with gravel; moist	4474.9
				SP-SM	50.4	SAND, poorly graded, with silt; loose, brown (10YR 5/3)	4474.9
				SP		SAND, very fine to medium-grained, with gravel and silt; loose, brown	

Grout (0' - 66' bgs)  
 PVC Pipe (2.383' ags - 93' bgs)

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM	
55	10	96	>4.0	SP	54.0		4471.3	
				SP-SM	54.3	SAND, very fine to medium-grained, with silt, trace angular gravel; very dense, moist, grayish brown (10YR 5/2)	4471.0	
				SP-SM		S.A.A., loose		
				SP-SM	57.0		4468.3	
				SP-SM	57.5	S.A.A., increasing moisture	4467.8	
60	11	83		SP-SM	60.0		4465.3	
						SAND, very fine to medium-grained, with silt, trace angular gravel; very dense, moist to wet, light brownish gray (10YR 6/2)		
				SP-SM	65.0		4460.3	
65	12	100		SM	66.0	SILTY SAND, very fine to fine-grained, no odor or staining; loose, moist, gray	4459.3	
				SP-SM		SAND, very fine to fine-grained, with silt; loose, moist, light brown		
				SP-SM	69.0	S.A.A., wet	4456.3	
70	13	47	3.0	SP-SM	72.5		4452.8	
				ML	72.8	SILT, with fine sand, noncohesive, nonplastic; very soft, wet, dark gray (10YR 4/1)	4452.5	
				SP-SM	74.0	SAND, very fine to fine-grained, with silt; loose, moist to wet, brown	4451.3	
				SM		SILTY SAND; very stiff, moist, grayish brown		
				SM	76.0	S.A.A., dry	4449.3	
75				SP-GP	78.3		4447.0	
				SP-GP	79.0	SAND, very fine to fine-grained, with gravel; stiff, dry, light gray	4446.3	
				SP-GP		S.A.A., medium stiff, moist		
80					82.0		4443.3	

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
85	14	30				No recovery	<p>Sandpack (70.5' - 93' bgs)</p> <p>0.010 Slotted Pipe (73' - 93' bgs)</p> <p>Total Depth of Well 93' bgs</p> <p>Native Clay Below Well - Natural Collapse</p>
90	15	100		SP	<p>SAND, very fine to fine-grained, trace silt, compact but breaks in hand; wet, brown</p> <p>@93.5' bgs: &lt;1 inch of CALICHE; hard, dry, light gray</p>		
						<p>Bottom of borehole at 94.0 feet.</p>	

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**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** \_\_\_\_\_  
**DATE STARTED** 8/8/2016 **COMPLETED** 8/9/2016 **GROUND ELEVATION** 4520.426 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** Major Drilling, Inc **GROUND WATER LEVELS:**  
**DRILLING METHOD** Rotary Sonic **AT TIME OF DRILLING** ---  
**LOGGED BY** Jeremy Hurshman **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 590358.4 N 734848.3 E **▼ AFTER DRILLING** 69.00 ft / Elev 4451.43 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 2.169 (ft) Casing Type: 2" PVC Pipe
0				ML		SILT, trace gravel, rootlets near surface, topsoil; dry, dark brown	Top of Casing (2.169' ags)
3.0				SP		SILT, with very fine-grained sand; dry, tan	
4517.4	1	100		SW-GP		SAND, well graded, with 30% round gravel and cobbles (max 3"), no odor or staining; dry, tan	
6.0				SP		SAND, poorly graded, with 25% subround gravel and 15% silt, few cobbles, no odor or staining; dry, light tan Material very hot from core barrel	Grout (0' - 62' bgs)
4514.4				SP		SAND, fine-grained; loose, slightly moist, light tan	PVC Pipe (2.169' ags - 89' bgs)
9.0				SP		@17' bgs: .5" thick cemented zone	
4511.4	2	100		CALICHE		CALICHE, sandy, breaks into discs, broken from drilling; hard, wet (due to drilling waters), white	
16.0				ML		SILT, little sand, trace clay, low plasticity, crumbles; moist, light tan to white	
4504.4	3	100		SM		SILTY SAND, fine-grained, trace clay; dry, light tan to white	
20.0							
4500.4	4	100					
4498.4							
4496.4							
25							

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
25							
26.5	5	100		SM		SILTY SAND, fine-grained, trace clay; dry, light tan to white @25.4-26.5' bgs: caliche modules	
				SM		SILTY SAND, fine-grained, no odor or staining; dry to moist, medium tan	
29.0				SM		SAND, fine grained, few hard cemented sand nodules, trace fines; hard, wet (due to drilling waters)	
				SP		SAND, fine grained, few hard cemented sand nodules, trace fines; hard, wet (due to drilling waters)	
30.3	6	100		ML		SILT, minor fine-grained sand, few white caliche nodules; moist to dry	
				ML		SILT, with very fine-grained sand, crumbles; medium tan to brown	
31.7				ML		SILT, with very fine-grained sand, crumbles; medium tan to brown	
				ML		SILT, with very fine-grained sand, crumbles; medium tan to brown	
34.0				SM		SILTY SAND, fine-grained; soft, wet (due to drilling waters)	
				SM		SILTY SAND, fine-grained; soft, wet (due to drilling waters)	
35.0	7	100		SP		SAND, fine-grained, with sandstone lenses, water in fractures, minor silt, no odor; stiff to very stiff	
				SP		SAND, fine-grained, with sandstone lenses, water in fractures, minor silt, no odor; stiff to very stiff	
36.7				SM		SILTY SAND, fine-grained, no odor or staining, crumbles; light tan to brown could be siltstone	
				SM		SILTY SAND, fine-grained, no odor or staining, crumbles; light tan to brown could be siltstone	
39.0				SM		SILTY SANDSTONE, very fine-grained; hard, wet in fractures, dry in macro core, light tan	
				SM		SILTY SANDSTONE, very fine-grained; hard, wet in fractures, dry in macro core, light tan	
40.5	8	100		SANDSTONE		SAND, fine-grained, with silt; loost, moist to wet (water in borehole), medium to dark brown	
				SP-SM		SAND, fine-grained, with silt; loost, moist to wet (water in borehole), medium to dark brown	
44.0				SP-SM		SAND, fine-grained, with silt; loost, moist to wet (water in borehole), medium to dark brown	
				SP-SM		SAND, fine-grained, with silt; loost, moist to wet (water in borehole), medium to dark brown	
45.0	9	100		SP		SAND, fine-grained, subround to round, minor silt; loose, moist to wet, tan to light tan	
				SP		S.A.A., dry	
50				SP		S.A.A., dry	
				SP		S.A.A., dry	
53.5	10	100		SP		@49-50' bgs: wet (due to drilling waters)	
				SP		@50-53' bgs: moist, grayish brown	

Grout (0' - 62' bgs)  
 PVC Pipe (2.169' ags - 89' bgs)


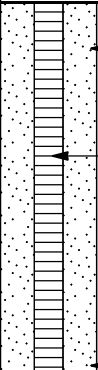
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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
55	11	100		SM	SP	54.0 SAND, fine-grained, minor medium-grained sand, compact and hard lenses of gray clay/silt; tan SILTY SAND, fine-grained, no odor or staining; loose, dry to moist @54-55' bgs: moist (due to drilling waters) 4466.4	<p>Grout (0' - 62' bgs)</p> <p>PVC Pipe (2.169' ags - 89' bgs)</p> <p>3/8" Bentonite Chips (62' - 67' bgs)</p> <p>10/20 Silica Sandpack (67' - 89' bgs)</p> <p>0.010 Slotted Pipe (69' - 89' bgs)</p>
60	12	50		SM	60.0 SILTY SAND, fine-grained, sloppy; very wet (due to drilling waters) mainly sluff 4460.4		
65	13	100		SM	64.0 SILTY SAND, fine-grained; loose, dry (moist to wet at top of core due to drilling water), light tan 4456.4		
70	14	100		SM	69.0 SILTY SAND; moist to wet (slightly compact in wet zone), light brownish tan 4451.4		
75	15	100		SM	74.0 S.A.A., slightly stiff @75-76' bgs: moist, gray 4446.4		
80				SM	80.0 SILTY SAND, breaks with hands; wet, brown 4440.4		

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION \_\_\_\_\_

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
85	16	100		SM		SILTY SAND, breaks with hands; wet, brown	 <p>10/20 Silica Sandpack (67' - 89' bgs)</p> <p>0.010 Slotted Pipe (69' - 89' bgs)</p>

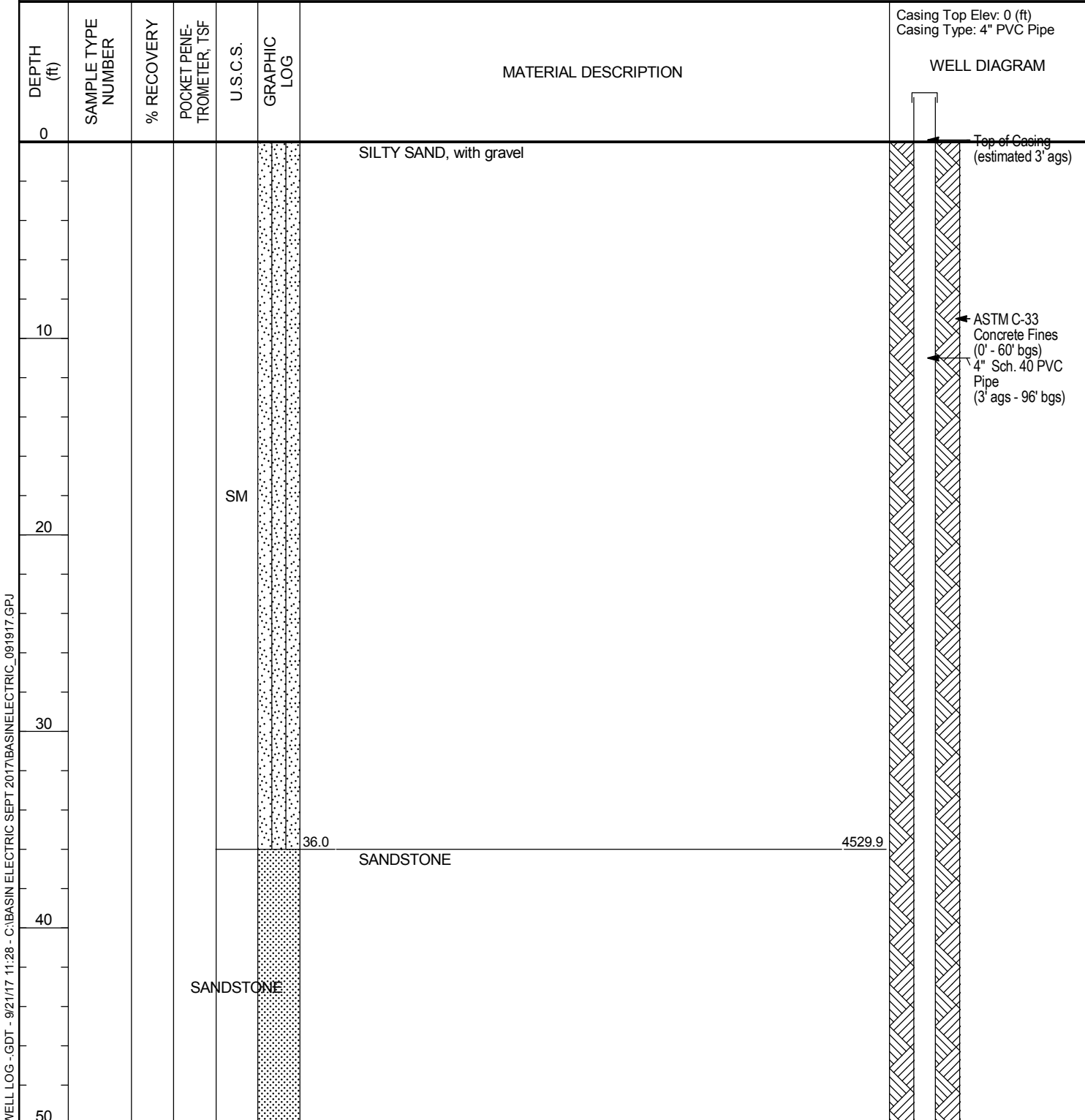
89.0

Bottom of borehole at 89.0 feet.

4431.4

Total Depth of Well 89' bgs

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** Wheatland, Wyoming  
**DATE STARTED** 8/18/1982 **COMPLETED** 8/18/1982 **GROUND ELEVATION** 4565.87 ft **HAMMER TYPE** \_\_\_\_\_  
**DRILLING CONTRACTOR** Northern Testing Laboratories **GROUND WATER LEVELS:**  
**DRILLING METHOD** B-53 Rock Bit **AT TIME OF DRILLING** ---  
**LOGGED BY** \_\_\_\_\_ **CHECKED BY** \_\_\_\_\_ **AT END OF DRILLING** ---  
**COORDINATES** 587159.1 N 729587.2 E **▼ AFTER DRILLING** 77.60 ft / Elev 4488.27 ft



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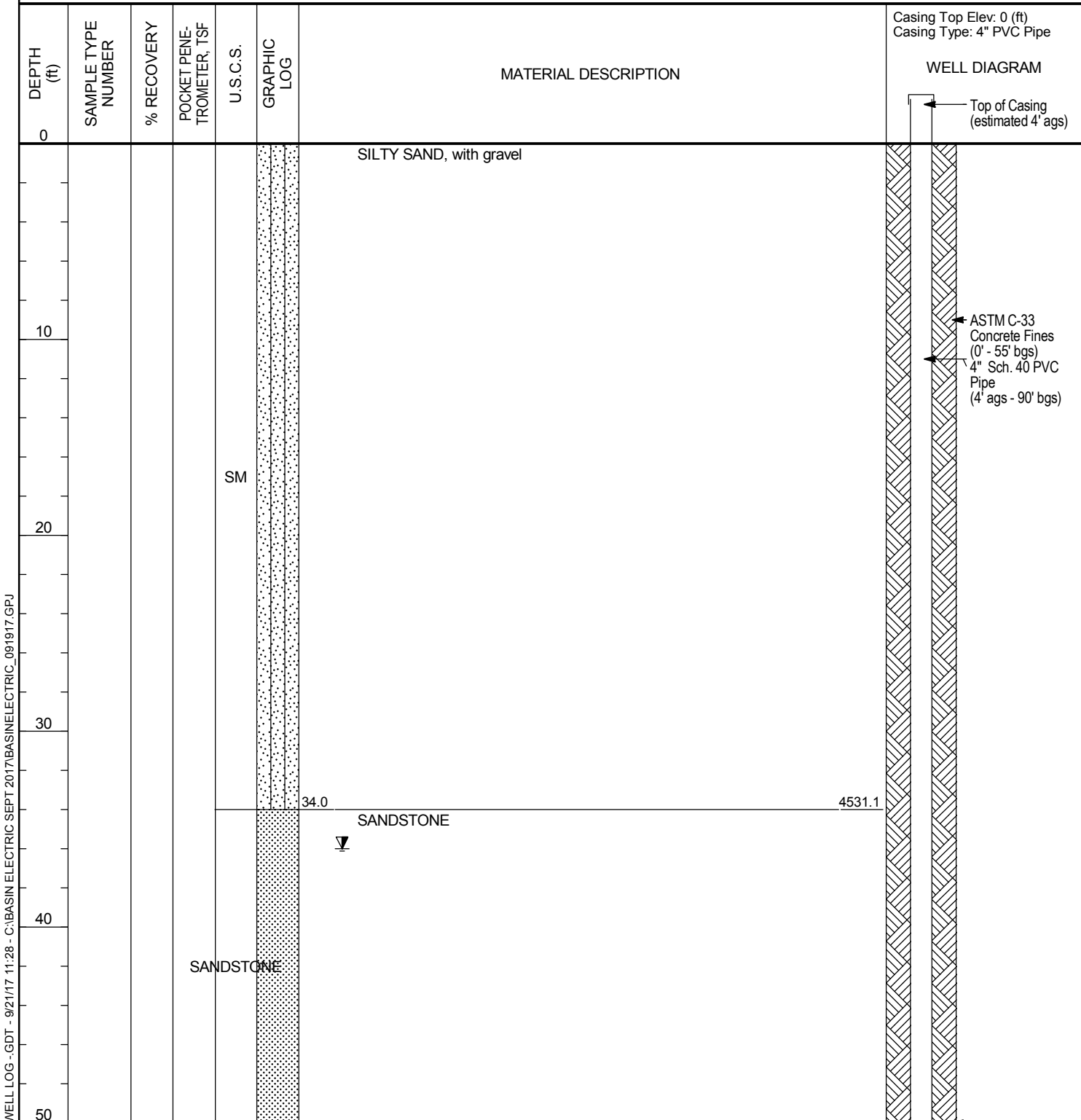
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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION Wheatland, Wyoming

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
50						SANDSTONE	
60							
70						SANDSTONE	
80							ASTM C-33 Concrete Fines (0' - 60' bgs)
90							Sandpack (60' - 96' bgs)
							#12 Pipe (66.3' - 96' bgs)
						96.0	4469.9
						Bottom of borehole at 96.0 feet.	Total Depth of Well 96' bgs

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**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** Wheatland, Wyoming  
**DATE STARTED** 8/21/1982 **COMPLETED** 8/21/1982 **GROUND ELEVATION** 4565.07 ft **HAMMER TYPE** \_\_\_\_\_  
**DRILLING CONTRACTOR** Northern Testing Laboratories **GROUND WATER LEVELS:**  
**DRILLING METHOD** B-53 Rock Bit **AT TIME OF DRILLING** ---  
**LOGGED BY** \_\_\_\_\_ **CHECKED BY** \_\_\_\_\_ **AT END OF DRILLING** ---  
**COORDINATES** 587179.9 N 728811.2 E **▼ AFTER DRILLING** 36.00 ft / Elev 4529.07 ft



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**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station

**PROJECT NUMBER** 60506860 **PROJECT LOCATION** Wheatland, Wyoming

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
50						SANDSTONE	ASTM C-33 Concrete Fines (0' - 55' bgs)
60							
70					SANDSTONE		Sandpack (55' - 90' bgs)
80							#12 Pipe (60.2' - 90' bgs)
90					90.0	Bottom of borehole at 90.0 feet.	4475.1

Total Depth of Well 90' bgs

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**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** Wheatland, Wyoming  
**DATE STARTED** 7/8/2017 **COMPLETED** 7/8/2017 **GROUND ELEVATION** 4571.27 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** O'Keefe Drilling **GROUND WATER LEVELS:**  
**DRILLING METHOD** Sonic Track Rig **AT TIME OF DRILLING** ---  
**LOGGED BY** C. Ahrendt **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 587197.1 N 728402.3 E **▼ AFTER DRILLING** 80.21 ft / Elev 4491.06 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 0 (ft) Casing Type: 2" PVC Pipe
0							Top of Casing (estimated 2.5' ags)
5	SONIC	100		ML		SANDY SILT, with gravel, nonplastic, noncohesive; hard (>4.0 qu tsf), moist, brown	
7.0						4564.3	
10				SM		SILTY SAND, very fine to medium sand, with subrounded gravel; hard, moist, brown	
10.0						4561.3	Neat Cement (0' - 71' bgs)
15	SONIC	100		ML		SANDY SILT, with gravel, nonplastic; hard, moist, brown	
16.0						4555.3	2" Sch. 40 PVC Pipe (2.5' ags - 100' bgs)
20				SM		SILTY SAND, very fine to medium sand, with subrounded gravel; hard, moist, brown	
20.0						4551.3	
25	SONIC	100		ML		SANDY SILT, very fine to fine sand, with gravel, nonplastic, noncohesive; hard, moist, brown	
22.0						4549.3	
27				SM		SILTY SAND, very fine to fine sand, with subrounded gravel; hard, moist, brown	
27.0						4544.3	
30				GW		WELL GRADED GRAVEL, subrounded gravel, with very fine to medium sand; loose, moist, gray	
33.0						4538.3	
35	SONIC	100		ML		SILT, with sand, nonplastic, noncohesive; hard, wet (due to drilling), brown	
40						4531.3	

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION Wheatland, Wyoming

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
40							
41.0				QUARTZITE		QUARTZITE; hard, moist, brown	
45.0	SONIC	100		ML		SANDY SILT, nonplastic, noncohesive; soft, moist, brownish gray	
45.0						4530.3	
45.0						4526.3	
50				SANDSTONE		SANDSTONE, thinly bedded, sand grains visible; hard, moist, brown	
54.5	SONIC	100		SM		SILTY SAND, very fine to fine sand; loose, moist, brown	
54.5						4516.8	
60.0						4511.3	
60.0						WELL GRADED SAND, very fine to fine sand, with some silt; loose, moist, brown	
65	SONIC	100		SW		S.A.A., .5" layers of sandstone	
70						S.A.A., .5" lenses of quartzite	
75	SONIC	100				S.A.A., no quartzite or sandstone	
80.0				SW		4491.3	
80.5				GW		WELL GRADED SAND; medium stiff, moist to wet, brown	
80.5				GM		4490.8	
81.0						WELL GRADED GRAVEL, with silt and very fine to fine sand; loose, wet, brownish gray	
81.0						4490.3	
85	SONIC	100		SW-SM		WELL GRADED SAND, very fine to fine sand, with silt, some .5" interbedded lenses of sandstone; medium stiff, wet, brown	

Neat Cement (0' - 71' bgs)

3/8" Bentonite Chips (71'-75' bgs)  
 2" Sch. 40 PVC Pipe (2.5' ags - 100' bgs)

1020 Silica Sandpack (75' - 100' bgs)

0.010 Slotted Pipe (80' - 100' bgs)

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION Wheatland, Wyoming

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
90						WELL GRADED SAND, very fine to fine sand, with silt, some .5" interbedded lenses of sandstone; medium stiff, wet, brown	<p>1020 Silica Sandpack (75' - 100' bgs)                      0.010 Slotted Pipe (80' - 100' bgs)</p>
95	SONIC	100		SW-SM			
100					100.0		

4471.3  
 Total Depth of Well 100' BGS

EOB = 100' bgs, no refusal  
 Bottom of borehole at 100.0 feet.

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** Wheatland, Wyoming  
**DATE STARTED** 7/9/2017 **COMPLETED** 7/13/2017 **GROUND ELEVATION** 4566.97 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** O'Keefe Drilling **GROUND WATER LEVELS:**  
**DRILLING METHOD** Sonic Track Rig **AT TIME OF DRILLING** ---  
**LOGGED BY** C. Ahrendt **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 587153.4 N 729978.4 E **▼ AFTER DRILLING** 79.22 ft / Elev 4487.75 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 0 (ft) Casing Type: 2" PVC Pipe
0				SW-SC		WELL GRADED SAND, very fine to fine sand, with clay and gravel; medium stiff, moist, brown	<p>Top of Casing (flush mount)</p> <p>Neat Cement (0' - 74' bgs)</p> <p>2" Sch. 40 PVC Pipe (0' bgs - 100' bgs)</p>
3.0				ML		SILT, with very fine to fine sand, nonplastic, noncohesive; medium stiff, moist, brown	
5.0	SONIC	100		SW-SC		WELL GRADED SAND, very fine sand, with clay; medium stiff, moist, brown	
12.0				ML		S.A.A., little gravel	
17.4				ML		SILT, with very fine to fine sand, little gravel; hard, moist, grayish brown @17-17.4' bgs: S.A.A., organic-like odor, dark gray	
24.0				ML		S.A.A., no odor	
26.0				ML		S.A.A., with gravel	
26.0	SONIC	100		SW-SM		WELL GRADED SAND, very fine to fine sand, with silt; hard, moist, brownish gray	
26.0				ML		SILT, with sand, nonplastic, noncohesive; hard, moist, brownish gray	
32.0				SW-SM		WELL GRADED SAND, very fine to fine sand, with silt, no gravel; hard, moist, brownish gray	
38.0				GW		WELL GRADED GRAVEL, some very fine to fine sand, trace fines; loose, moist, brown	
40.0	SONIC	100		ML			

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION Wheatland, Wyoming

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
40						SILT, with sand, nonplastic, noncohesive; hard, moist, light brown WELL GRADED SAND, very fine to fine sand, with silt; dense, moist, brown	
45	SONIC	70		SW-SM			
50						50.0 WELL GRADED SAND, very fine to fine sand, little silt; loose, moist, brown 4517.0	
55	SONIC	100		SW		S.A.A., .5" interbedded quartzite	
60							
63.0						63.0 SANDSTONE, horizontal fractures, trace sand; hard, dry, white brown 4504.0	
63.5						63.5 SANDSTONE, horizontal fractures, trace sand; hard, dry, white brown 4503.5	
65	SONIC	100		SW		WELL GRADED SAND, very fine to fine; loose, moist, brown	
70							Neat Cement (0' - 74' bgs)
75	SONIC	100		SANDSTONE		75.0 SANDSTONE, horizontal fractures; hard, moist, whitish brown 4492.0	
76.0						76.0 SANDSTONE, horizontal fractures; hard, moist, whitish brown 4491.0	
80				SW		WELL GRADED SAND, very fine to fine sand, little silt; medium dense, moist, brown	3/8" Bentonite Chips (74'-78' bgs) 2" Sch. 40 PVC Pipe (0' bgs - 100' bgs)
81.0				SW		81.0 WELL GRADED SAND, very fine to fine sand; stiff, moist, brown 4487.0 SANDSTONE, massive, platy; hard, wet, brown 4486.0	1020 Silica Sandpack (78' - 100' bgs) 0.010 Slotted Pipe (80' - 100' bgs)
85	SONIC	100		SANDSTONE			

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION Wheatland, Wyoming

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
90				SANDSTONE	[Dotted pattern]	SANDSTONE, massive, platy; hard, wet, brown	<p>1020 Silica Sandpack (78' - 100' bgs)                      0.010 Slotted Pipe (80' - 100' bgs)</p>
91.0				SANDSTONE	[Dotted pattern]	4476.0	
92.0				SANDSTONE	[Dotted pattern]	SANDSTONE, weathered, with very fine to fine sand; stiff, wet, brown 4475.0	
95	SONIC	100		SW	[Dotted pattern]	WELL GRADED SAND, very fine to fine sand, some silt, trace gravel; medium stiff, wet, brown	
100					[Dotted pattern]	100.0	4467.0

EOB = 100' bgs, no refusal  
 Bottom of borehole at 100.0 feet.

Total Depth of Well 100' bgs

**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** Wheatland, Wyoming  
**DATE STARTED** 7/6/2017 **COMPLETED** 7/6/2017 **GROUND ELEVATION** 4590.95 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** O'Keefe Drilling **GROUND WATER LEVELS:**  
**DRILLING METHOD** Sonic Track Rig **AT TIME OF DRILLING** ---  
**LOGGED BY** C. Ahrendt **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 586231.9 N 728742.5 E **▼ AFTER DRILLING** 93.61 ft / Elev 4497.34 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 0 (ft) Casing Type: 2" PVC Pipe
0						SILT, with sand, little gravel, nonplastic, noncohesive; stiff, moist (wet due to drilling), light brownish gray	
5	SONIC	80		ML		S.A.A., increasing gravel	
10				GW		10.0 4581.0 11.0 4580.0 WELL GRADED GRAVEL, rounded gravel, with silt and very fine to fine sand; loose, moist, light brownish gray	
15	SONIC	100		ML		SILT, with very fine sand, nonplastic, noncohesive; stiff, moist (wet due to drilling), light brownish gray	
16.0						16.0 4575.0 SANDY SILT, very fine sand, nonplastic, noncohesive; stiff, moist, light brownish gray	
20				ML			
25	SONIC	100					
27.0				ML		27.0 4564.0 GRAVELLY SILT, nonplastic, noncohesive; stiff, moist, brown	
30							
30.0						30.0 4561.0 SANDY SILT, with gravel, nonplastic, noncohesive; stiff, moist, light brown	
35	SONIC	100		ML			
40						40.0 4551.0	

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION Wheatland, Wyoming

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
40							
44.0				SW		WELL GRADED SAND, very fine to medium sand; medium stiff, moist, brown	<p>Neat Cement (0' - 86.5' bgs)                      2" Sch. 40 PVC Pipe (0' bgs - 120' bgs)</p>
45.0	SONIC	100		ML		SILT, with very fine sand, trace rounded gravel, nonplastic, noncohesive; medium stiff, moist, light brown	
50.5				SW		WELL GRADED SAND, very fine to medium sand; loose, moist, brown, no oxidation	
55.0	SONIC	100		SANDSTONE		SANDSTONE; very stiff, dry, brown	
59.0							
60.0				SW		WELL GRADED SAND, very fine to medium sand, little silt, trace gravel; loose, moist, brown	
65.0	SONIC	100				WELL GRADED SAND, very fine to fine sand, with <1" interbedded sandstone lenses, some silt; loose, moist, brown	
70.0				SW		S.A.A., with fine silt and .5-1" sandstone lenses	
75.0	SONIC	100					
81.0				SANDSTONE		SANDSTONE, blocky, with little sand; ahrd, dry, brown	
82.0							
85.0	SONIC	100		SW		WELL GRADED SAND, very fine to fine sand, some silt, no gravel; loose, moist, brown	

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION Wheatland, Wyoming

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
90						WELL GRADED SAND, very fine to fine sand, some silt, no gravel; loose, moist, brown	<p>3/8" Bentonite Chips (86.5'-89.5' bgs)                  2" Sch. 40 PVC Pipe (0' bgs - 120' bgs)                  Natural Cave In</p>
95	SONIC	100		SW	S.A.A., medium dense		
100					S.A.A., wet		
100.0					100.0 4491.0		
				QUARTZITE		101.0 QUARTZITE, cleavage planes; very hard, moist, brown	<p>1020 Silica Sandpack (97' - 120' bgs)                  0.010 Slotted Pipe (100' - 120' bgs)</p>
105	SONIC	100		SM	SILTY SAND, very fine to fine sand; medium stiff, wet, brown, no oxidation or staining		
110					111.0 4480.0		
115	SONIC	100		SW	WELL GRADED SAND, very fine to fine sand, with silt; medium dense, wet, brown		
120					S.A.A., .5" sandstone lenses	120.0 4471.0	

EOB = 120' bgs, no refusal  
 Bottom of borehole at 120.0 feet.

Total Depth of Well 120' bgs

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**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** Wheatland, Wyoming  
**DATE STARTED** 6/29/2017 **COMPLETED** 7/1/2017 **GROUND ELEVATION** 4591.51 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** O'Keefe Drilling **GROUND WATER LEVELS:**  
**DRILLING METHOD** Sonic Track Rig **AT TIME OF DRILLING** ---  
**LOGGED BY** C. Ahrendt **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 586215.1 N 729312.9 E **▼ AFTER DRILLING** 95.22 ft / Elev 4496.29 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 0 (ft) Casing Type: 2" PVC Pipe
0						GRAVELLY CLAY, lean, with sand, nonplastic, noncohesive, massive, no odor or staining; hard (>4.0 qu tsf), moist, grayish brown	Top of Casing (flush mount)
5	SONIC	100					
10				CL		10.0 S.A.A., decreasing gravel 4581.5	Neat Cement (0' - 93.5' bgs)
15	SONIC	100				15.0 S.A.A., increasing gravel 4576.5	2" Sch. 40 PVC Pipe (0' bgs - 120' bgs)
20						20.0 WELL GRADED GRAVEL, rounded gravel, with very fine to coarse sand and clay; dense, moist, light brownish gray 4571.5	
22				GW-GC		22.0 WELL GRADED SAND, very fine to medium sand, with clay; hard, moist, light brown 4569.5	
25	SONIC	100					
30				SW-SC		30.0 S.A.A., with rounded gravel 4561.5	
35	SONIC	100				35.0 S.A.A., little gravel 4556.5	
40						40.0 4551.5	

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION Wheatland, Wyoming

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
40							
43.0						SILT, with very fine sand, nonplastic, noncohesive; hard, moist, light brown	
45	SONIC	100		SW-SM		WELL GRADED SAND, very fine to medium sand, with silt; loose, moist, light brown, mottled gray and orange	
48.0						WELL GRADED SAND, fine to coarse sand, little silt; loose, moist, dark gray	
49.5				SW		S.A.A., with rounded gravel	
50						SILT, trace very fine sand, nonplastic, noncohesive, soft; loose, moist, light brown	
51.0						S.A.A., hard, moist	
55	SONIC	100				S.A.A., hard	
60				ML		SANDY SILT, very fine sand, nonplastic, noncohesive; medium stiff, moist, light brown	
65	SONIC	100				SANDSTONE; hard, moist, brown	
70				ML		SILTY SAND, fine sand; medium dense, moist, light brown	
74.5						S.A.A., little gravel	
75	SONIC	100		SANDSTONE			
80				SM			
85	SONIC	70					

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Neat Cement (0' - 93.5' bgs)  
 2" Sch. 40 PVC Pipe (0' bgs - 120' bgs)

CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION Wheatland, Wyoming

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
89.0				SM		SILTY SAND, fine sand, little gravel; medium dense, moist, light brown	<p>3/8" Bentonite Chips (93.5'-96.0' bgs)                  2" Sch. 40 PVC Pipe (0' bgs - 120' bgs)</p> <p>1020 Silica Sandpack (96' - 120' bgs)                  0.010 Slotted Pipe (100' - 120' bgs)</p> <p>Total Depth of Well 120' bgs</p>
90.0				SANDSTONE		SANDSTONE, thinly bedded; hard, moist, brown	
95.0	SONIC 40			ML		SILT, nonplastic, noncohesive, massive; very stiff, moist, light grayish brown	
100.0							
100.0						SILTY SAND, very fine sand, little sandstone fragments; medium stiff, wet, brown, no oxidation (100-105' bgs: expansive soil, expanded 10%)	
105.0	SONIC 100			SM		S.A.A., stiff (105-110' bgs: expansive soil, expanded 10%)	
110.0	SONIC 100					WELL GRADED SAND, very fine to fine, with sandstone; very stiff, wet, light brown (110-115' bgs: expansive soil, expanded 10%)	
113.0				SW			
115.0				MUDSTONE		MUDSTONE, with very fine to fine sand, layered, thinly bedded, platy; very stiff, moist, light brown (115-120' bgs: expansive soil, expanded 10%)	
120.0	SONIC 100			ML		SILT, with sand, very fine sand, nonplastic, noncohesive; medium stiff, moist, light brown	
120.0						EOB = 120' bgs, no refusal Bottom of borehole at 120.0 feet.	

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**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** Wheatland, Wyoming  
**DATE STARTED** 6/23/2017 **COMPLETED** 6/27/2017 **GROUND ELEVATION** 4592.21 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** O'Keefe Drilling **GROUND WATER LEVELS:**  
**DRILLING METHOD** Sonic Track Rig **AT TIME OF DRILLING** ---  
**LOGGED BY** C. Ahrendt **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 586198 N 729809.7 E **▼ AFTER DRILLING** 96.75 ft / Elev 4495.46 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	ELEVATION (ft)	WELL DIAGRAM
0								Casing Top Elev: 0 (ft) Casing Type: 2" PVC Pipe
0.8				CL		Top .75" road bed	4591.5	Top of Casing (flush mount)
5	SONIC	80		ML		SANDY SILT, very fine sand, nonplastic, noncohesive; soft, moist, grayish brown		
10				ML		SILT, with sand, nonplastic, noncohesive; very stiff (3.0 qu tsf), moist, brownish gray	4582.2	Neat Cement (0' - 98.6' bgs)
12.0	SONIC	90		ML		SANDY SILT, trace gravel, nonplastic, noncohesive, no odor or staining; medium dense, moist, brownish gray	4580.2	2" Sch. 40 PVC Pipe (0' bgs - 125' bgs)
14.0				ML			4578.2	
15	SONIC	90		CL		SANDY CLAY, lean, subrounded gravel, nonplastic, noncohesive, no oxidation or staining; soft, moist (wet due to drilling), light grayish brown S.A.A., decreasing gravel; stiff		
20				CL		SANDY CLAY, lean; hard (>4.0 qu tsf), moist, light brownish gray	4572.2	
25	SONIC	95		CL		S.A.A., increasing sand, little subangular gravel; moist		
30				GW		WELL GRADED GRAVEL, subrounded gravel; loose, moist (wet due to drilling), gray	4562.2	
31.0				CL		SANDY CLAY, with gravel; very stiff, moist, grayish brown	4561.2	
35	SONIC	80		CL			4557.2	
35.0				SW		WELL GRADED SAND, very fine to fine sand, with white deposits (calcite); medium stiff, moist, brown, no oxidation		
40								

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION Wheatland, Wyoming

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
40							
42.0				SW		S.A.A., dark brown	
						SILTY SAND; loose, moist (wet due to drilling), light brownish gray	
45	SONIC	80					
						S.A.A., very fine sand; hard, brown, no oxidation	
50				SM			
						S.A.A., thin lenses of 1-2 mm of calcite deposits	
55	SONIC	100					
						S.A.A., light olive green with brown oxidation spots	
58.5						S.A.A., trace gravel; light brown	
60.0				SANDSTONE		SANDSTONE, very fine to medium sand, thinly bedded; hard, moist, light brown	
60.3				QUARTZITE		3" of quartzite, hard, laminated, visible sand	
						SAND, with silt; loose, moist, light brown	
						S.A.A., blocky lenses of sand with silt, very fine to fine sand; moist	
65	SONIC	100		SW-SM			
						S.A.A., hard	
						S.A.A., very fine to fine sand, soft; loose	
70				QUARTZITE			
						S.A.A., with little gravel	
						3" of quartzite, hard, laminated, visible sand	
						SAND, with silt, very fine to fine sand, no odor or stain; loose, moist (wet due to drilling), brown	
75	SONIC	30		SP-SM			
80							
						SANDY SILT, very fine sand, nonplastic, noncohesive; soft, moist, brown	
85	SONIC	100		ML			

Neat Cement (0' - 98.6' bgs)  
 2" Sch. 40 PVC Pipe (0' bgs - 125' bgs)

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CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION Wheatland, Wyoming

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
90				ML		SANDY SILT, very fine sand, nonplastic, noncohesive; soft, moist, brown	
90.0				ML		4502.2	
91.0				QUARTZITE		SANDY SILT, with 1" sandstone lenses, nonplastic, noncohesive; loose, moist, brown	
92.0				SILTSTONE		4501.2	
92.0						QUARTZITE, layered; hard, moist, gray	
93.0						4500.2	
93.0						SILTSTONE, little very fine sand; hard, moist, brown	
93.0						4499.2	
95	SONIC	30		SM		SILTY SAND, very fine sand; medium stiff, moist, brown, no oxidation	
98.0				QUARTZITE		4494.2	
98.5						QUARTZITE, fractured; hard, wet, white gray	
98.5						4493.7	
100				ML		SILT, with very fine sand, nonplastic, noncohesive; medium stiff, moist	
102.0						4490.2	
105	SONIC	85		QUARTZITE		QUARTZITE; hard, moist, white gray	
105.0						4487.2	
110	SONIC	0		ML		SILT, with very fine sand and thin lenses of interbedded sandstone, nonplastic, noncohesive; medium stiff, moist, brown	
113.0						4479.2	
115	SONIC	0		ML		GRAVELLY SILT, angular gravel, with very fine sand, nonplastic, noncohesive; soft, wet, light brown	
120						4471.7	
120.5				SW-SM		WELL GRADED SAND, very fine sand, with silt; hard, wet, brown	
125.0	SONIC	100				4467.2	
125						EOB = 125' bgs, no refusal Bottom of borehole at 125.0 feet.	

3/8" Bentonite Chips (98.6'-101' bgs)  
 2" Sch. 40 PVC Pipe (0' bgs - 125' bgs)

1020 Silica Sandpack (96' - 125' bgs)  
 0.010 Slotted Pipe (105' - 125' bgs)

Total Depth of Well 125' bgs

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**CLIENT** Basin Electric **PROJECT NAME** Laramie River Station  
**PROJECT NUMBER** 60506860 **PROJECT LOCATION** Wheatland, Wyoming  
**DATE STARTED** 6/20/2017 **COMPLETED** 6/28/2017 **GROUND ELEVATION** 4591.84 ft **HAMMER TYPE** Not Applicable  
**DRILLING CONTRACTOR** O'Keefe Drilling **GROUND WATER LEVELS:**  
**DRILLING METHOD** Sonic Track Rig **AT TIME OF DRILLING** ---  
**LOGGED BY** C. Ahrendt **CHECKED BY** A. Lanning **AT END OF DRILLING** ---  
**COORDINATES** 586189 N 730213.8 E **▼ AFTER DRILLING** 97.06 ft / Elev 4494.78 ft

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
0							Casing Top Elev: 0 (ft) Casing Type: 2" PVC Pipe
0.5				GW	●	WELL GRADED GRAVEL (road bed), with sand; loose, dry, gray	Top of Casing (flush mount)
1.0				ML	▨	SILT, with sand, bedded, nonplastic, noncohesive; stiff, dry, brown No recovery	
5	SONIC	10					
10						10.0	4581.8
10				ML	▨	SILT, with sand, bedded, nonplastic, noncohesive; soft, moist, light brown @10-12' bgs: with WHITE SPOTS	Neat Cement (0' - 95' bgs)
15	SONIC	100					2" Sch. 40 PVC Pipe (0' bgs - 120' bgs)
16.5						16.5	4575.3
20						WELL GRADED SAND, very fine to fine, with silt; hard (>4.0 qu tsf), moist, brown, no oxidation or staining	
25	SONIC	100				S.A.A., medium dense, light brown	
30							
30				SW-SM	▨	S.A.A., very dense blocky, white calcite deposits, no odor or staining	
35	SONIC	60					
36.5						36.5	4555.3
37.5				MUDSTONE	▨	MUDSTONE, blocky, bedded; hard (>4.0 qu tsf), moist, brown (10YR 4/3)	
37.5						37.5	4554.3
40				SANDSTONE	▨	SANDSTONE, little silt and sand; dense, moist, light brown	
40.0						40.0	4551.8

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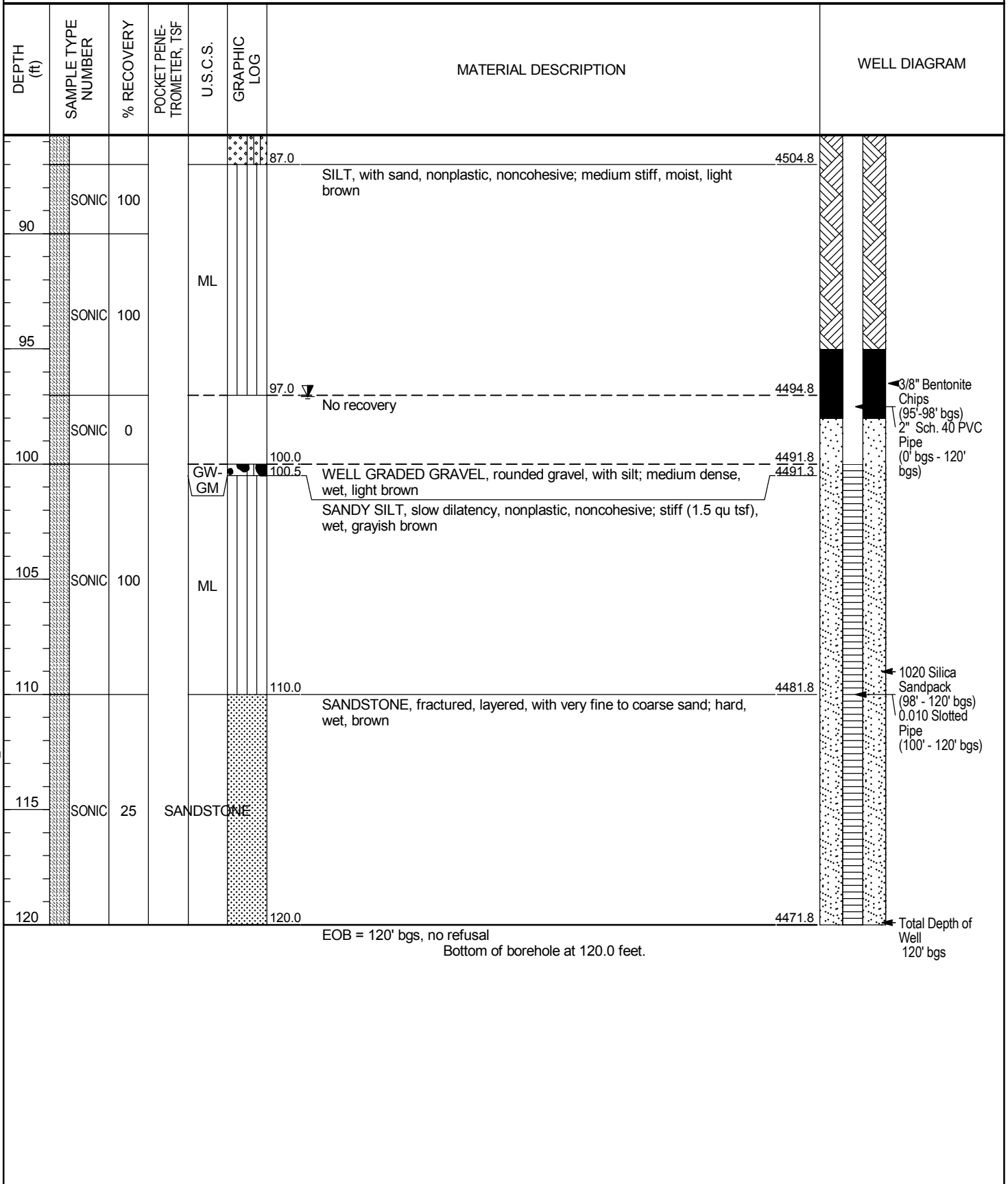


CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION Wheatland, Wyoming

DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE-TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
40						No recovery	
45	SONIC	30					
47.0						4544.8	
50				SANDSTONE		SANDSTONE, some very fine sand, thinly bedded; dense, moist, light brown	
55	SONIC	30					
57.0						4534.8	
60				SW		WELL GRADED SAND, very fine to fine sand, trace silt; medium dense, moist, grayish brown S.A.A., dense, moist, light brown	
60.0						4531.8	
65	SONIC	50		ML		GRAVELLY SILT, subrounded gravel, with very fine to fine sand, nonplastic, noncohesive; soft, moist, light brown	
70						4521.8	
75	SONIC	100				WELL GRADED SAND, very fine sand, with silt; loose, moist, light brown, no oxidation or staining	Neat Cement (0' - 95' bgs)
80				SW-SM		S.A.A., medium stiff, light brown	2" Sch. 40 PVC Pipe (0' bgs - 120' bgs)
85	SONIC	100					

WELL LOG - GDT - 9/21/17 11:28 - C:\BASIN ELECTRIC SEPT 2017\BASINELECTRIC\_091917.GPJ

CLIENT Basin Electric PROJECT NAME Laramie River Station  
 PROJECT NUMBER 60506860 PROJECT LOCATION Wheatland, Wyoming



WELL LOG - GDT - 9/21/17 11:28 - C:\BASIN ELECTRIC SEPT 2017\BASINELECTRIC\_091917.GPJ



Project Name: Basin Electric Laramie River Station  
 Client: Basin Electric Laramie River Station  
 Project Number: 60577052

Boring ID: MW-38C

Date(s) Drilled	4/4/19 - 4/6/19	Logged By	J. Hurshman	Checked By		Total Depth of Borehole (ft)		Depth to Water (bgs)	
Drilling Method	Hollow Stem Auger	Diameter of Borehole (in)	8 1/4 inch OD			Ground Surface Elevation (ft-msl)	TBD		
Drill Rig Type	CME	Drilling Company	Inberg Miller			Groundwater Elevation (ft-msl)	TBD		
Driller's Name	Barry	Sampler Type	5 foot core barrel			Measuring Point Elevation (ft-msl)	TBD		
Description of Sample Location						Northing	TBD		
						Easting	TBD		

Depth (ft-bgs)	SAMPLES			USCS Symbol	PID (ppm)	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Sample ID					
1						Blind Drilled to 75 ft See MW-38B boring log for details		
2								
3								
4								
5								
6								
7								
8								
9								
10								
11								
12								
13								
14								
15								
16								
17								
18								
19								
20								



Project Name: Basin Electric Laramie River Station  
 Client: Basin Electric Laramie River Station  
 Project Number: 60577052

Boring ID: MW-38C

Date(s) 4/4/19 - 4/6/19	Logged By J. Hurshman	Checked By	Total Depth of Borehole (ft)	Depth to Water (bgs)
Drilling Method Hollow Stem Auger	Diameter of Borehole (in)	8 1/4 inch OD	Ground Surface Elevation (ft-msl)	TBD
Drill Rig Type CME	Drilling Company	Inberg Miller	Groundwater Elevation (ft-msl)	TBD
Driller's Name Barry	Sampler Type	5 foot core barrel	Measuring Point Elevation (ft-msl)	TBD
Description of Sample Location			Northing	TBD
			Eastings	TBD

Depth (ft-bgs)	SAMPLES			USCS Symbol	Graphic Log	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Sample ID					
21						Blind Drilled to 75 ft See MW-38B boring log for details		
22								
23								
24								
25								
26								
27								
28								
29								
30								
31								
32								
33								
34								
35								
36								
37								
38								
39								
40								



Project Name: Basin Electric Laramie River Station  
 Client: Basin Electric Laramie River Station  
 Project Number: 60577052

Boring ID: MW038C

Date(s) 4/4/19 - 4/6/19	Logged By J. Hurshman	Checked By	Total Depth of Borehole (ft)	Depth to Water (bgs)
Drilled Method Hollow Stem Auger	Diameter of Borehole (in)	8 1/4 inch OD	Ground Surface Elevation (ft-msl)	TBD
Drill Rig Type CME	Drilling Company	Inberg Miller	Groundwater Elevation (ft-msl)	TBD
Driller's Name Barry	Sampler Type	5 foot core barrel	Measuring Point Elevation (ft-msl)	TBD
Description of Sample Location			Northing Easting	TBD

Depth (ft-bgs)	SAMPLES			USCS Symbol	Graphic Log	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Sample ID					
41						Blind Drilled to 75 ft See MW-38B boring log for details		
42								
43								
44								
45								
46								
47								
48								
49								
50								
51								
52								
53								
54								
55								
56								
57						hard sandstone lens drilled through (~1 foot thick)		
58								
59								
60								



Project Name: Basin Electric Laramie River Station  
 Client: Basin Electric Laramie River Station  
 Project Number: 60577052

Boring ID: MW-38C

Date(s) 4/4/19 - 4/6/19	Logged By J. Hurshman	Checked By	Total Depth of Borehole (ft)	Depth to Water (bgs)
Drilled Method Hollow Stem Auger	Diameter of Borehole (in)	8 1/4 inch OD	Ground Surface Elevation (ft-msl)	TBD
Drill Rig Type CME	Drilling Company Inberg Miller		Groundwater Elevation (ft-msl)	TBD
Driller's Name Barry	Sampler Type 5 foot core barrel		Measuring Point Elevation (ft-msl)	TBD
Description of Sample Location			Northing Easting	TBD

Depth (ft-bgs)	SAMPLES			USCS Symbol	Graphic Log	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Sample ID					
61						Blind Drilled to 75 ft See MW-38B boring log for details		
62								
63								
64								
65								
66								
67								
68								
69								
70								
71								
72								
73								
74								
75						end of blind drilling - switch to 5 foot core barrel		
76						very fine to fine sand, well sorted, homogeneous, brown, wet, loosely packed, few interbedded white burrow casts 79-80 ft ( 1-3 mm diameter)		
77	1	75	N/A	SP	N/A			
78								
79								
80								



Project Name: Basin Electric Laramie River Station  
 Client: Basin Electric Laramie River Station  
 Project Number: 60577052

Boring ID: MW-38C

Date(s) 4/4/19 - 4/6/19	Logged By J. Hurshman	Checked By	Total Depth of Borehole (ft)	Depth to Water (bgs)
Drilling Method Hollow Stem Auger	Diameter of Borehole (in)	8 1/4 inch OD	Ground Surface Elevation (ft-msl)	TBD
Drill Rig Type CME	Drilling Company	Inberg Miller	Groundwater Elevation (ft-msl)	TBD
Driller's Name Barry	Sampler Type	5 foot core barrel	Measuring Point Elevation (ft-msl)	TBD
Description of Sample Location			Northing Easting	TBD

Depth (ft-bgs)	SAMPLES			USCS Symbol	Graphic Log	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Sample ID					
81				SP	N/A	as above, little recovery 80-82 ft		
82	2	60	N/A			82 ft: fine sand as above, wet, few interbedded burrow casts-white		
83				CL		82.7: gray thin clay lens, ~1 cm thick, soft clay, few lenses from 82.7 to 82.8 ft.		
84								
85						85-90 ft: fine sand as above, well sorted, wet, easy to drill, flowing sand from 85-86.5 ft bgs, minor silt or very fine sand		
86								
87	3	100	N/A					
88				SP				
89								
90						90-95 ft: fine sand as above, tightly packed, slow to drill, not cemented		
91								
92	4	50	N/A					
93								
94								
95						95-100 ft: as above, tight sand, interbedded white burrow casts, wet, top foot is liquified (soupy), possibly due to drilling - slight gray color		
96								
97	5	100	N/A					
98						last 2 feet slow hard drilling		
99								
100								



Project Name: Basin Electric Laramie River Station  
 Client: Basin Electric Laramie River Station  
 Project Number: 60577052

Boring ID: MW-38C

Date(s) 4/4/19 - 4/6/19	Logged By J. Hurshman	Checked By	Total Depth of Borehole (ft)	Depth to Water (bgs)
Drilled Method Hollow Stem Auger	Diameter of Borehole (in)	8 1/4 inch OD	Ground Surface Elevation (ft-msl)	TBD
Drill Rig Type CME	Drilling Company	Inberg Miller	Groundwater Elevation (ft-msl)	TBD
Driller's Name Barry	Sampler Type	5 foot core barrel	Measuring Point Elevation (ft-msl)	TBD
Description of Sample Location			Northing Easting	TBD

Depth (ft- bgs)	SAMPLES			USCS Symbol	Graphic Log	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Sample ID					
101			N/A	SP	N/A	as above, fine to very fine sand, wet, trace white burrow casts, few hard nodules of sand, top foot is soupy sand (liquified), trace silt in sand		
102	6	90						
103								
104								
105						silty fine sand, very soft and soupy, wet 105 to 107 ft, then more compact and tight sand, light gray/medium grey thin lens at 107.5 ft in sand. Thinly bedded silt lenses < 2 mm thick from 108 to 109 feet.		
106								
107	7	100						
108								
109								
110						as above, top 2.1 feet is wet and soupy fine sand		
111								
112	8	50				112-115: fine sand with interbedded 2 mm thick silt lessen every 1 to 1.5 cm, wet, tan to brown color		
113								
114								
115						as above, top 2.5 feet very soupy, falls out of core barrel		
116								
117	9	60						
118						118-120: interbedded very fine sand and silt, wet, brown to tan,		
119								
120								





Project Name: Basin Electric Laramie River Station  
 Client: Basin Electric Laramie River Station  
 Project Number: 60577052

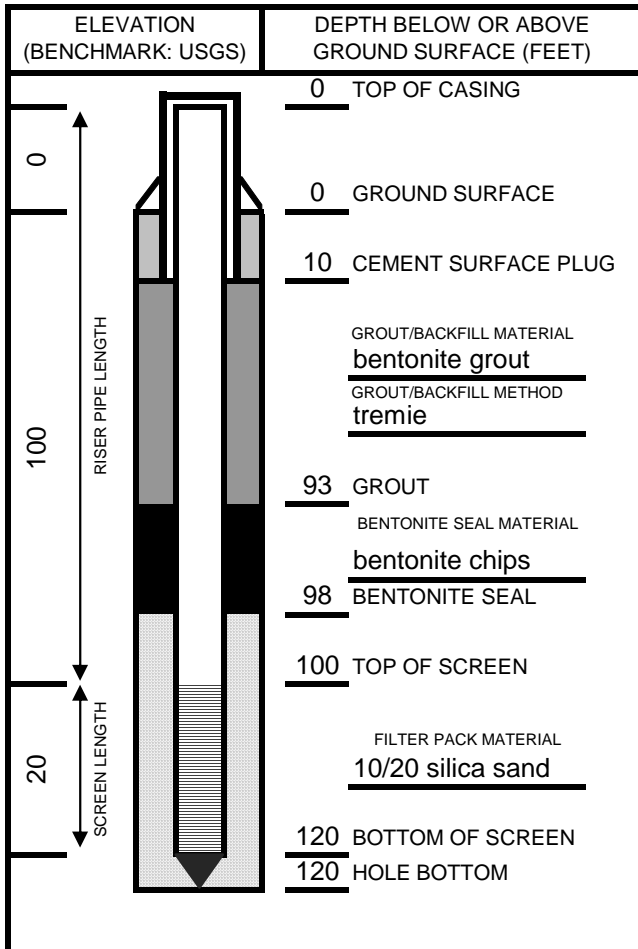
Boring ID: MW-38C

Date(s) 4/4/19 - 4/6/19	Logged By J. Hurshman	Checked By	Total Depth of Borehole (ft)	Depth to Water (bgs)
Drilling Method Hollow Stem Auger	Diameter of Borehole (in)	8 1/4 inch OD	Ground Surface Elevation (ft-msl)	TBD
Drill Rig Type CME	Drilling Company	Inberg Miller	Groundwater Elevation (ft-msl)	TBD
Driller's Name Barry	Sampler Type	5 foot core barrel	Measuring Point Elevation (ft-msl)	TBD
Description of Sample Location			Northing	TBD
			Eastings	TBD

Depth (ft-bgs)	SAMPLES			USCS Symbol	Graphic Log	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Sample ID					
121	10	100	N/A	SP	N/A	fine sand with silt as above, flowing sands		
122						harder drilling 122-126 feet		
123						minor sandstone chunks stuck on augers and core barrel		
124						605		
125						blind drilled 125 to 130 feet, no recovery		
126								
127								
128								
129								
130						END OF BORING = 130 FEET BGS		
131						Well Completion		
132						0.0-1.0 ft: cement for above-grade well protection		
133						1.0-107.5 ft: bentonite grout with cement		
134						107.5-112.3 ft: 3/8" diameter bentonite pellets		
135						112.3-130.0 ft: 10/20 silica sandpack		
136						0-114.0 ft: 2" diameter, schedule 80 PVC, threaded riser pipe		
137						114.0-125.0 ft: Pre-Packed Well Screen (Two 5-foot segments with 3/4' riser in between segments)		
138						Note: Drillers overdrilled well to compensate for flowing sand		
139								
140								

# WELL CONSTRUCTION DATA

PROJECT NAME: Basin Electric LRS Well Replacement	WELL ID: MW-53BR
PROJECT NO: 60727167	DATE INSTALLED: 4/20/2024
INSTALLED BY: David Buhl	CHECKED BY:



CASING AND SCREEN DETAILS	
TYPE OF RISER:	PVC
PIPE SCHEDULE:	Schedule 40
PIPE JOINTS:	N/A
SOLVENT USED:	N/A
SCREEN TYPE:	Slotted
SCR. SLOT SIZE:	0.010 INCH
BOREHOLE DIAMETER	6 3/8 IN. FROM 0 TO 120 FT. IN. FROM TO FT.
SURF. CASING DIAMETER	2 IN. FROM 0 TO 120 FT. IN. FROM TO FT.

WELL DEVELOPMENT	
DEVELOPMENT METHOD:	Not developed at time of installation
TIME DEVELOPING:	HOURS
WATER REMOVED:	GALLONS
WATER ADDED:	GALLONS
WATER CLARITY BEFORE / AFTER DEVELOPMENT	
CLARITY BEFORE:	
COLOR BEFORE:	
CLARITY AFTER:	
COLOR AFTER:	
ODOR (IF PRESENT):	

NOTES:

Materials used in annulus:

- 14 bags of bentonite grout
- 11 bags of 10/20 silica sand
- 5 bags of cement for surface plug
- 2 bags of bentonite chips

WATER LEVEL SUMMARY		
SWE MEASUREMENT	DATE	TIME
BEFORE DEVELOPING	T/PVC	
AFTER DEVELOPING:	T/PVC	
OTHER	T/PVC	
OTHER	T/PVC	
PROTECTIVE COVER AND LOCK INSTALLED? <input checked="" type="checkbox"/> YES <input type="checkbox"/> NO PERMANENT, LEGIBLE WELL LABEL ADDED? <input type="checkbox"/> YES <input checked="" type="checkbox"/> NO		



Project Name: Laramie River Station Well Replacement  
 Client: Basin Electric  
 Project Number: 60727167

Boring ID: MW-53BR

Date(s) Drilled	April 17-19, 2024	Logged By	David Buhl	Checked By		Total Depth of Borehole (ft bgs)	120	Depth to Water (bgs)	106
Drilling Method	Sonic	Diameter of Borehole (in)	6 3/8			Ground Surface Elevation (ft-msl)	4590.8		
Drill Rig Type	Pro Sonic	Drilling Company	Cascade			Groundwater Elevation (ft-msl)	4484.3		
Driller's Name	Ryan Miller	Sampler Type	6 inch diameter, 2.5 foot long sample bags			Measuring Point Elevation (ft-msl)	4590.3		
Description of Sample Location	On an elevated berm road between two coal-ash settling ponds, approximately 500 feet west of the northeast corner of the settling pond berm road.					Northing	586183.818		
						Easting	730230.477		

Depth (ft-bgs)	SAMPLES				USCS Symbol	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Core Length (Inches)	Core Depth (ft bgs)				
1	Excavated to around 10 feet bgs via Hydrovac No recovery from hydrovac excavation	No recovery from hydrovac excavation	N/A	N/A	N/A	No recovery through the first 10 feet bgs due to drilling into the hydrovac pothole	Concrete	Concrete
2								
3								
4								
5								
6								
7								
8								
9								
10								
11	100				ML	10 YR 5/3 brown sandy silt, mottled, soft, moist, medium plasticity, ~20% fine sand	Bentonite Grout	Schedule 40 PVC Casing
12		24"	12					
13	100				ML	fewer cobbles	Bentonite Grout	Bentonite Grout
14		30"	14.5					
15	100				SW	10 YR 4/3 brown silty, gravelly sandstone, loose, moist, very fine - very coarse grains, ~20% gravel and cobbles, sand grains are high sphericity, subrounded, well graded	Bentonite Grout	Bentonite Grout
16		30"	17					
17	100				SW		Bentonite Grout	Bentonite Grout
18		30"	19.5					
19	93				CL	10 YR 6/2 light brownish gray sandy clay, medium stiff, moist, medium plasticity, ~20% fine sand	Bentonite Grout	Bentonite Grout
20		28"	22					



Project Name: Laramie River Station Well Replacement  
 Client: Basin Electric  
 Project Number: 60727167

Boring ID: MW-53BR

Date(s) Drilled	April 17-19, 2024	Logged By	David Buhl	Checked By		Total Depth of Borehole (ft bgs)	120	Depth to Water (bgs)	106
Drilling Method	Sonic	Diameter of Borehole (in)	6 3/8			Ground Surface Elevation (ft-msl)	4590.8		
Drill Rig Type	Pro Sonic	Drilling Company	Cascade			Groundwater Elevation (ft-msl)	4484.3		
Driller's Name	Ryan Miller	Sampler Type	6 inch diameter, 2.5 foot long sample bags			Measuring Point Elevation (ft-msl)	4590.3		
Description of Sample Location	On an elevated berm road between two coal-ash settling ponds, approximately 500 feet west of the northeast corner of the settling pond berm road.					Northing	586183.818		
						Easting	730230.477		

Depth (ft-bgs)	SAMPLES				USCS Symbol	MATERIAL DESCRIPTION	Well Construction		
	Run Number	Recovery (%)	Core Length (Inches)	Core Depth (ft bgs)					
21	93		28"	22	CL	Same as above with some gravel, mottled	Bentonite Grout	Schedule 40 PVC Casing	Bentonite Grout
22					SW	10 YR 5/3 brown clayey, gravelly sand, mottled loose, moist, very fine - very coarse, ~15% clay, ~20% gravel, high sphericity, subrounded, well graded.			
23	93		28"	24.5	ML	10 YR 6/3 pale brown sandy silt, mottled, medium stiff, medium - low plasticity, slightly moist, sand is very fine - fine			
24					ML	10 YR 5/3 brown sandy silt, stiff, moist, low plasticity, ~20 fine sand, grayish white nodules (possibly gypsum)			
25	93		28"	27	ML				
26					ML				
27	100		30"	29.5	CH	10 YR 5/4 yellowish brown sandy clay, mottled, soft, high plasticity, moist, ~20 very fine - fine sand			
28					ML	10 YR 5/3 brown sandy silt, dry, soft - medium stiff, mottled, low plasticity, ~20% fine sand			
29	100		30"	32	SM	10 YR 4/3 brown silty sand, moist, loose, fine, ~20% silt, high sphericity, subrounded, poorly graded			
30					SM	10 YR 6/2 light brownish gray silty sand, slightly moist, very loose, very fine sand, ~20% silt			
31	93		28"	34.5	SM				
32					SM				
33	90		27"	37	ML	10 YR 3/4 dark yellowish brown sandy silt, slightly moist, stiff, low - medium plasticity, ~20% very fine - fine sand			
34					ML	10 YR 5/3 brown silty sand, moist, dense, very fine - fine sand, between 10% - 20% silt content			
35	100		18"	38.5	SM				
36					SM				
37	93		28"	41	SM				
38					SM				
39									
40									



Project Name: Laramie River Station Well Replacement  
 Client: Basin Electric  
 Project Number: 60727167

Boring ID: MW-53BR

Date(s) Drilled	April 17-19, 2024	Logged By	David Buhl	Checked By		Total Depth of Borehole (ft bgs)	120	Depth to Water (bgs)	106
Drilling Method	Sonic	Diameter of Borehole (in)	6 3/8			Ground Surface Elevation (ft-msl)	4590.8		
Drill Rig Type	Pro Sonic	Drilling Company	Cascade			Groundwater Elevation (ft-msl)	4484.3		
Driller's Name	Ryan Miller	Sampler Type	6 inch diameter, 2.5 foot long sample bags			Measuring Point Elevation (ft-msl)	4590.3		
Description of Sample Location					On an elevated berm road between two coal-ash settling ponds, approximately 500 feet west of the northeast corner of the settling pond berm road.	Northing	586183.818		
						Easting	730230.477		

Depth (ft-bgs)	SAMPLES				USCS Symbol	MATERIAL DESCRIPTION	Well Construction		
	Run Number	Recovery (%)	Core Length (inches)	Core Depth (ft-bgs)					
41		93	28"	41		Same as above			
42		90							
43	4		27"	43.5					
44									
45		80							
46			24"	46		Slightly moist, sand is very fine, otherwise same as above			
47		100	12"	47					
48		90			SM				
49			27"	49.5					
50		87							
51	5		26"	52		becoming more silty			
52		93							
53			28"	54.5					
54									
55		93				more sandy			
56			28"	57					
57									
58	6	97			CH	10 YR 4/2 dark grayish brown sandy clay, moist, soft, high plasticity, between 30% - 40% fine sand			
59			29	59.5					
60		93	28	62	SM	10 YR 6/3 pale brown silty sand, loose, moist - dry, very fine sand, ~20% silt and clay, some gravelly zones			



Project Name: Laramie River Station Well Replacement  
 Client: Basin Electric  
 Project Number: 60727167

Boring ID: MW-53BR

Date(s) Drilled	April 17-19, 2024	Logged By	David Buhl	Checked By		Total Depth of Borehole (ft bgs)	120	Depth to Water (bgs)	106	
Drilling Method	Sonic	Diameter of Borehole (in)	6 3/8		Ground Surface Elevation (ft-msl)	4590.8				
Drill Rig Type	Pro Sonic	Drilling Company	Cascade		Groundwater Elevation (ft-msl)	4484.3				
Driller's Name	Ryan Miller	Sampler Type	6 inch diameter, 2.5 foot long sample bags		Measuring Point Elevation (ft-msl)	4590.3				
Description of Sample Location	On an elevated berm road between two coal-ash settling ponds, approximately 500 feet west of the northeast corner of the settling pond berm road.				Northing	586183.818		Easting		730230.477

Depth (ft-bgs)	SAMPLES				USCS Symbol	MATERIAL DESCRIPTION	Well Construction		
	Run Number	Recovery (%)	Core Length (inches)	Core Depth (ft bgs)					
61		93			SM	10 YR 6/3 pale brown silty sand, loose, moist - dry, very fine sand, ~20% silt and clay, some gravelly zones			
62			28"	62		10 YR 6/3 pale brown sandy silt, medium stiff - very stiff, dry, low plasticity, very fine sand, ~40% sand, some gravel			
63	6	87			ML				
64			26"	64.5					
65									
66		83							
67			25"	67					
68		100							
69			18"	68.5		10 RY 6/3 pale brown silty sand, loose, dry, slightly moist, fine sand, ~20% - 30% silt, hard while drilling			
70		93							
71			28"	71					
72	7	87							
73									
74			26"	73.5					
75		90			SM				
76			27"	76					
77		100				Same as above			
78			18"	77.5					
79	8	100							
80			30"	80					



Project Name: Laramie River Station Well Replacement  
 Client: Basin Electric  
 Project Number: 60727167

Boring ID: MW-53BR

Date(s) Drilled	April 17-19, 2024	Logged By	David Buhl	Checked By		Total Depth of Borehole (ft bgs)	120	Depth to Water (bgs)	106	
Drilling Method	Sonic	Diameter of Borehole (in)	6 3/8		Ground Surface Elevation (ft-msl)	4590.8				
Drill Rig Type	Pro Sonic	Drilling Company	Cascade		Groundwater Elevation (ft-msl)	4484.3				
Driller's Name	Ryan Miller	Sampler Type	6 inch diameter, 2.5 foot long sample bags		Measuring Point Elevation (ft-msl)	4590.3				
Description of Sample Location	On an elevated berm road between two coal-ash settling ponds, approximately 500 feet west of the northeast corner of the settling pond berm road.				Northing	586183.818		Easting		730230.477

Depth (ft-bgs)	SAMPLES				USCS Symbol	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Core Length (inches)	Core Depth (ft bgs)				
81		100						
82			24"	82				
83	9	100						
84			30"	84.5				
85								
86		93					Bentonite Grout	Bentonite Grout
87			28"	87		moist, otherwise same as above		
88		87						
89			26"	89.5				
90					SM			
91		87						
92	10		26"	92				
93		93						
94			28"	94.5				
95						Some gravel, otherwise same as above		
96		77						
97			23"	97				
98		100				becoming very moist - wet, otherwise same as above		
99	11		18"	98.5				
100		100					Filter Pack - Sand	Filter Pack - Sand
			30"	101				



Project Name: Laramie River Station Well Replacement  
 Client: Basin Electric  
 Project Number: 60727167

Boring ID: MW-53BR

Date(s) Drilled	April 17-19, 2024	Logged By	David Buhl	Checked By		Total Depth of Borehole (ft bgs)	120	Depth to Water (bgs)	106
Drilling Method	Sonic	Diameter of Borehole (in)	6 3/8			Ground Surface Elevation (ft-msl)	4590.8		
Drill Rig Type	Pro Sonic	Drilling Company	Cascade			Groundwater Elevation (ft-msl)	4484.3		
Driller's Name	Ryan Miller	Sampler Type	6 inch diameter, 2.5 foot long sample bags			Measuring Point Elevation (ft-msl)	4590.3		
Description of Sample Location	On an elevated berm road between two coal-ash settling ponds, approximately 500 feet west of the northeast corner of the settling pond berm road.					Northing	586183.818		
						Eastings	730230.477		

Depth (ft-bgs)	SAMPLES				USCS Symbol	MATERIAL DESCRIPTION	Well Construction
	Run Number	Recovery (%)	Core Length (inches)	Core Depth (ft bgs)			
101		100	30"	101		moist, otherwise same as above	
102		100					
103	11		30"	103.5			
104						some cobbles	
105		100					
106			30"	106		wet, same as above, probable water level	
107		100	12"	107			
108		100					
109			30"	109.5			
110					SM		
111		100					
112	12		30"	112			
113		100					
114			30"	114.5			
115						very fine - medium sand grains but larger grain size overall, otherwise same as above	
116		100					
117			30"	117			
118		0	0"	118		No Recovery	
119	13					very fine - fine sand grains but smaller grain size overall, otherwise same as above	
120		100	24"	120			





Project Name: Basin Electric Laramie River Station  
 Client: Basin Electric Laramie River Station  
 Project Number: 60577052

Boring ID: \_\_\_\_\_

Date(s) Drilled	02-Apr-19	Logged By	J. Hurshman	Checked By		Total Depth of Borehole (ft)	<b>25 ft</b>	Depth to Water (bgs)	
Drilling Method	Hollow Stem Auger	Diameter of Borehole (in)	8 1/4 inch OD			Ground Surface Elevation (ft-msl)	TBD		
Drill Rig Type	CME	Drilling Company	Inberg Miller			Groundwater Elevation (ft-msl)	TBD		
Driller's Name	Jose/Barry	Sampler Type	2 inch Acetate sleeve			Measuring Point Elevation (ft-msl)	TBD		
Description of Sample Location						Northing	TBD		
						Easting	TBD		

Depth (ft-bgs)	SAMPLES			USCS Symbol	Blow Counts	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Sample ID					
1				CL	2	0-0.5 ft: fill material 0.5-1 ft: dark brown top soil, silty sand with clay, rootlets, moist. 1-5 ft: clay with silt, brown, moist, slightly sticky at 2.5 ft, wet 2 to 2.5 ft, moderate plasticity, very soft, no gravel, no sand.		
2				CL	2			
3	1	40	N/A	CL	2			
4				CL	2			
5				CL	2			
6				SW	1	poor recovery		
7				SW	7	wet, coarse sand, subrounded, poorly sorted, sand is medium to fine at 7 ft for 6 inches then coarse sand with few gravels/pebbles, no silt/clay		
8	2	55	N/A	SW	9			
9				SW	7			
10				SW	16			
11				SW	17	no recovery 10-12.5 ft, water on acetate sleeve is micaceous	bentonite chips	
12				SW	20			
13	3	50	N/A	SW	22	12.5 ft: fine sand grading into medium and coarse sand, poorly sorted, brown, sand appears granitic, subrounded, saturated		
14				SW	26			
15				SW	29	few pebbles at 14.5 ft (1 inch diameters)		
16				SW	13	flowing sand 15-16 ft: coarse sand with 10% gravel, wet, poorly sorted, rounded to subrounded grains		
17				SW	33	16-17 ft: color change to reddish, fine silt matrix	10/20 silica sandpack	
18	4	100	N/A	SW	74	17-18 ft: light tan matrix, pebbles/sand mix, very poorly sorted, wet, rounded pebbles (1 inch diameter), fine to medium sand		
19				SW	86			
20				SW	96	no recovery 19-25 ft		0.01 silt screen



Project Name: Basin Electric Laramie River Station  
 Client: Basin Electric Laramie River Station  
 Project Number: 60577052

Boring ID: \_\_\_\_\_

Date(s) 02-Apr-19	Logged By J. Hurshman	Checked By	Total Depth of Borehole (ft)	25 ft	Depth to Water (bgs)
Drilled Method Hollow Stem Auger	Diameter of Borehole (in) 8 1/4 inch OD	Ground Surface Elevation (ft-msl) TBD	Groundwater Elevation (ft-msl) TBD	Measuring Point Elevation (ft-msl) TBD	Northing Easting TBD
Drill Rig Type CME	Drilling Company Inberg Miller	Sampler Type 2 inch acetate sleeve		Description of Sample Location	

Depth (ft-bgs)	SAMPLES			USCS Symbol	Blow Counts	MATERIAL DESCRIPTION	Well Construction		
	Run Number	Recovery (%)	Sample ID						
21					100	no recovery, refusal with 2 inch push probe			
22	5	0	N/A	SW				10/20 silica sandpack	
23									
24									
25						Total Depth = 25 feet			
26						Well completion: 0-14.5: schedule 40 riser 14.5-24.5 ft: schedule 40 0.01 slot screen 2-12.5 ft: medium bentonite chips 12.5-24.5 ft: 10/20 silica sandpack			
27						note: flowing sands present in borehole in middle section of bentonite chips, minimum of 1 ft bentonite on top of sandpack.			
28									
29									
30									
31									
32									
33									
34									
35									
36									
37									
38									
39									
40									



Project Name: Basin Electric Laramie River Station  
 Client: Basin Electric Laramie River Station  
 Project Number: 60577052

Boring ID: MW-55B

Date(s) Drilled	03-Apr-19	Logged By	J. Hurshman	Checked By		Total Depth of Borehole (ft)		Depth to Water (bgs)	
Drilling Method	Hollow Stem Auger	Diameter of Borehole (in)	8 1/4 inch OD			Ground Surface Elevation (ft-msl)	TBD		
Drill Rig Type	CME	Drilling Company	Inberg Miller			Groundwater Elevation (ft-msl)	TBD		
Driller's Name	Barry	Sampler Type	5 foot core barrel			Measuring Point Elevation (ft-msl)	TBD		
Description of Sample Location						Northing	TBD		
						Easting	TBD		

Depth (ft-bgs)	SAMPLES			USCS Symbol	PID (ppm)	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Blow Counts					
1			0		N/A	0-5 ft: silty fine sand, very soft from 0-3 ft, rootlets 0-0.5 ft, dark broan 0-4 ft, harder from 4-5 ft, increased sand content/less silt 4-5 ft, medium sand, light tan color, dry		
2	1	70	3					
3			8					
4			8	SM				
5			6			as above to 9 ft bgs.		
6			9					
7	2	75	9					
8			24					
9			38			9-10 ft: sandy gravel, dry poorly sorted, hard to drill, rounded gravels broken up by drill rig, sand is fine to medium		
10			23	GM		as above to 12.8 ft, sandy gravel with pebbles, broken by drilling, poorly sorted		grout
11			34					
12	3	100	88					
13			100/6"	SP		12.8 - 13.5 ft: fine sand, tight, well sorted, dry, light tan, refusal at 13.5 ft with acetate sleeve.		
14			0					
15			29			15-15.5 ft: fine sand with rounded gravel, poorly sorted, dry, light tan color		
16	4	100	100/11"			15.5-17 ft: fine sand, dry, well sorted, homogeneous, soft, refusal at 17 ft.		
17						overdrilled to 20 ft with solid stem auger, no recovery		
18			0					
19								
20								



Project Name: Basin Electric Laramie River Station  
 Client: Basin Electric Laramie River Station  
 Project Number: 60577052

Boring ID: MW-55B

Date(s) 03-Apr-19	Logged J. Hurshman	Checked By	Total Depth of Borehole (ft)	Depth to Water (bgs)
Drilled Hollow Stem Auger	By	Diameter of Borehole (in) 8 1/4 inch OD	Ground Surface Elevation (ft-msl) TBD	
Drill Rig Type CME	Drilling Company Inberg Miller		Groundwater Elevation (ft-msl) TBD	
Driller's Name Barry	Sampler Type 5 foot core barrel		Measuring Point Elevation (ft-msl) TBD	
Description of Sample Location			Northing Easting TBD	

Depth (ft-bgs)	SAMPLES			USCS Symbol	Graphic Log	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Sample ID					
21				SP	N/A	as above fine sand to 24 ft, well sorted, dry, homogeneous, light tan		
22	5	100						
23								
24		0		SS		hard layer at 24 ft, light tan to gray sandstone lens, fine grained, well sorted, homogeneous, blind drilled to 25 ft		
25						25-29 ft: fine sand, homogeneous, well sorted, hard packed, light tan, moist		grout
26				SP				
27	6	100				hard lens at 27 ft for 2 inches		
28								
29						hard light tan/gray fine grained sandstone lens		
30						blind drilled to 35 ft (solid tip) harder sand/sandstone material		
31				SS/SP				
32	7	0						
33								
34								
35								
36				SP		fine sand as above, tight, hard to 38 ft, softer 38-40 ft, light tan, dry to moist, well sorted, homogeneous		
37	8	100						
38								
39								
40								

schedule 80 riser



Project Name: **Basin Electric Laramie River Station**  
 Client: **Basin Electric Laramie River Station**  
 Project Number: **60577052**

Boring ID: **MW-55B**

Date(s) 03-Apr-19	Logged By J. Hurshman	Checked By	Total Depth of Borehole (ft)	Depth to Water (bgs)
Drilled Method Hollow Stem Auger	Diameter of Borehole (in) 8 1/4 inch OD		Ground Surface Elevation (ft-msl) TBD	
Drill Rig Type CME	Drilling Company Inberg Miller		Groundwater Elevation (ft-msl) TBD	
Driller's Name Barry	Sampler Type 5 foot core barrel		Measuring Point Elevation (ft-msl) TBD	
Description of Sample Location			Northing Easting	TBD

Depth (ft-bgs)	SAMPLES			USCS Symbol	Graphic Log	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Sample ID					
41			N/A	SP	N/A	as above, increasing moisture content, appears almost wet at 41 ft to 42 ft. hard 40-42 ft, then softer 42-45 ft medium to tan color	grout	
42	9	100						
43							hydrated bentonite seal	
44								
45						as above, darker tan to brown, increased moisture, hard packed, stiff few interbedded white burrow casts 1-2 mm in diameter		schedule 80 riser
46								
47	10	100						
48								
49								
50						as above, core is wet		
51							10/20 silica	
52								
53	11	100						
54								
55						as above, wet, softer from 55-56.5 ft, then hard packed, slightly cemented, few interbedded white burrow casts in sand near 58-59 ft		schedule 80 0.01 slot screen
56								
57								
58	12	100						
59								
60								



Project Name: Basin Electric Laramie River Station  
 Client: Basin Electric Laramie River Station  
 Project Number: 60577052

Boring ID: MW-55B

Date(s) 03-Apr-19	Logged By J. Hurshman	Checked By	Total Depth of Borehole (ft)	Depth to Water (bgs)
Drilled Method Hollow Stem Auger	Diameter of Borehole (in) 8 1/4 inch OD	Ground Surface Elevation (ft-msl) TBD	Groundwater Elevation (ft-msl) TBD	
Drill Rig Type CME	Drilling Company Inberg Miller	Measuring Point Elevation (ft-msl) TBD	Northing Easting TBD	
Driller's Name	Sampler Type 5 foot core barrel	Description of Sample Location		

Depth (ft-bgs)	SAMPLES			USCS Symbol	Graphic Log	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Sample ID					
61			N/A	SP	N/A	as above, wet, hard packed sand 60-62 ft, softer 62-65 ft - easy to drill, brown color, few interbedded white burrow casts		
62	13	100						
63								
64								
65						as above, wet, flowing fine sand to 67.5 ft white burrow casts 69-70 ft - interbedded	10/20 silica	schedule 80 0.01 slot screen
66								
67	14	100						
68								
69								
70						TD = 70 ft		
71						Well Completion: Schedule 80 0.01 slot screen 50-70 ft 10/20 silica sand pack from 47.2-70 ft hydrated bentonite seal 41.8 - 47.2 ft schedule 80 riser 0-50 ft no centralizers used		
72								
73								
74								
75								
76								
77								
78								
79								
80								



Project Name: Basin Electric Laramie River Station  
 Client: Basin Electric Laramie River Station  
 Project Number: 60577052

Boring ID: MW-56B

Date(s) Drilled	02-Apr-19	Logged By	J. Hurshman	Checked By		Total Depth of Borehole (ft)		Depth to Water (bgs)	
Drilling Method	Hollow Stem Auger	Diameter of Borehole (in)	8 1/4 inch OD			Ground Surface Elevation (ft-msl)	TBD		
Drill Rig Type	CME	Drilling Company	Inberg Miller			Groundwater Elevation (ft-msl)	TBD		
Driller's Name	Barry	Sampler Type	5 foot core barrel			Measuring Point Elevation (ft-msl)	TBD		
Description of Sample Location						Northing	TBD		
						Easting	TBD		

Depth (ft-bgs)	SAMPLES			USCS Symbol	PID (ppm)	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Blow Counts					
1			3		N/A	silty fine sand, well sorted, dark brown 0-2 ft bgs, rootlets 0-1 ft, medium brown 2-5 ft, no gravel, no clay omogeneous in appearance, moist, soft, crumbles easily		
2	1	90	4	SM				
3			4					
4			3					
5			2			as above to 10 ft		
6			4					
7	2	90	5					
8			4					
9			4					
10			19			as above to 11 ft - softer, little recovery		grout
11			76			gravelly sand with pebbles/cobbles, dry, hard, broken pices of rock/non sandstonein core, light tan to mottled colors depending on rock/cobble type, poorly sorted		schedule 80 riser
12	3	70	94	GW				
13			100/10"					
14								
15						14.5 ft: light tan, fine sand, well sorted, homogeneous, softer		
16						15-20 ft: light tan sand, very hard, lightly cemented/hard packed, slight moisture, well sorted, fine grained, homogeneous, suboumded to rounded grains		
17	4	100		SP				
18								
19								
20						hard sandstone lans at 20 ft.		



Project Name: **Basin Electric Laramie River Station**  
 Client: **Basin Electric Laramie River Station**  
 Project Number: **60577052**

Boring ID: **MW-56B**

Date(s) 02-Apr-19	Logged By J. Hurshman	Checked By	Total Depth of Borehole (ft)	Depth to Water (bgs)
Drilled Method Hollow Stem Auger	Diameter of Borehole (in) 8 1/4 inch OD		Ground Surface Elevation (ft-msl) TBD	
Drill Rig Type CME	Drilling Company Inberg Miller		Groundwater Elevation (ft-msl) TBD	
Driller's Name Barry/Jose	Sampler Type 5 foot core barrel		Measuring Point Elevation (ft-msl) TBD	
Description of Sample Location			Northing Easting	TBD

Depth (ft-bgs)	SAMPLES			USCS Symbol	Graphic Log	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Sample ID					
21			N/A	SP	N/A	sandstone lens to 21 ft (solid tipon augers)		
22	5	100				21-25 ft: light tan very fine sand, homogeneous, well sorted, moist, no clay, no larger sand, soft but tightly packed		
23								
24								
25						as above		
26								
27	6	50				hard sandstone lens from 27-28 ft		
28						as above fine sand, 1 cm thick sandstone lens at 28.7 ft, soft sand below		
29								
30							grout	
31						as above, hard packed fine sand, light tan, moist, sandstone lenses at 30.2-30.4 ft, and 30.9 to 31 ft		
32								
33	7	100						schedule 80 riser
34								
35						as above, hard packed fine to very fine sand, medium brown, very poor to no cementation, hard, moist.		
36								
37								
38	8	100						
39								
40								





Project Name: **Basin Electric Laramie River Station**  
 Client: **Basin Electric Laramie River Station**  
 Project Number: **60577052**

Boring ID: **MW-56B**

Date(s) 02-Apr-19	Logged By J. Hurshman	Checked By	Total Depth of Borehole (ft)	Depth to Water (bgs)
Drilled Method Hollow Stem Auger	Diameter of Borehole (in) 8 1/4 inch OD		Ground Surface Elevation (ft-msl) TBD	
Drill Rig Type CME	Drilling Company Inberg Miller		Groundwater Elevation (ft-msl) TBD	
Driller's Name Barry/Jose	Sampler Type 5 foot core barrel		Measuring Point Elevation (ft-msl) TBD	
Description of Sample Location			Northing Easting	TBD

Depth (ft-bgs)	SAMPLES			USCS Symbol	Graphic Log	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Sample ID					
41			N/A	SP	N/A	as above, hard packed		
42	9	100				slightly darker brown 42-43 ft		
43								
44						soft sand 44-45 ft		
45						as above, hard packed 45-47.5 ft, softer 47.5-50 ft minor white streaks at 46 and 48 ft < 1 inch thick		
46								
47								
48	10	100						
49							grout	
50						as above to 54.5 ft		
51								
52								
53	11	100						
54								
55				SS		almost platy texture with depth	bentonite seal	
56				SP		54.5 ft: hard sandstone, light gray, fine grained, well sorted, well cemented, homogeneous solid stem to drill through sandstone, wet beneath		
57						55-60 ft: well sorted, hard packed sandstone, wet at 55 ft, appears wet below but very tightly packed, medium tan in color		schedule 80 riser
58	12	100					10/20 silica	
59								
60						Note: SS = sandstone		



Project Name: Basin Electric Laramie River Station  
 Client: Basin Electric Laramie River Station  
 Project Number: 60577052

Boring ID: MW-56B

Date(s) 02-Apr-19	Logged By J. Hurshman	Checked By	Total Depth of Borehole (ft)	Depth to Water (bgs)
Drilled Method Hollow Stem Auger	Diameter of Borehole (in) 8 1/4 inch OD		Ground Surface Elevation (ft-msl) TBD	
Drill Rig Type CME	Drilling Company Inberg Miller		Groundwater Elevation (ft-msl) TBD	
Driller's Name Barry	Sampler Type 5 foot core barrel		Measuring Point Elevation (ft-msl) TBD	
Description of Sample Location			Northing Easting TBD	

Depth (ft-bgs)	SAMPLES			USCS Symbol	Graphic Log	MATERIAL DESCRIPTION	Well Construction	
	Run Number	Recovery (%)	Sample ID					
61			N/A	SP	N/A	sand as above, saturated, hard packed,		
62	13	100						
63						dark brown color change at 63.5 ft for 3 inches, softer than above 63.5-65 ft, slightly mottled light tan to dark brown color in this zone,		
64						trace red granite gravel in bottom of core		
65						65-70 ft: as above, medium tan sand, fine grained, wet, well sorted		
66								
67	14	100						
68								
69								
70						as above to 72 ft		
71								
72						72-74 ft: fine sand with interbedded chips of brown/reddish almost chert, angular framents, poorly sorted		
73	15	100					10/20 silica	
74						74-75 ft: fine sand as above, wet, hard packed		
75						75-79 ft: fine grained hard packed sand, very poorly to no cementation, well sorted, tan to light brown, interbedded white burrow casts mainly 76.5 to 77.5 ft		
76								
77	16	100						
78								
79						TD = 79 ft		
80						Well completion: schedule 80 0.01 slot screen 59-79 ft, schedule 80 riser 0-59 ft, 10/20 silica sandpack 57-79 ft, bentonite seal 52-57 ft, grout 0-52 ft		

## **Appendix B**

# **Aquifer Test Procedures, Data and Analysis**

PUMPING TEST DATA FORM (Slug Test)

Well ID MW-33B Personnel Harshman  
 Location Buism Electric LPS Static Water Level ~~66.8~~ 69.88  
 Type of Well Monitoring well Extraction Well Distance —  
 Test Date 8/22/16 Total Casing Depth 86.90  
 Measuring Point Elevation TOC - TSD Borehole Diameter 6 inch  
 Type of Test Slug Test Casing Diameter 2 inch  
 Step Number — Screened Interval —  
 Data logger Test Run No. 1 Sand Pack Interval —  
 Pumping Rate — Lithology Tested —  
 Test Start Time — Test End Time —

Slug = 644 x 1 inch

Time	Elapsed Time (min)	Water Depth (ft)	Time	Elapsed Time (min)	Water Depth (ft)
1321	Ø	69.88			
1322	Start Test	NM			
1323	slug in	NM			
1325	4 min	69.77			
1336	15 min	69.88			
1337	16 min	Slug out			
1339	18 min	70.09			
1345	24 min	69.91			
1349	28 min	69.90			
1356	35 min	69.89			
1358	37 min	Stopped test			

See transducer data for details on Test.

### PUMPING TEST DATA FORM (slug Test)

Well ID	<u>MW-35B</u>	Personnel	<u>Hurshman</u>
Location	<u>Basin Electric LPS</u>	Static Water Level	<u>66.43</u>
Type of Well	<u>Monitoring well</u>	Extraction Well Distance	<u>—</u>
Test Date	<u>8/22/16</u>	Total Casing Depth	<u>88.31</u>
Measuring Point Elevation	<u>TOC - TRD</u>	Borehole Diameter	<u>6 inch</u>
Type of Test	<u>Slug Test</u>	Casing Diameter	<u>2 inch</u>
Step Number	<u>NA</u>	Screened Interval	<u>—</u>
Data logger Test Run No.	<u>1</u>	Sand Pack Interval	<u>—</u>
Pumping Rate	<u>—</u>	Lithology Tested	<u>—</u>
Test Start Time	<u>1055</u>	Test End Time	<u>1126</u>

slug = 6 ft x 1 inch

Time	Elapsed Time (min)	Water Depth (ft)	Time	Elapsed Time (min)	Water Depth (ft)
1054	∅	66.42			
1055	Start slug Test	NM			
1102	7 min	66.41			
1111	16 min	66.42			
1112	17 min	removed slug			
1114	19 min	66.59			
1122	27 min	66.43			
1124	29 min	66.43			
1126	31 min	stopped Test.			

see transducer data for details

### PUMPING TEST DATA FORM

Well ID MW-37B Personnel H. Shuman  
 Location Basin Electric LPS Static Water Level 62.32  
 Type of Well Monitoring Well Extraction Well Distance —  
 Test Date 8/19/16 Total Casing Depth 78.53  
 Measuring Point Elevation TOC - TBD Borehole Diameter 6 inch  
 Type of Test Slug Test Casing Diameter 2 inch  
 Step Number — Screened Interval —  
 Data logger Test Run No. 1 Sand Pack Interval —  
 Pumping Rate NA (slug) Lithology Tested —  
 Test Start Time 1118 Test End Time 1143

Slug = 6 qt x 1 inch

Time	Elapsed Time (min)	Water Depth (ft)	Time	Elapsed Time (min)	Water Depth (ft)
1117	0	62.36			
1118	Start slug Test	—			
1127	5 min	62.35			
1128	10 min	62.36			
1129	Slug out	NM			
1139	21 min	62.37			
1141	23 min	62.37			
1143	Stopped slug Test				

see transducer data for details.

### PUMPING TEST DATA FORM (slug Test)

Well ID	MW-388	Personnel	Hershman
Location	Basin Electric LPS	Static Water Level	60.08
Type of Well	Monitoring Well	Extraction Well Distance	—
Test Date	8/22/16	Total Casing Depth	77.75
Measuring Point Elevation	TDC - TBD	Borehole Diameter	6 inch
Type of Test	Slug Test	Casing Diameter	2 inch
Step Number	—	Screened Interval	—
Data logger Test Run No.	1	Sand Pack Interval	—
Pumping Rate	—	Lithology Tested	—
Test Start Time	—	Test End Time	—

slug = 6.4 x 1 inch.

Time	Elapsed Time (min)	Water Depth (ft)	Time	Elapsed Time (min)	Water Depth (ft)
1637	0	60.08			
1638	1 min	slug in well			
1639	2 min	59.76			
1644	7 min	59.97			
1651	14 min	60.05			
1653	16 min	60.07			
1659	22 min	60.07			-transducer may have bumped slightly
1700	23 min	slug out			
1703	26 min	60.40			
1706	29 min	60.23			
1709	32 min	60.15			
1712	35 min	60.12			
1715	38 min	60.11			
1719	42 min	60.10			
1722	45 min	60.09			
1723	46 min	Stopped Test.			

see Transducer for details.

### PUMPING TEST DATA FORM (slug Test)

Well ID	<u>MW - 39B</u>	Personnel	<u>Hurdman, Alzredt</u>
Location	<u>Basin Electric LRS</u>	Static Water Level	<u>81.69</u>
Type of Well	<u>Monitoring Well</u>	Extraction Well Distance	<u>—</u>
Test Date	<u>8/23/16</u>	Total Casing Depth	<u>110.71</u>
Measuring Point Elevation	<u>TDC - TRD</u>	Borehole Diameter	<u>6 inch</u>
Type of Test	<u>Slug Test</u>	Casing Diameter	<u>2 inch</u>
Step Number	<u>—</u>	Screened Interval	<u>—</u>
Data logger Test Run No.	<u>1</u>	Sand Pack Interval	<u>—</u>
Pumping Rate	<u>—</u>	Lithology Tested	<u>—</u>
Test Start Time	<u>slug - 6 ft x 1 inch</u>		

Time	Elapsed Time (min)	Water Depth (ft)	Time	Elapsed Time (min)	Water Depth (ft)
0737	0	81.69			
0738	1 min	Start Test slug in			
0739	2 min	80.78			
0743	6 min	81.54			
0747	10 min	81.67			
0751	14 min	81.69			
0752	15 min	slug out			
0754	17 min	82.42			
0758	21 min	81.75			
0802	25 min	81.72			
0804	27 min	81.71			
0813	36 min	81.71			
0815	56 min	Stopped Test.			

See transducer data for details.



### PUMPING TEST DATA FORM (slug test)

Well ID	<u>MW-42B</u>	Personnel	<u>Hershman</u>
Location	<u>Basin Electric LRS</u>	Static Water Level	<u>46.37</u>
Type of Well	<u>Monitoring Well</u>	Extraction Well Distance	<u>—</u>
Test Date	<u>8/12/16</u>	Total Casing Depth	<u>70.07</u>
Measuring Point Elevation	<u>TDC - TSD</u>	Borehole Diameter	<u>6 inch</u>
Type of Test	<u>slug test</u>	Casing Diameter	<u>2 inch</u>
Step Number	<u>—</u>	Screened Interval	<u>—</u>
Data logger Test Run No.	<u>1</u>	Sand Pack Interval	<u>—</u>
Pumping Rate	<u>—</u>	Lithology Tested	<u>—</u>
Test Start Time	<u>0844</u>	Test End Time	<u>0907</u>

slug = 6 lt x 1 mch

Time	Elapsed Time (min)	Water Depth (ft)	Time	Elapsed Time (min)	Water Depth (ft)
0843	∅	46.36			
0844	start test, slug in well.				
0852	9 min	46.35			
0856	13 min	46.36			
0857	slug out	NM			
0859	16 min	46.56			
0904	21 min	46.36			
0907	Stop test	NM			

see transducer data for details

### PUMPING TEST DATA FORM (Slug Test)

Well ID	<u>MW-45B</u>	Personnel	<u>Hurshman</u>
Location	<u>Busin Electric LPS</u>	Static Water Level	<u>76.59</u>
Type of Well	<u>Monitoring Well</u>	Extraction Well Distance	<u>—</u>
Test Date	<u>8/16/16</u>	Total Casing Depth	<u>91.18</u>
Measuring Point Elevation	<u>TDC</u>	Borehole Diameter	<u>6 inch</u>
Type of Test	<u>Slug test</u>	Casing Diameter	<u>2 inch</u>
Step Number	<u>—</u>	Screened Interval	<u>—</u>
Data logger Test Run No.	<u>slug test 1</u>	Sand Pack Interval	<u>—</u>
Pumping Rate	<u>NA</u>	Lithology Tested	<u>—</u>
Test Start Time	<u>13:43</u>	Test End Time	<u>—</u>

slug dimensions: 6 ft x 1 inch diameter.

	Time	Elapsed Time (min)	Water Depth (ft)		Time	Elapsed Time (min)	Water Depth (ft)
Slug test 1  Note: Slug may not have been fully submerged.	1343	0	76.59				
	1345	slug in	—				
	1348	5	76.55				
	1352	slug out					
	1356	13	76.63				
	1401	18	76.63				
	1402	stop test					

Slug Test 2	1405	0	76.62
	1406	start test	NM
	1408	slug in	NM
	1418	13	76.57
	1423	18	76.60
	1425	slug out	NM
	1432	27	76.69
	1435	30	76.65
	1438	33	76.64
	1439	stopped Test	

see transducer data for details.

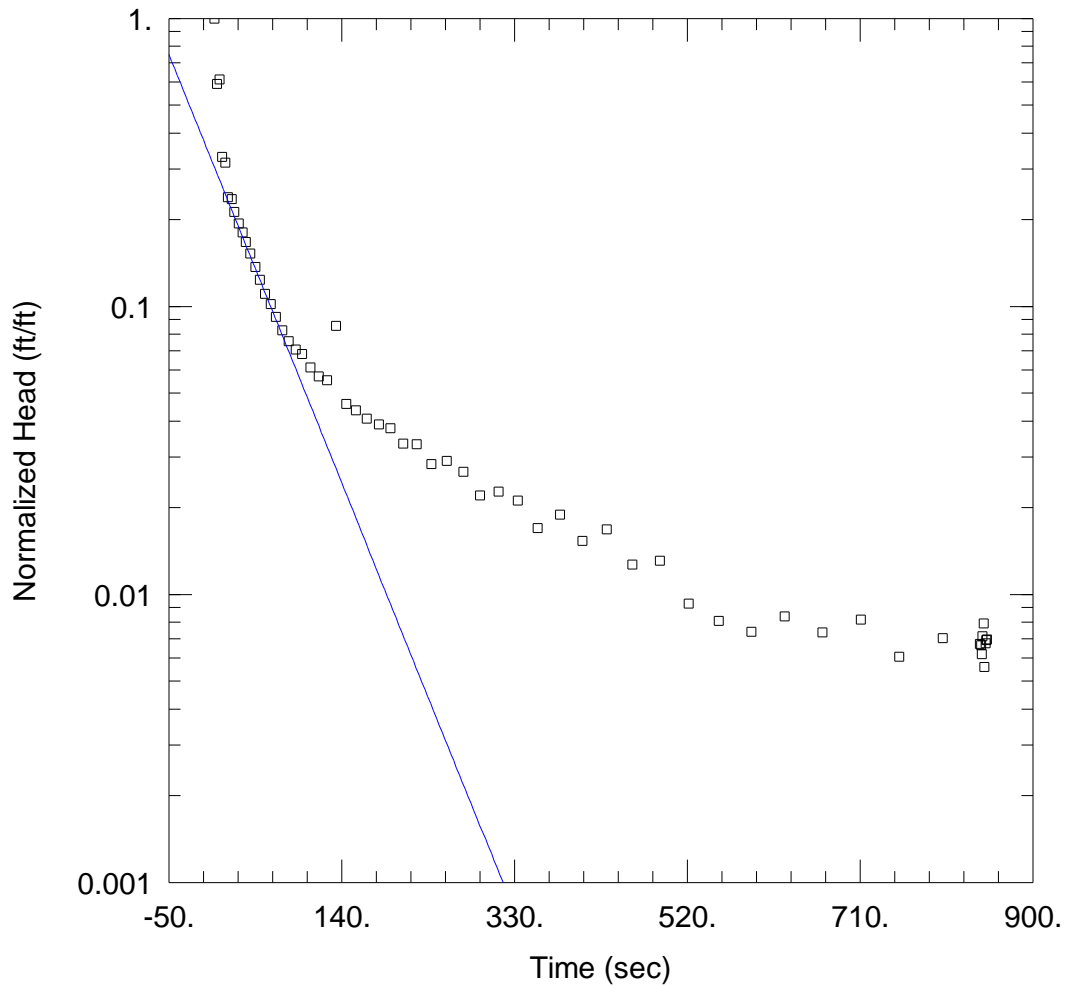
### PUMPING TEST DATA FORM (slug Test)

Well ID	<u>MW-43B</u>	Personnel	<u>Harshman</u>
Location	<u>Basin Electric L&amp;E</u>	Static Water Level	<u>75.86 btoe</u>
Type of Well	<u>Monitoring well</u>	Extraction Well Distance	<u>—</u>
Test Date	<u>8/18/10</u>	Total Casing Depth	<u>90.76 btoe</u>
Measuring Point Elevation	<u>TOC</u>	Borehole Diameter	<u>6 inch</u>
Type of Test	<u>—</u>	Casing Diameter	<u>2 inch</u>
Step Number	<u>—</u>	Screened Interval	<u>—</u>
Data logger Test Run No.	<u>1</u>	Sand Pack Interval	<u>—</u>
Pumping Rate	<u>NA (slug)</u>	Lithology Tested	<u>—</u>
Test Start Time	<u>1525</u>	Test End Time	<u>1610</u>

Test 1

Time	Elapsed Time (min)	Water Depth (ft)	Time	Elapsed Time (min)	Water Depth (ft)
1524	0	75.86			
1525	test started	NM			
1526	slug in	NM			
1533	9 min	75.73			
1538	14 min	75.81			
1546	22 min	75.84			
1549	25 min	75.85			
1551	slug out	NM			
1555	31 min	76.05			
1600	36 min	75.92			
1604	40 min	75.89			
1609	45 min	75.89			
1610	stop test	NM			

see transducer data for details



WELL TEST ANALYSIS

Data Set: C:\...\MW-33B\_Slug\_in.aqt  
 Date: 09/21/16

Time: 13:27:20

PROJECT INFORMATION

Company: AECOM  
 Client: Basin Electric  
 Project: 60506860  
 Test Well: 33B  
 Test Date: 8/22/16

AQUIFER DATA

Saturated Thickness: 16.36 ft

Anisotropy Ratio ( $K_z/K_r$ ): 1.

WELL DATA (33B)

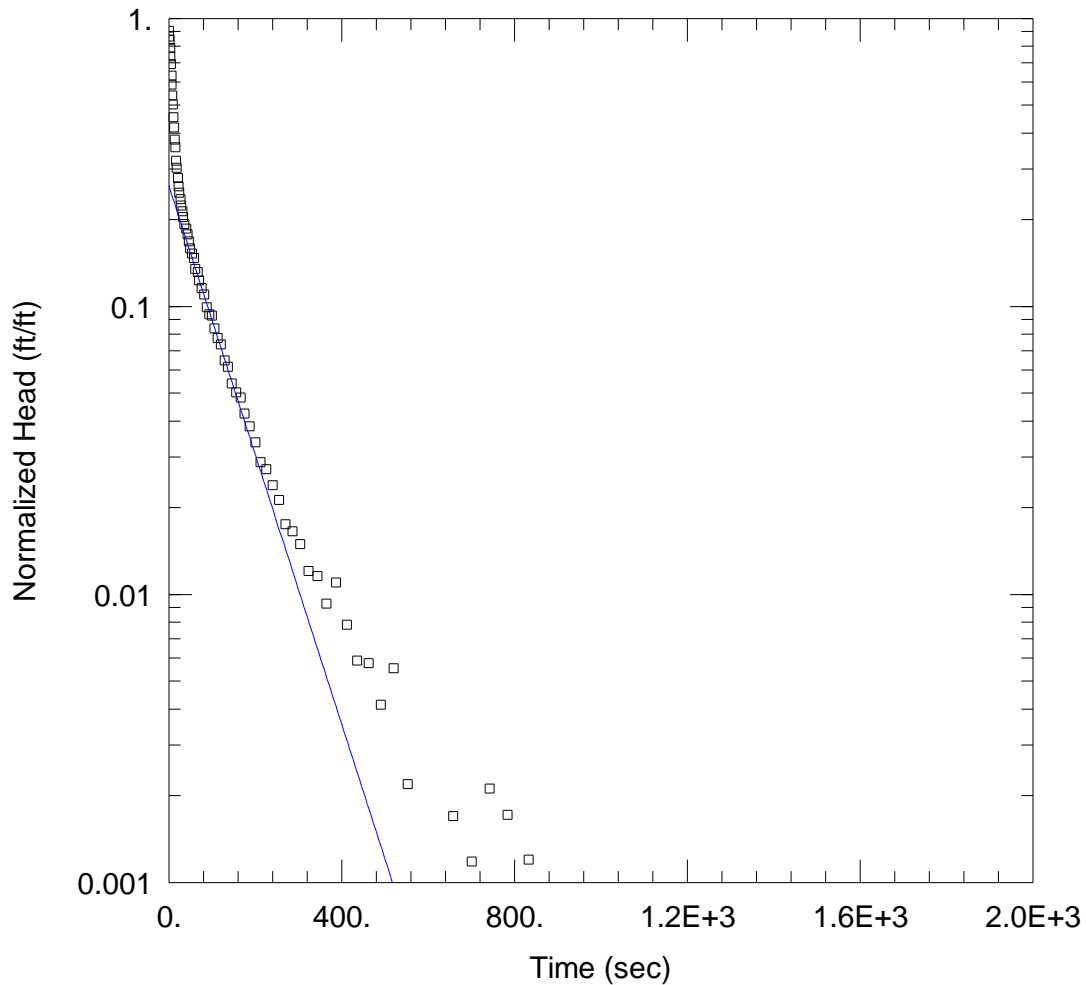
Initial Displacement: 2.428 ft  
 Total Well Penetration Depth: 20. ft  
 Casing Radius: 0.08612 ft

Static Water Column Height: 16.36 ft  
 Screen Length: 20. ft  
 Well Radius: 0.25 ft  
 Gravel Pack Porosity: 0.3

SOLUTION

Aquifer Model: Unconfined  
 K = 3.801 ft/day

Solution Method: Bouwer-Rice  
 $y_0$  = 0.7403 ft



### WELL TEST ANALYSIS

Data Set: C:\...\MW-33B\_Slug\_out.aqt

Date: 09/15/16

Time: 18:00:51

### PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 33B

Test Date: 8/22/16

### AQUIFER DATA

Saturated Thickness: 16.36 ft

Anisotropy Ratio ( $K_z/K_r$ ): 1.

### WELL DATA (33B)

Initial Displacement: -2.428 ft

Total Well Penetration Depth: 20. ft

Casing Radius: 0.08612 ft

Static Water Column Height: 16.36 ft

Screen Length: 20. ft

Well Radius: 0.25 ft

Gravel Pack Porosity: 0.3

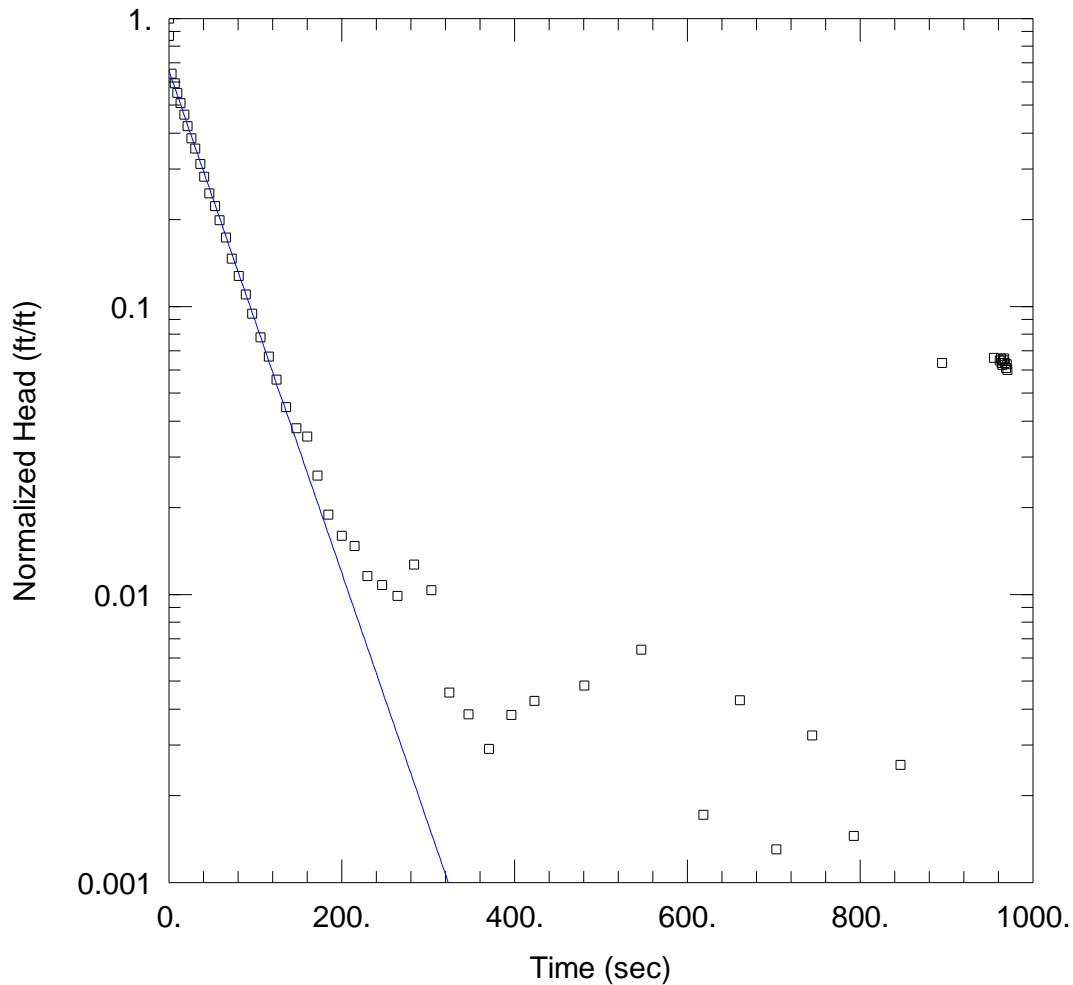
### SOLUTION

Aquifer Model: Unconfined

$K = 2.268$  ft/day

Solution Method: Bouwer-Rice

$y_0 = -0.6358$  ft



WELL TEST ANALYSIS

Data Set: C:\...\MW-35B\_Slug\_in.aqt  
 Date: 09/15/16

Time: 18:01:23

PROJECT INFORMATION

Company: AECOM  
 Client: Basin Electric  
 Project: 60506860  
 Test Well: 35B  
 Test Date: 8/22/16

AQUIFER DATA

Saturated Thickness: 19.96 ft

Anisotropy Ratio ( $K_z/K_r$ ): 1.

WELL DATA (35B)

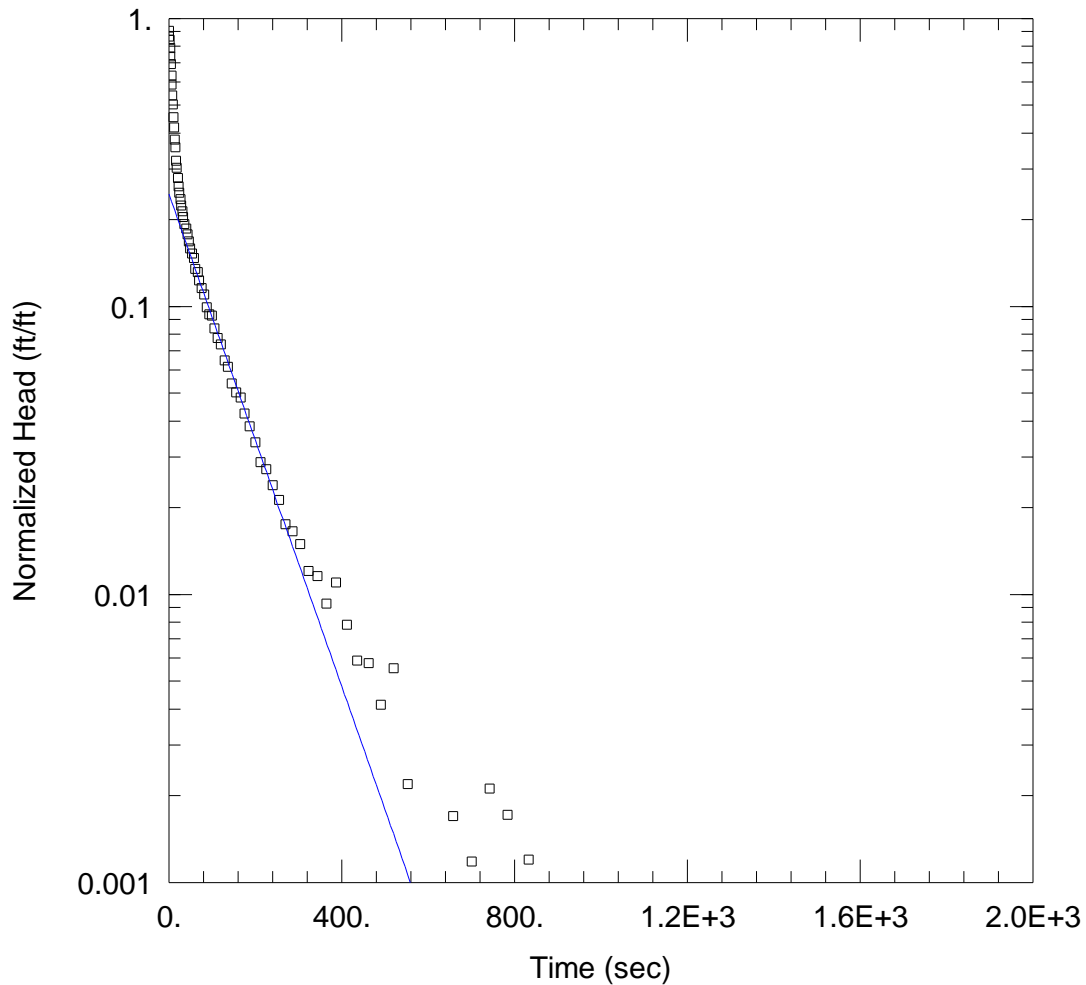
Initial Displacement: 2.428 ft  
 Total Well Penetration Depth: 20. ft  
 Casing Radius: 0.08612 ft

Static Water Column Height: 19.96 ft  
 Screen Length: 20. ft  
 Well Radius: 0.25 ft  
 Gravel Pack Porosity: 0.3

SOLUTION

Aquifer Model: Unconfined  
 K = 3.502 ft/day

Solution Method: Bouwer-Rice  
 $y_0$  = 1.6 ft



### WELL TEST ANALYSIS

Data Set: C:\...\MW-35B\_Slug\_out.aqt

Date: 09/15/16

Time: 18:01:50

### PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 35B

Test Date: 8/22/16

### AQUIFER DATA

Saturated Thickness: 19.96 ft

Anisotropy Ratio ( $K_z/K_r$ ): 1.

### WELL DATA (35B)

Initial Displacement: -2.428 ft

Total Well Penetration Depth: 20. ft

Casing Radius: 0.08612 ft

Static Water Column Height: 19.96 ft

Screen Length: 20. ft

Well Radius: 0.25 ft

Gravel Pack Porosity: 0.3

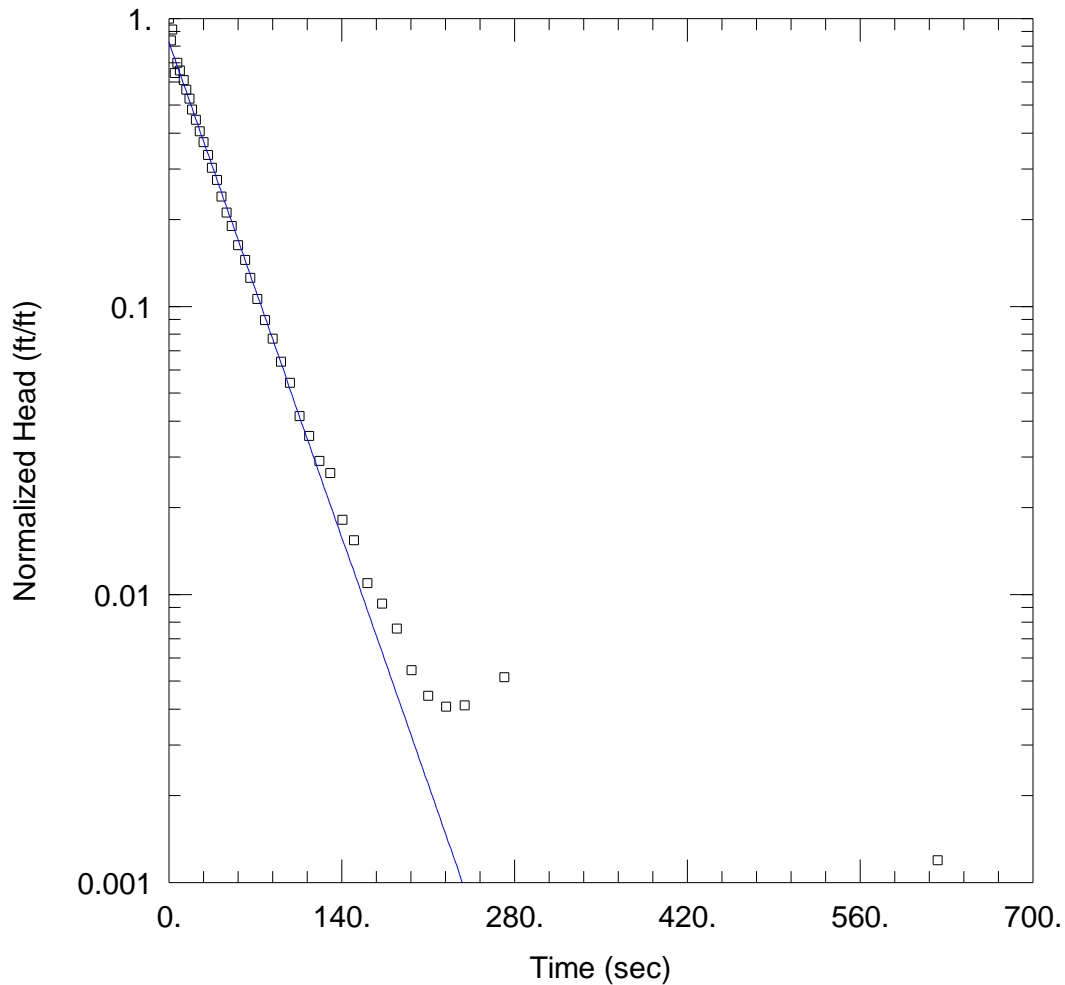
### SOLUTION

Aquifer Model: Unconfined

$K = 1.717$  ft/day

Solution Method: Bouwer-Rice

$y_0 = -0.5973$  ft



WELL TEST ANALYSIS

Data Set: C:\...\MW-37B\_Slug\_in.aqt  
 Date: 09/21/16

Time: 13:36:01

PROJECT INFORMATION

Company: AECOM  
 Client: Basin Electric  
 Project: 60506860  
 Test Well: 37B  
 Test Date: 8/19/16

AQUIFER DATA

Saturated Thickness: 16.14 ft

Anisotropy Ratio ( $K_z/K_r$ ): 1.

WELL DATA (37B)

Initial Displacement: 2.428 ft  
 Total Well Penetration Depth: 20. ft  
 Casing Radius: 0.08612 ft

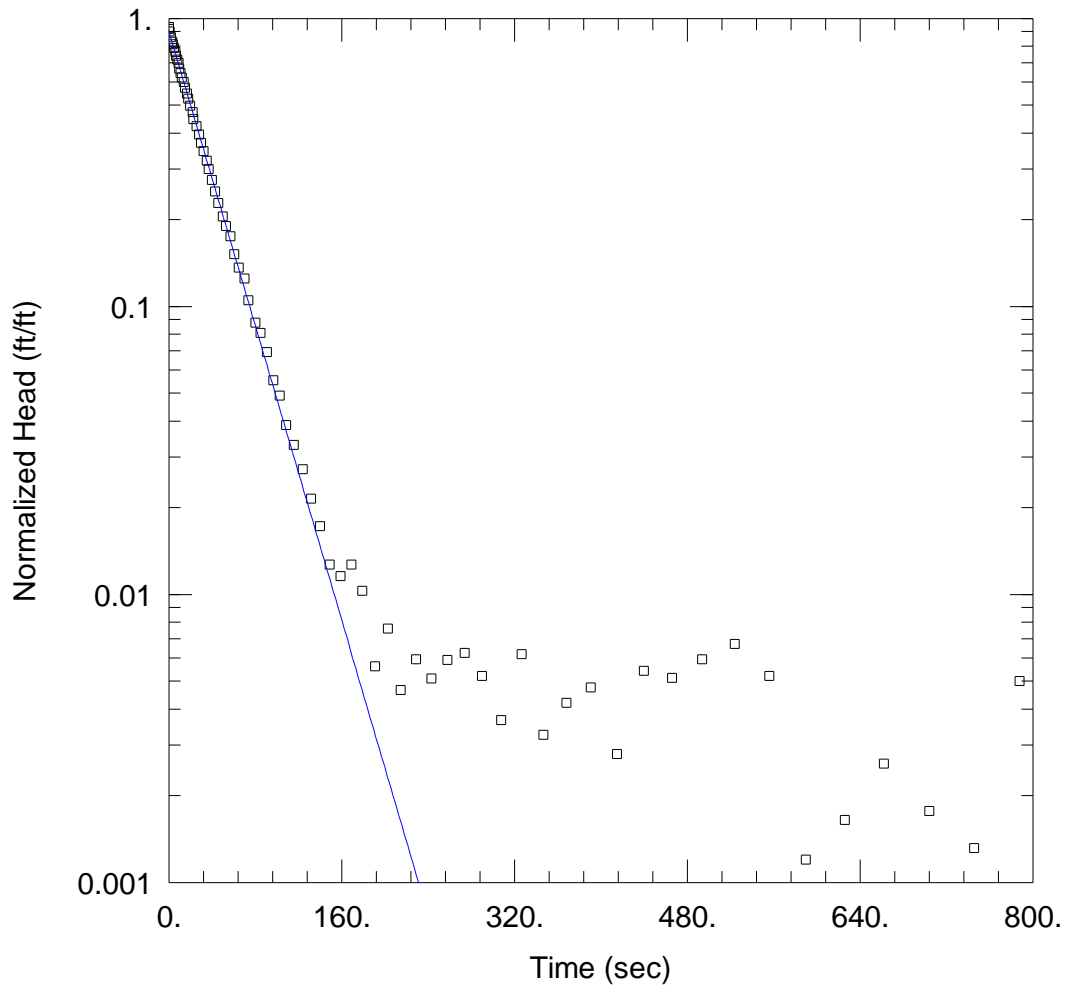
Static Water Column Height: 16.14 ft  
 Screen Length: 20. ft  
 Well Radius: 0.25 ft  
 Gravel Pack Porosity: 0.3

SOLUTION

Aquifer Model: Unconfined  
 K = 6.039 ft/day

Solution Method: Bouwer-Rice  
 $y_0$  = 2.014 ft





WELL TEST ANALYSIS

Data Set: C:\...\MW-37B\_Slug\_out.aqt

Date: 09/21/16

Time: 13:37:13

PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 37B

Test Date: 8/19/16

AQUIFER DATA

Saturated Thickness: 16.14 ft

Anisotropy Ratio ( $K_z/K_r$ ): 1.

WELL DATA (37B)

Initial Displacement: -2.428 ft

Total Well Penetration Depth: 20. ft

Casing Radius: 0.08612 ft

Static Water Column Height: 16.14 ft

Screen Length: 20. ft

Well Radius: 0.25 ft

Gravel Pack Porosity: 0.3

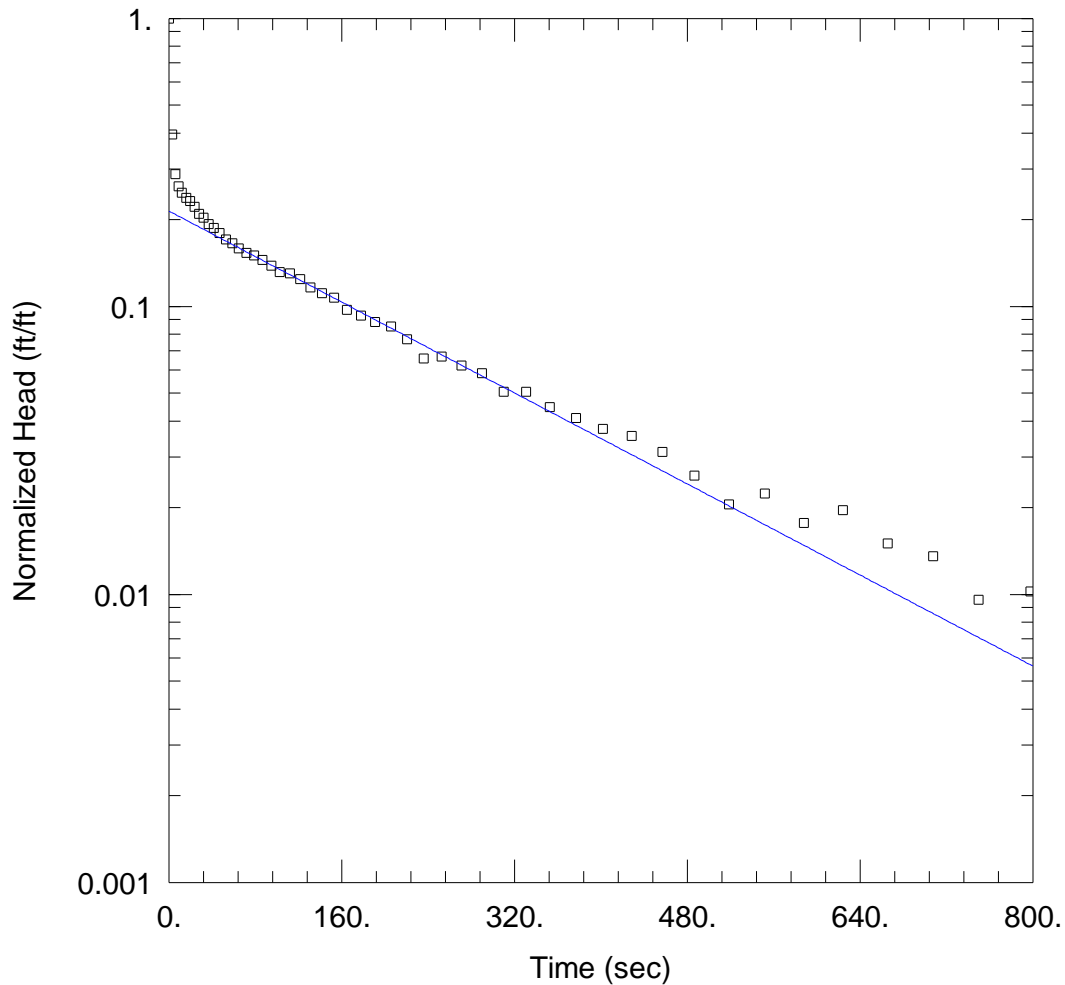
SOLUTION

Aquifer Model: Unconfined

$K = 6.284$  ft/day

Solution Method: Bouwer-Rice

$y_0 = -2.192$  ft



WELL TEST ANALYSIS

Data Set: C:\...\MW-38B\_Slug\_in.aqt  
 Date: 09/15/16

Time: 17:10:28

PROJECT INFORMATION

Company: AECOM  
 Client: Basin Electric  
 Project: 60506860  
 Test Well: 38B  
 Test Date: 8/22/16

AQUIFER DATA

Saturated Thickness: 15.83 ft

Anisotropy Ratio ( $K_z/K_r$ ): 1.

WELL DATA (38B)

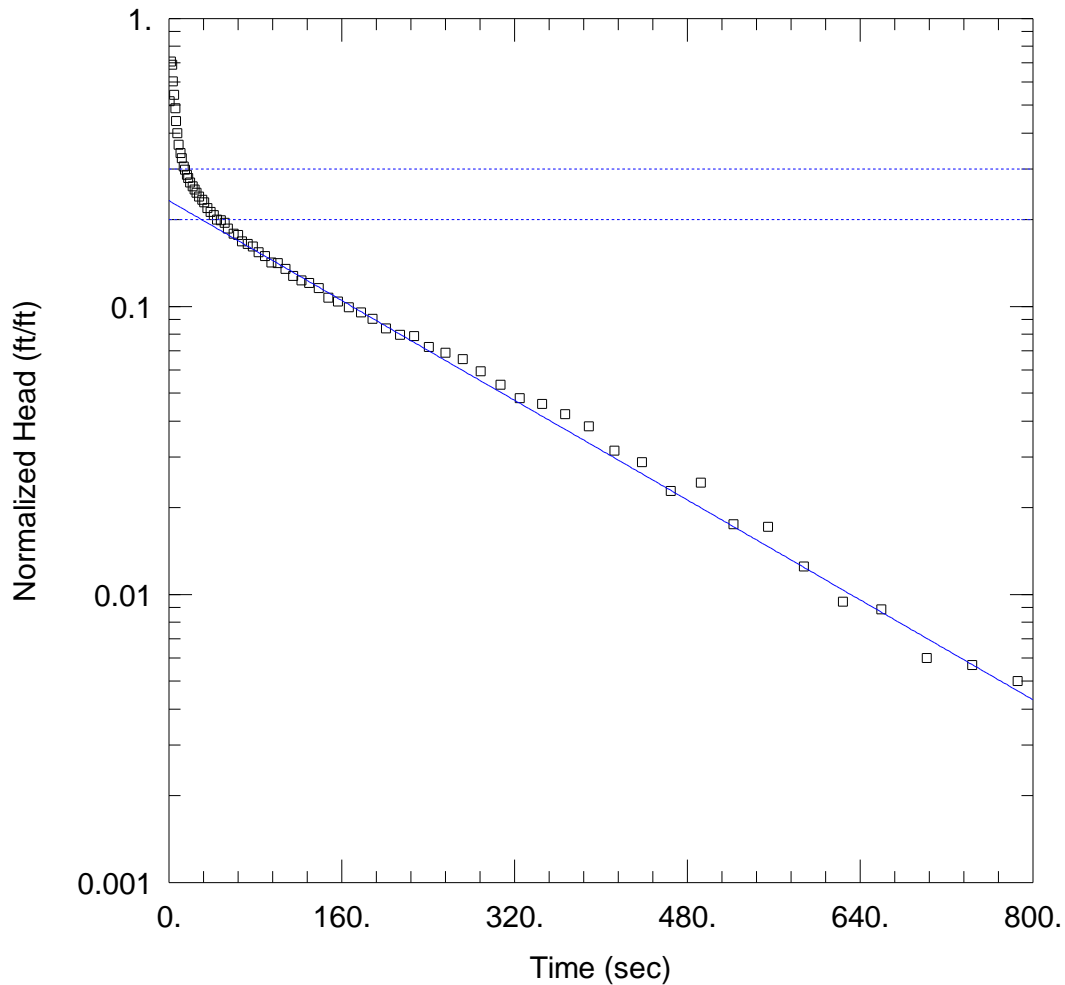
Initial Displacement: 2.428 ft  
 Total Well Penetration Depth: 20. ft  
 Casing Radius: 0.08612 ft

Static Water Column Height: 15.83 ft  
 Screen Length: 20. ft  
 Well Radius: 0.25 ft  
 Gravel Pack Porosity: 0.3

SOLUTION

Aquifer Model: Unconfined  
 K = 0.99 ft/day

Solution Method: Bouwer-Rice  
 $y_0$  = 0.5201 ft



WELL TEST ANALYSIS

Data Set: C:\...\MW-38B\_Slug\_out.aqt

Date: 09/15/16

Time: 17:09:06

PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 38B

Test Date: 8/22/16

AQUIFER DATA

Saturated Thickness: 15.83 ft

Anisotropy Ratio ( $K_z/K_r$ ): 1.

WELL DATA (38B)

Initial Displacement: -2.428 ft

Static Water Column Height: 15.83 ft

Total Well Penetration Depth: 20. ft

Screen Length: 20. ft

Casing Radius: 0.08612 ft

Well Radius: 0.25 ft

Gravel Pack Porosity: 0.3

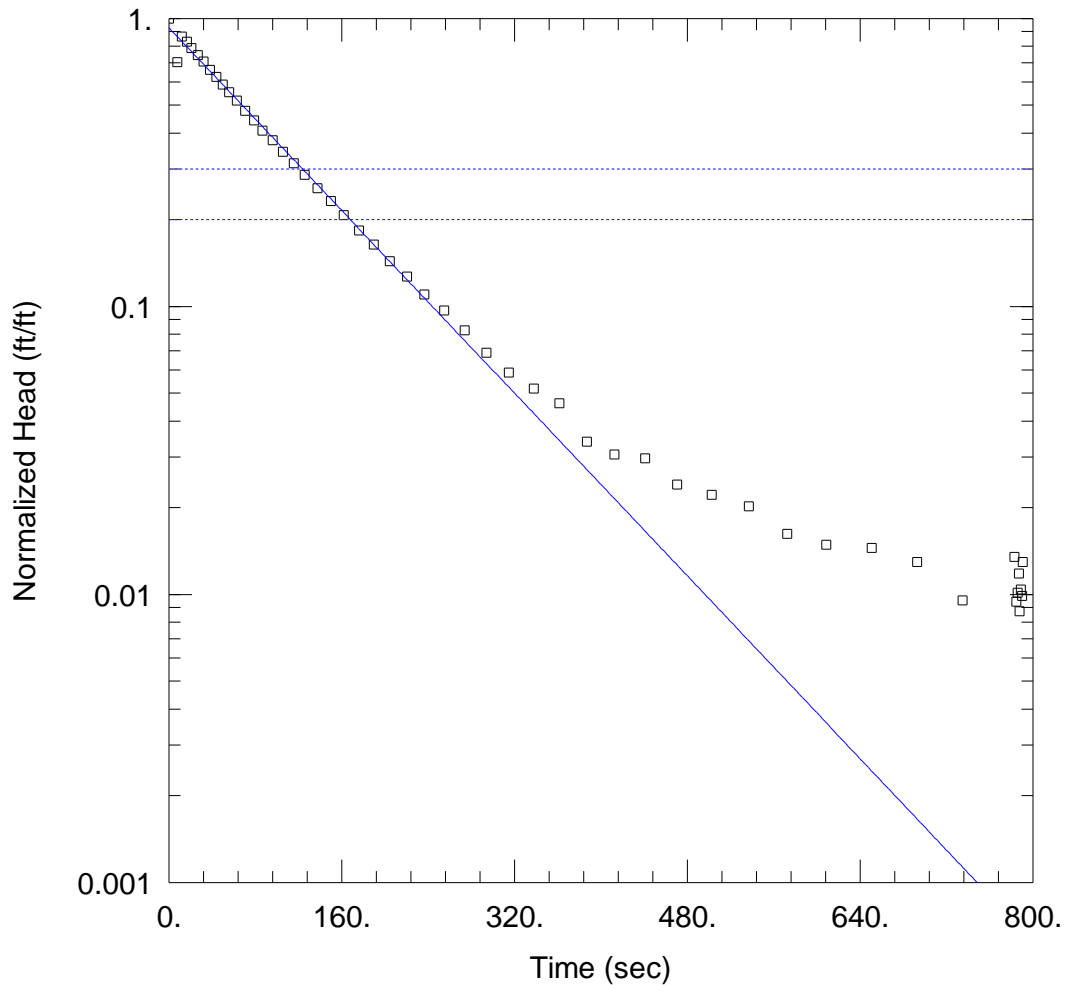
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 1.086$  ft/day

$y_0 = -0.5652$  ft



WELL TEST ANALYSIS

Data Set: C:\...\MW-39B\_Slug\_in.aqt  
 Date: 09/15/16

Time: 17:42:17

PROJECT INFORMATION

Company: AECOM  
 Client: Basin Electric  
 Project: 60506860  
 Test Well: 39B  
 Test Date: 8/23/16

AQUIFER DATA

Saturated Thickness: 25.17 ft

Anisotropy Ratio ( $K_z/K_r$ ): 1.

WELL DATA (39B)

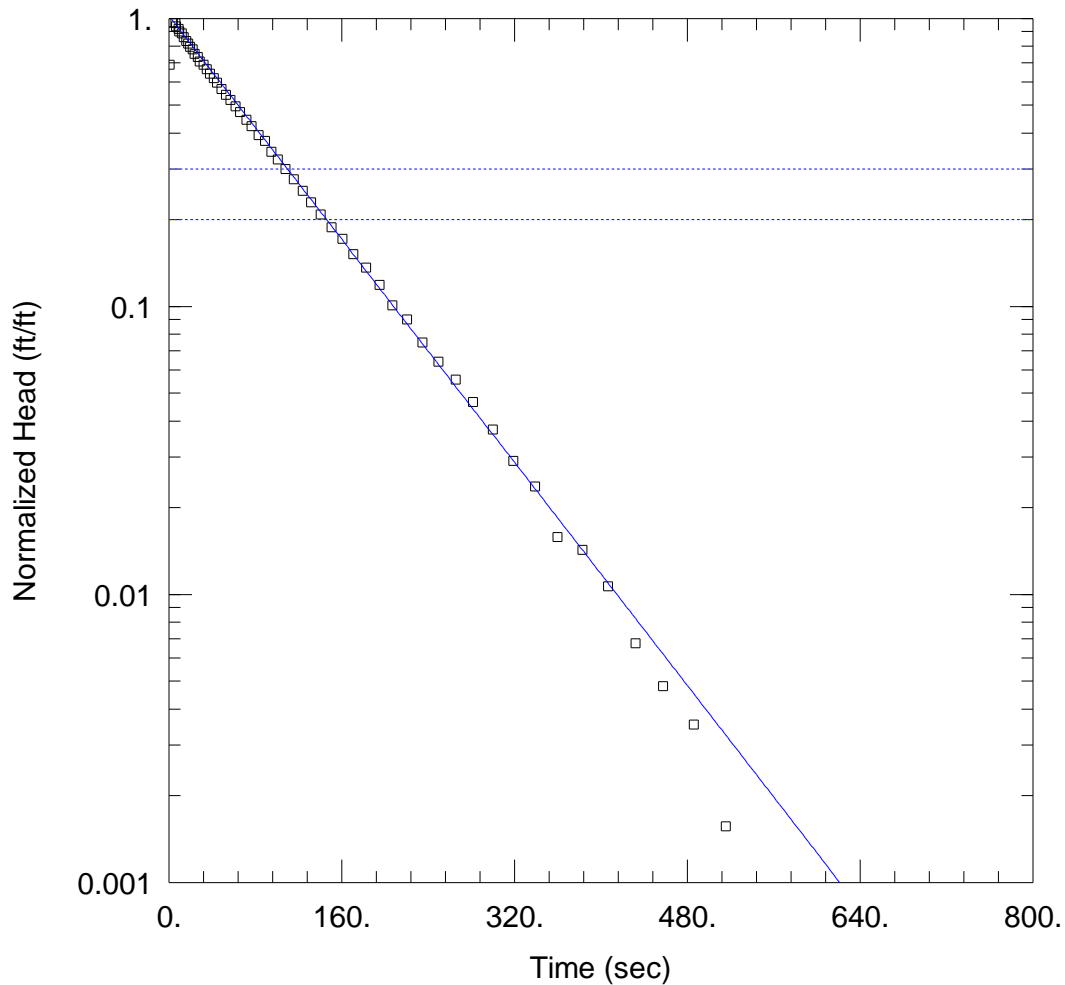
Initial Displacement: 2.428 ft  
 Total Well Penetration Depth: 20. ft  
 Casing Radius: 0.08612 ft

Static Water Column Height: 25.17 ft  
 Screen Length: 20. ft  
 Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined  
 K = 0.4514 ft/day

Solution Method: Bouwer-Rice  
 $y_0$  = 2.254 ft



### WELL TEST ANALYSIS

Data Set: C:\...\MW-39B\_Slug\_out.aqt

Date: 09/15/16

Time: 17:43:53

### PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 39B

Test Date: 8/23/16

### AQUIFER DATA

Saturated Thickness: 25.17 ft

Anisotropy Ratio ( $K_z/K_r$ ): 1.

### WELL DATA (39B)

Initial Displacement: -2.428 ft

Static Water Column Height: 25.17 ft

Total Well Penetration Depth: 20. ft

Screen Length: 20. ft

Casing Radius: 0.08612 ft

Well Radius: 0.25 ft

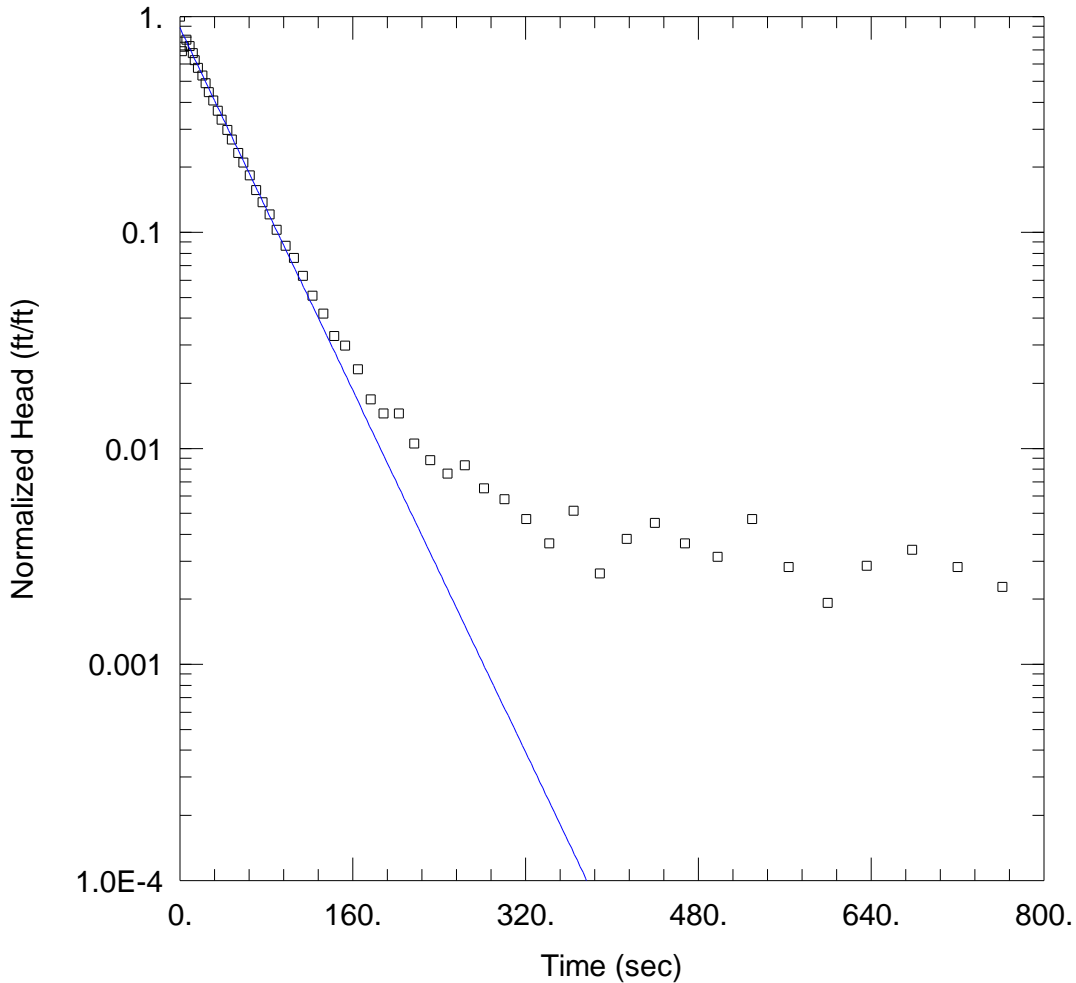
### SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.5514$  ft/day

$y_0 = -2.477$  ft



WELL TEST ANALYSIS

Data Set: C:\...\MW-42B\_Slug\_in.aqt  
 Date: 09/15/16

Time: 17:46:50

PROJECT INFORMATION

Company: AECOM  
 Client: Basin Electric  
 Project: 60506860  
 Test Well: 42B  
 Test Date: 8/19/16

AQUIFER DATA

Saturated Thickness: 21.62 ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (42B)

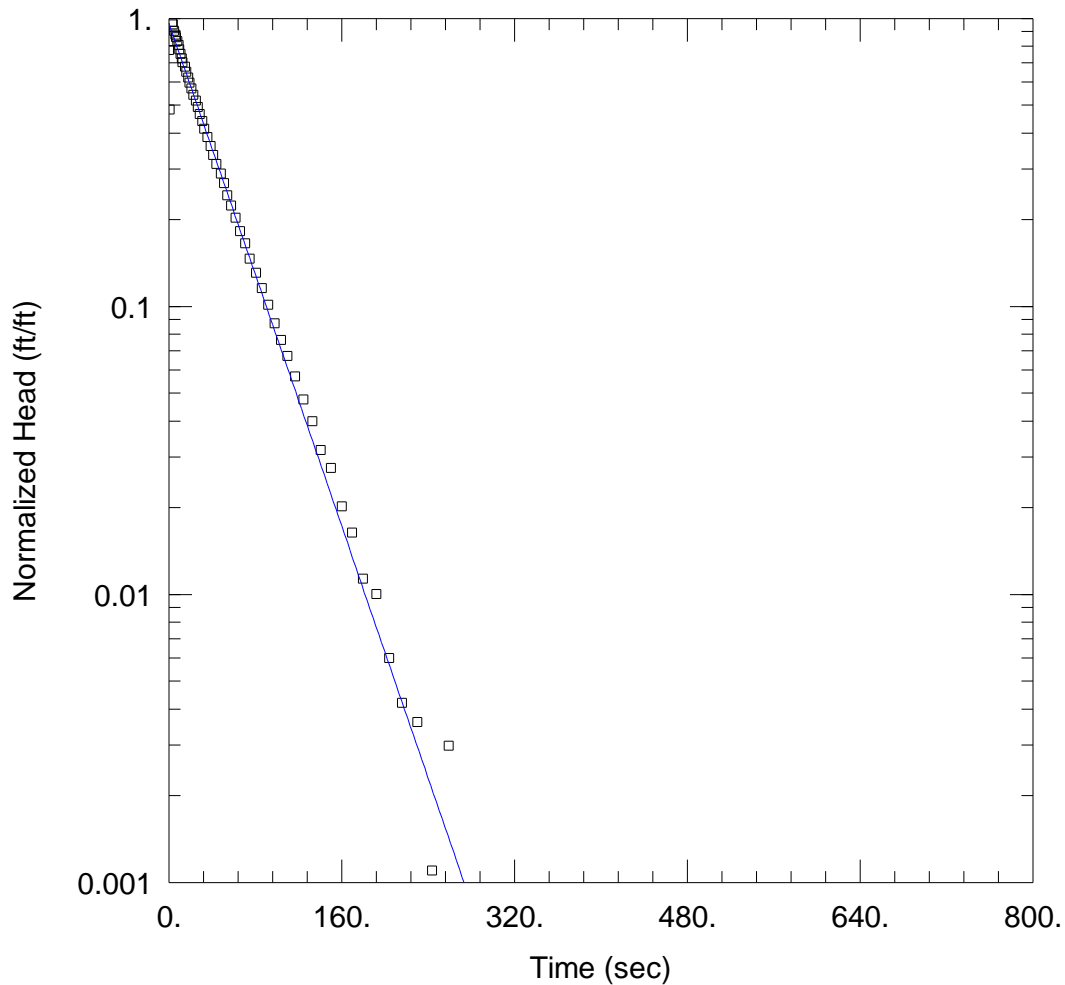
Initial Displacement: 2.428 ft  
 Total Well Penetration Depth: 20. ft  
 Casing Radius: 0.08612 ft

Static Water Column Height: 21.62 ft  
 Screen Length: 20. ft  
 Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined  
 K = 1.227 ft/day

Solution Method: Bouwer-Rice  
 y0 = 2.148 ft



WELL TEST ANALYSIS

Data Set: C:\...\MW-42B\_Slug\_out.aqt

Date: 09/15/16

Time: 17:49:00

PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 42B

Test Date: 8/19/16

AQUIFER DATA

Saturated Thickness: 21.62 ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (42B)

Initial Displacement: -2.428 ft

Static Water Column Height: 21.62 ft

Total Well Penetration Depth: 20. ft

Screen Length: 20. ft

Casing Radius: 0.08612 ft

Well Radius: 0.25 ft

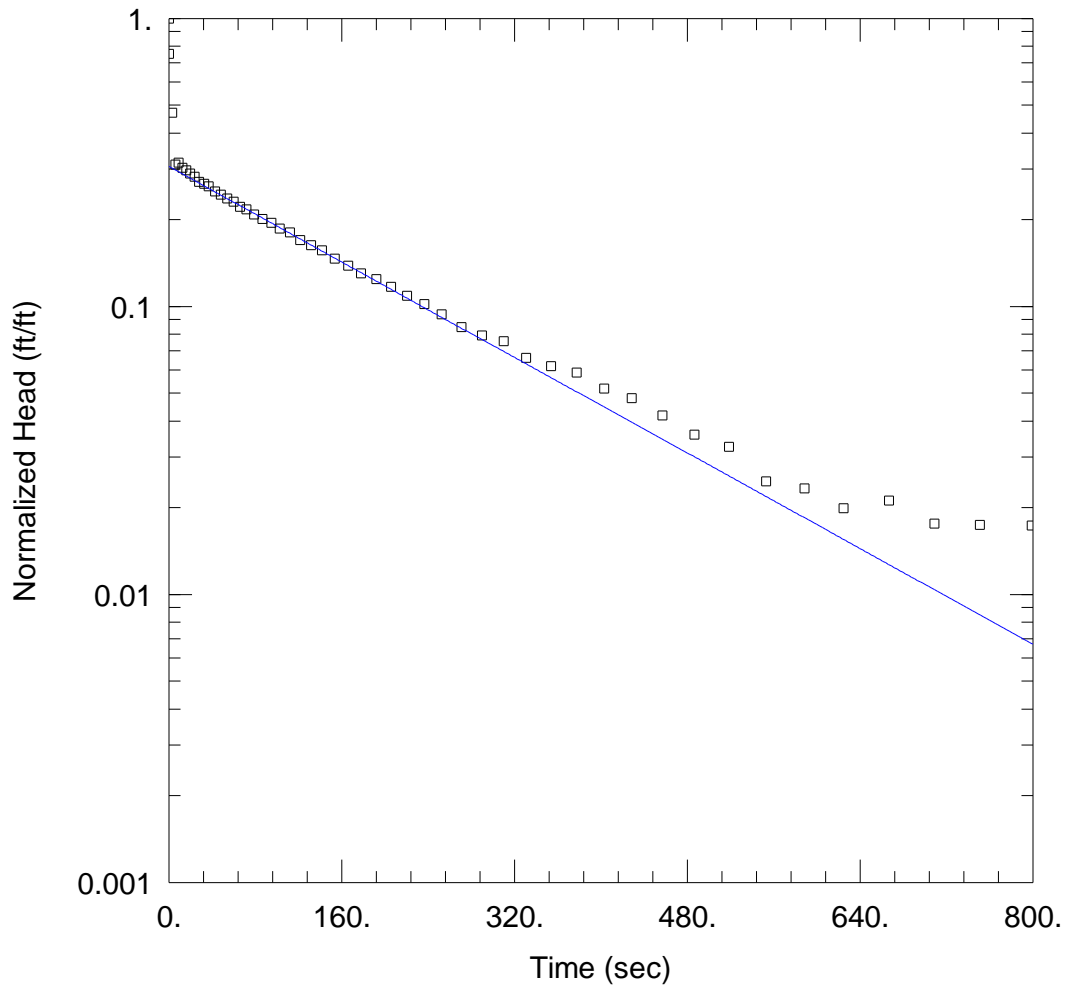
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 1.278 ft/day

y0 = -2.342 ft



### WELL TEST ANALYSIS

Data Set: C:\...\MW-45B\_Slug\_in.aqt  
 Date: 09/15/16

Time: 17:51:45

### PROJECT INFORMATION

Company: AECOM  
 Client: Basin Electric  
 Project: 60506860  
 Test Well: 45B  
 Test Date: 8/18/16

### AQUIFER DATA

Saturated Thickness: 12.8 ft

Anisotropy Ratio ( $K_z/K_r$ ): 1.

### WELL DATA (45B)

Initial Displacement: 2.428 ft  
 Total Well Penetration Depth: 20. ft  
 Casing Radius: 0.08612 ft

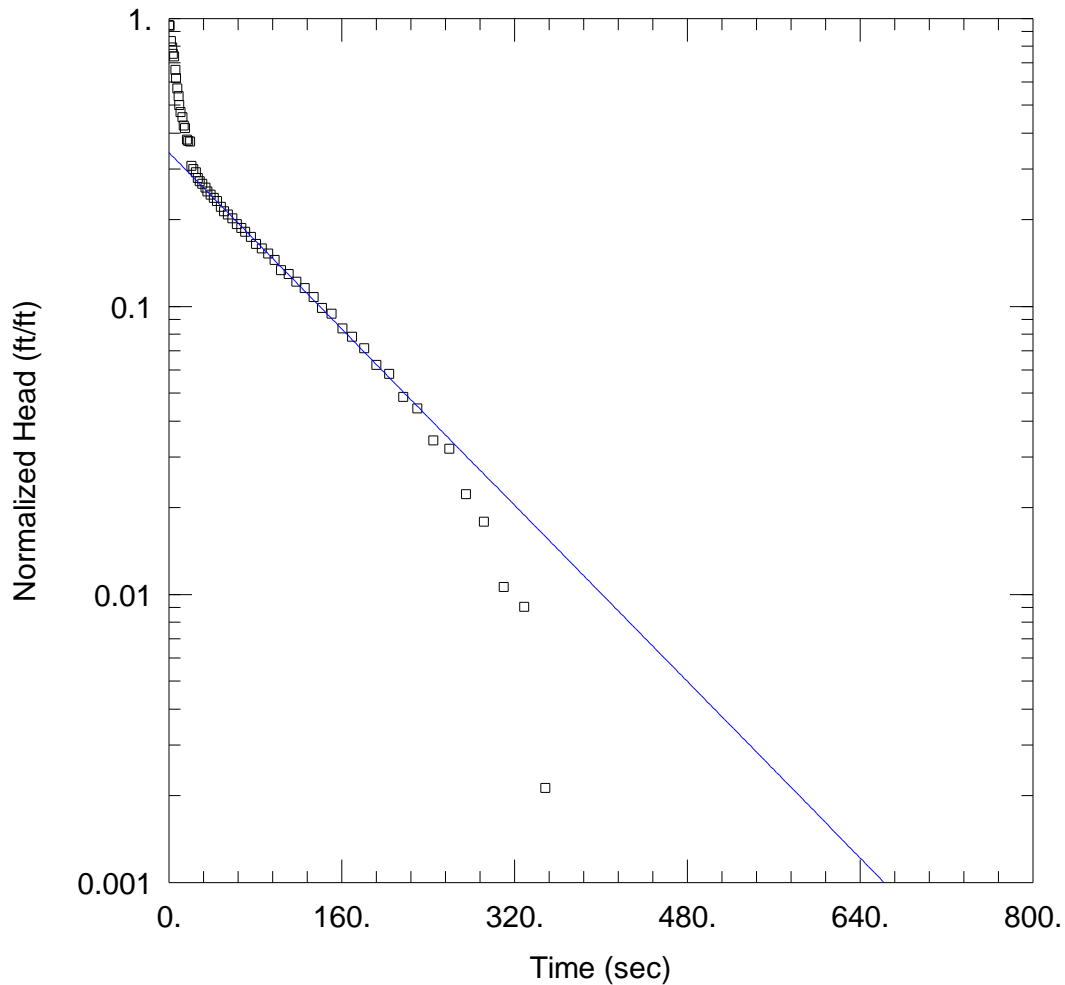
Static Water Column Height: 12.8 ft  
 Screen Length: 20. ft  
 Well Radius: 0.25 ft  
 Gravel Pack Porosity: 0.3

### SOLUTION

Aquifer Model: Unconfined  
 K = 1.272 ft/day

Solution Method: Bouwer-Rice  
 $y_0$  = 0.7434 ft





### WELL TEST ANALYSIS

Data Set: C:\...\MW-45B\_Slug\_out.aqt

Date: 09/15/16

Time: 17:55:35

### PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 45B

Test Date: 8/18/16

### AQUIFER DATA

Saturated Thickness: 12.8 ft

Anisotropy Ratio (Kz/Kr): 1.

### WELL DATA (45B)

Initial Displacement: -2.428 ft

Total Well Penetration Depth: 20. ft

Casing Radius: 0.08612 ft

Static Water Column Height: 12.8 ft

Screen Length: 20. ft

Well Radius: 0.25 ft

Gravel Pack Porosity: 0.3

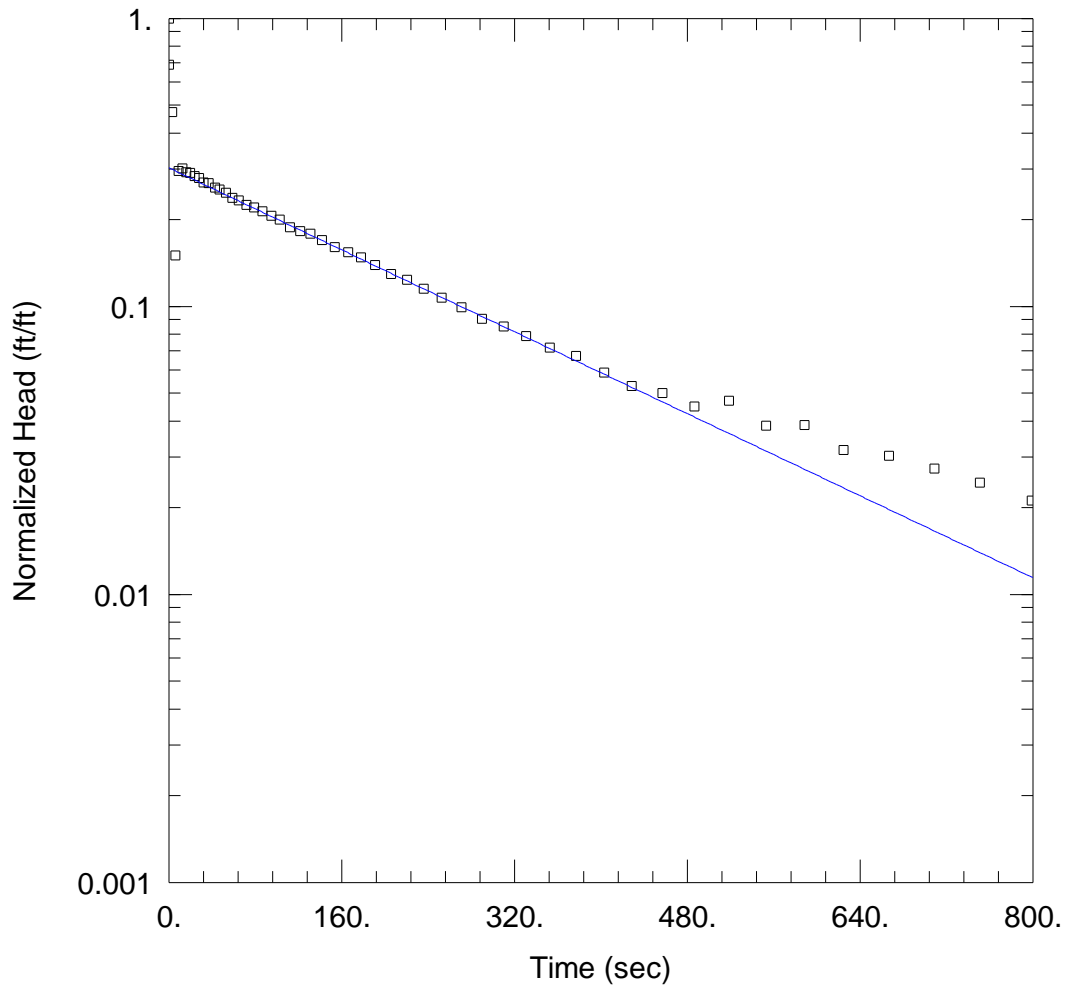
### SOLUTION

Aquifer Model: Unconfined

K = 2.347 ft/day

Solution Method: Bouwer-Rice

y0 = -0.8308 ft



WELL TEST ANALYSIS

Data Set: C:\...\MW-47B\_Slug\_in.aqt  
 Date: 09/15/16

Time: 17:58:04

PROJECT INFORMATION

Company: AECOM  
 Client: Basin Electric  
 Project: 60506860  
 Test Well: 47B  
 Test Date: 8/18/16

AQUIFER DATA

Saturated Thickness: 12.53 ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (45B)

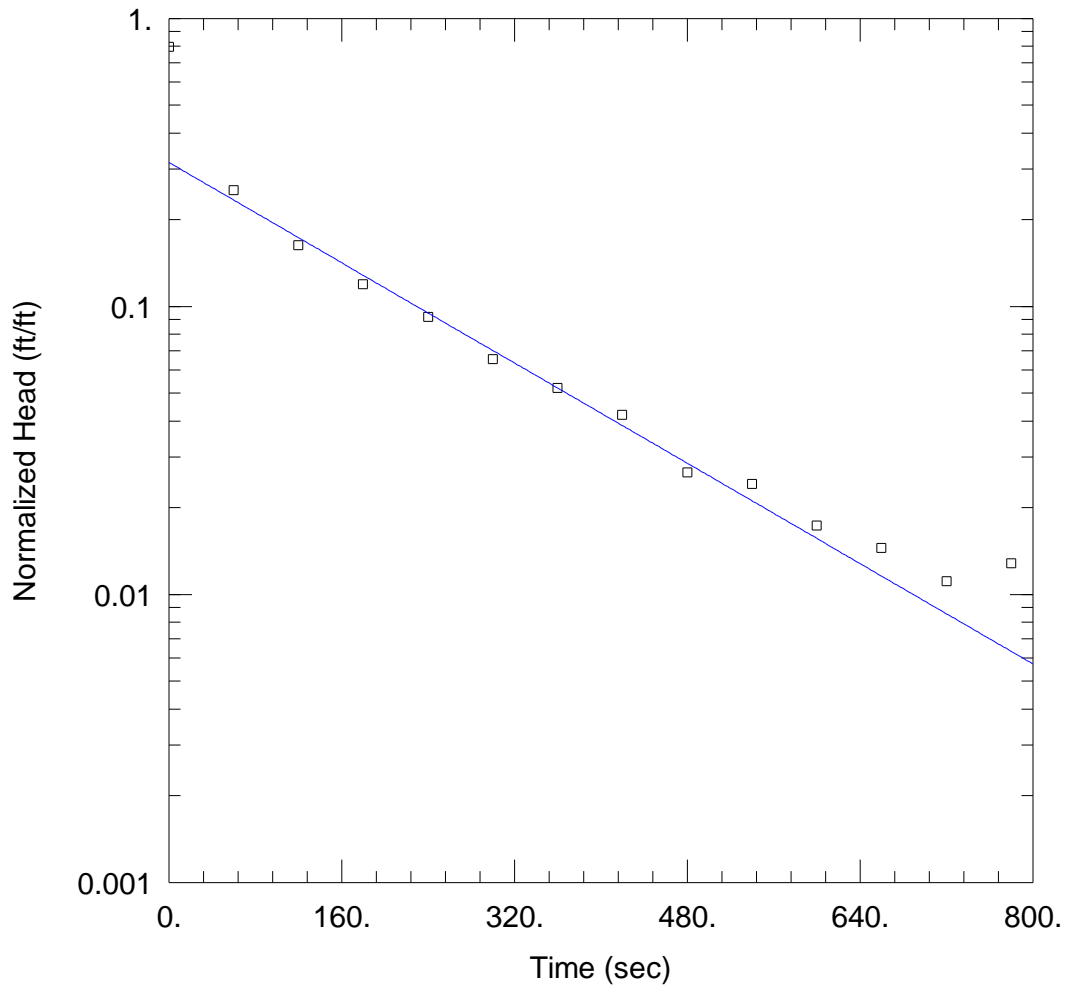
Initial Displacement: 2.428 ft  
 Total Well Penetration Depth: 20. ft  
 Casing Radius: 0.08612 ft

Static Water Column Height: 12.53 ft  
 Screen Length: 20. ft  
 Well Radius: 0.25 ft  
 Gravel Pack Porosity: 0.3

SOLUTION

Aquifer Model: Unconfined  
 K = 1.112 ft/day

Solution Method: Bouwer-Rice  
 y0 = 0.7345 ft



WELL TEST ANALYSIS

Data Set: C:\...\MW-47B\_Slug\_out.aqt

Date: 09/15/16

Time: 17:59:43

PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 47B

Test Date: 8/18/16

AQUIFER DATA

Saturated Thickness: 12.53 ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (45B)

Initial Displacement: -2.428 ft

Total Well Penetration Depth: 20. ft

Casing Radius: 0.08612 ft

Static Water Column Height: 12.53 ft

Screen Length: 20. ft

Well Radius: 0.25 ft

Gravel Pack Porosity: 0.3

SOLUTION

Aquifer Model: Unconfined

K = 1.361 ft/day

Solution Method: Bouwer-Rice

y0 = -0.7672 ft

PUMPING TEST DATA FORM

Well ID MW-32B Personnel Chris Ahrendt & Jeremy Hurshman  
 Location Basin Electric LB Static Water Level 60.43  
 Type of Well PVC Schedule 40 Extraction Well Distance —  
 Test Date 8/22/2016 Total Casing Depth 76.74  
 Measuring Point Elevation Top of Inner Casing Borehole Diameter 6"  
 Type of Test Recovery Casing Diameter 2"  
 Step Number — Screened Interval —  
 Data logger Test Run No. 1 Sand Pack Interval —  
 Pumping Rate 0.8 gpm Lithology Tested —  
 Test Start Time 1606 Test End Time 1830

Start 1604 AM  
1843

Pump off 1735

Time	Elapsed Time (min)	Water Depth (ft)	Time	Elapsed Time (min)	Water Depth (ft)
1604	0	60.30			
1620	14	10gal / 7.76			
1631	25	20gal / 7.62			
1644	38	30gal / 7.54			
1657	51	40gal / 7.51			
1709	63	50gal / 7.47			
1722	76	60gal / 7.48			
1735	89	70gal / 7.47			
1740	94	60.22			
1748	102	60.65			
1755	109	60.56			
1759	113	60.51			
1804	118	60.49			
1814	128	60.45			
1819	133	60.45			
1824	135	60.43			

**PUMPING TEST DATA FORM**

Well ID MW-34B Personnel Chris Almond & Jeremy Hurshman  
 Location Basin Electric Static Water Level 66.54  
 Type of Well PC, Schedule 40 Extraction Well Distance \_\_\_\_\_  
 Test Date 8/22/2016 Total Casing Depth 88.78  
 Measuring Point Elevation Top of Inner Casing Borehole Diameter 6"  
 Type of Test Recorder Casing Diameter 2"  
 Step Number \_\_\_\_\_ Screened Interval \_\_\_\_\_  
 Data logger Test Run No. \_\_\_\_\_ Sand Pack Interval \_\_\_\_\_  
 Pumping Rate 1 gpm Lithology Tested \_\_\_\_\_  
 Test Start Time 12:52 PM Test End Time \_\_\_\_\_

Time	Elapsed Time (min)	Water Depth (ft)	Time	Elapsed Time (min)	Water Depth (ft)
1251	0	66.56			
1304	12	10 gal / 69.05			
1316	24	20 gal / 7.67			
1327	35	30 gal / 7.70			
1339	47	40 gal / 7.72			
1350	58	50 gal / 7.78			
1402	70	60 gal / 7.71			
1409	79	70 gal / 7.76			
1414	stopped pump	nm			
1416	86	72.40			
1423	93	67.22			
1432	102	66.69			
1439	109	66.67			
1452	122	66.63			
1502	132	66.61			
1509	139	66.62			

PUMPING TEST DATA FORM

Well ID MW-36B Personnel Chris Anzart & Jeremy Hurshin  
 Location Basin Electric LRS Static Water Level 61.21  
 Type of Well PVC Schedule 40 Extraction Well Distance N/A  
 Test Date 8/22/2016 Total Casing Depth 80.25  
 Measuring Point Elevation Top of PVC casing Borehole Diameter 6"  
 Type of Test \_\_\_\_\_ Casing Diameter 2"  
 Step Number \_\_\_\_\_ Screened Interval \_\_\_\_\_  
 Data logger Test Run No. - Sand Pack Interval \_\_\_\_\_  
 Pumping Rate 0.7 gpm Lithology Tested \_\_\_\_\_  
 Test Start Time 10:17 AM Test End Time 12:12 PM

10:17 AM  
start  
pump

stopped pump @  
11:51 PM

stopped test

Time	Elapsed Time (min)	Water Depth (ft)	Height of the over press	Time	Elapsed Time (min)	Water Depth (ft)
10:15 AM	0	61.22				
10:31	14	10 gal / 12.90	↓			
10:46	29	20 gal / 12.85	↓			
11:00	43	30 gal / 12.87	↑			
11:14	57	40 gal / 12.84	↓			
11:28	71	50 gal / 12.84	-			
11:43	86	60 gal / 12.85	↑			
11:51		62.5 gal / NR				
12:04		61.23				
12:12 PM		61.22				

PUMPING TEST DATA FORM

Well ID MW-40B Personnel Chris Ahrendt & Jeremy Hurshman  
 Location Basin Electric Static Water Level 94.89  
 Type of Well PVC, Schedule 40 Extraction Well Distance —  
 Test Date 8/23/2010 Total Casing Depth 111.10  
 Measuring Point Elevation Top of Inner casing Borehole Diameter 6"  
 Type of Test Agulter Test Casing Diameter 2"  
 Step Number — Screened Interval —  
 Data logger Test Run No. 1 Sand Pack Interval —  
 Pumping Rate ~ 0.9 gpm Lithology Tested —  
 Test Start Time — Test End Time —

Time	Elapsed Time (min)	Water Depth (ft)	Time	Elapsed Time (min)	Water Depth (ft)
0939	0	94.88			
0940	1 min	Pump on			
0951	12 min	10 gal / 3.10			
1003	26 min	20 gal / 2.72			
1016	39 min	30 gal / 2.65			
1029	52 min	40 gal / 2.61			
1042	65 min	50 gal / 2.58			
1054	77 min	60 gal / 2.55			
1101	84 min	65 gal / 2.56			
1104	Pump off	NM			
1106	89 min	98.58			
1112	95 min	96.62			
1118	104 min	95.69			
1132	118 min	95.15			
1138	126 min	95.10			
1146	134 min	95.05			
1157	145 min	95.03			
1206	154 min	95.02			

\* See transducer data for details

**PUMPING TEST DATA FORM**

Well ID MW-413 Personnel Chris Ahrendt  
 Location Basin Electric Static Water Level 56.71 1040 AM 8/19/2016 pre set-up  
 Type of Well Schedule 40 PVC Extraction Well Distance —  
 Test Date 8/19/2016 Total Casing Depth 75.51  
 Measuring Point Elevation Top of Inner Casing Borehole Diameter 6"  
 Type of Test Aquifer constant rate Casing Diameter 2"  
 Step Number — Screened Interval —  
 Data logger Test Run No. 1 Sand Pack Interval —  
 Pumping Rate 1 gpm Lithology Tested —  
 Test Start Time 1049 Test End Time —

Time	Elapsed Time (min)	Water Depth (ft)	Time	Elapsed Time (min)	Water Depth (ft)
1048	0	56.77			
1059	11	70 gal / 12.81			
1107	19	20 gal / 12.80			
1117	29	30 gal / 12.79			
1128	40	40 gal / 12.78			
1142	54	55 gal / 12.76-12.78			
1150	62	60 gal / 12.78			
1200	72	70 gal /			
1201	73	71 gal /			
1224		56.81 ft			
1238		56.81 ft			

pump off

Temperature drop and wind increase occurred at 11:20-11:30 AM, strong wind gusts



PUMPING TEST DATA FORM

Well ID MW-43B Personnel Chris Albrecht & Jeremy Hurshman  
 Location Basin Electric Static Water Level 7.38' static 24.48' Top of Inner Casing  
 Type of Well PVC Schrod 40 Extraction Well Distance \_\_\_\_\_  
 Test Date 8/19/2016 Total Casing Depth 7.38' @ 14 79.15' Top of Inner Casing  
 Measuring Point Elevation Top of PVC Casing Borehole Diameter 6"  
 Type of Test Constant Rate Recovery Casing Diameter 2"  
 Step Number - Screened Interval \_\_\_\_\_  
 Data logger Test Run No. \_\_\_\_\_ Sand Pack Interval \_\_\_\_\_  
 Pumping Rate ~ 1 gpm start of test Lithology Tested \_\_\_\_\_  
 Test Start Time \_\_\_\_\_ Test End Time \_\_\_\_\_

start 8:19 AM  
test & pump  
  
~ 1 gpm

Time	Elapsed Time (min)	Water Depth (ft)	Time	Elapsed Time (min)	Water Depth (ft)
8:18 AM	0	24.49 static			
8:29	10	10 gal / 43.95			
8:40	21	20 gal / 43.80			
8:48	29	30 gal / 43.77			
0858	39	40 gal / 43.77			
0908	49	50 gal / 43.77			
0919	60	60 gal / 43.81			
0930	71	70 gal / 43.79			
0942	83	80 gal / 43.78			
0947	88	85 gal / 43.77			
0947	pump stopped - recovery				
0951	91	24.91' static			
0959	99	24.56			
1002	102	24.54			
1007	107	24.52			
1011	111	24.52			

PUMPING TEST DATA FORM

Well ID MW-44B Personnel Chris Ahrens & Jeremy Hurshman  
 Location Basin Electric LBS Static Water Level 70.58' without equipment  
 Type of Well 2" PVC Extraction Well Distance \_\_\_\_\_  
 Test Date 8/18/2016 Total Casing Depth 94.06'  
 Measuring Point Elevation Top of PVC casing Borehole Diameter 6"  
 Type of Test Constant Rate Casing Diameter 2"  
 Step Number - Screened Interval \_\_\_\_\_  
 Data logger Test Run No. \_\_\_\_\_ Sand Pack Interval \_\_\_\_\_  
 Pumping Rate \_\_\_\_\_ Lithology Tested \_\_\_\_\_  
 Test Start Time \_\_\_\_\_ Test End Time \_\_\_\_\_

(Bad data)

(Bad data)

	Time	Elapsed Time (min)	Water Depth (ft)		Time	Elapsed Time (min)	Water Depth (ft)
Test 1 (Trial) (1 gpm)	09:18	∅	70.59 static				
	09:37		71.34 recovery				
	09:44		70.65				
	09:46		70.64				
Test 2 (0.5 gpm)	09:55	∅	70.63 static				
	10:09		70.64 recovery				

PUMPING TEST DATA FORM

Well ID MW-44B Personnel Chris Alvarado & Jeremy Hurshman  
 Location Basin Electric LRS Static Water Level \_\_\_\_\_  
 Type of Well 2" PVC Extraction Well Distance \_\_\_\_\_  
 Test Date 8/10/2016 Total Casing Depth 94.06  
 Measuring Point Elevation Top of firmer PVC casing Borehole Diameter 6"  
 Type of Test Constant Rate Casing Diameter 2"  
 Step Number - Screened Interval \_\_\_\_\_  
 Data logger Test Run No. \_\_\_\_\_ Sand Pack Interval \_\_\_\_\_  
 Pumping Rate 0.4 gpm Lithology Tested \_\_\_\_\_  
 Test Start Time \_\_\_\_\_ Test End Time \_\_\_\_\_

44B  
 MW-44B  
 Test 3  
 (Bad data)

Time	Elapsed Time (min)	Water Depth (ft)	Time	Elapsed Time (min)	Water Depth (ft)
1044	∅	70.58			
1045	1 start test				

MW-44B  
 Test 4  
 ~ 1.5 gpm  
 (good data)

1121	∅	70.59
1122	start test	NM
1130	10 gallons	NM
1137	20 gallons	NM
1144	30 gallons	NM
1151	40 gallons	NM
1158	50 gallons	NM
Stopped pump at 1158 - recovery time.		
1202		70.84
1205		70.68
1210		70.64
1213		70.63
1235		70.60
1236	Stopped test	

**PUMPING TEST DATA FORM**

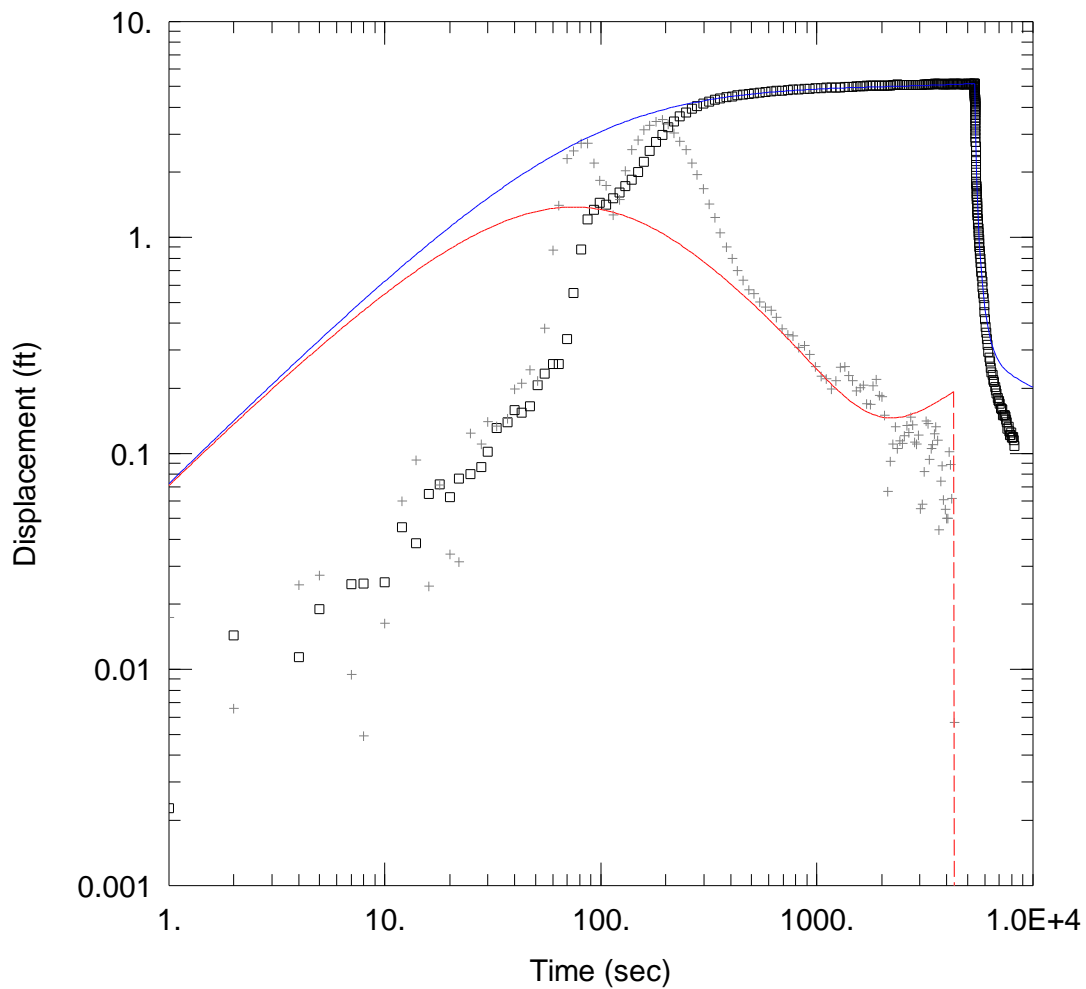
Well ID NW-46B Personnel Chris Ahrendt & Jeremy Hurshman  
 Location Basin Electric LRS Static Water Level 76.00 76.00  
 Type of Well PVC, Sch 40 Extraction Well Distance NA  
 Test Date 8/18/2016 Total Casing Depth 95.41  
 Measuring Point Elevation Top of inner PVC casing Borehole Diameter 6"  
 Type of Test Recovery Casing Diameter 2"  
 Step Number - Screened Interval \_\_\_\_\_  
 Data logger Test Run No. - Sand Pack Interval \_\_\_\_\_  
 Pumping Rate ~1.4 gpm Lithology Tested \_\_\_\_\_  
 Test Start Time 13:18 Test End Time \_\_\_\_\_

Time	Elapsed Time (min)	Water Depth (ft) / <small>ft above transducer</small>	Time	Elapsed Time (min)	Water Depth (ft)
1317	0	76.00			
1318	start test	NM			
1327	9	10 gal			
1335	17	20 gal / 7.97			
1344	26	30 gal / 7.59			
1353	35	40 gal / 7.44			
1401	43	50 gal / 7.39			
1410	52	60 gal / 7.36			
1419	61	70 gal / 7.34			
1427	69	80 gal / 7.32			
1435	77	90 gal / 7.32			
1444	86	100 gal / 7.24			
1454	96	110 gal / 7.25			
1505	107	120 gal / 7.28			
1511	113	130 / 7.31			
1519	121	140 gal / 7.30			
1520 AM		1425 total gallons			
1526 PM		77.86' / 14.78'			
1531 PM		76.87' / 16.27'			
1536 PM		76.41' / 16.52'			
1541 PM		76.23' / 16.83'			
1546 PM	stopped test	76.16 / 16.92			

1.2 gpm

1.2 gpm

pump off @



### WELL TEST ANALYSIS

Data Set: C:\...\MW-32B\_Pumping\_Test.aqt

Date: 09/22/16

Time: 20:00:17

### PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 32B

Test Date: 8/22/16

### AQUIFER DATA

Saturated Thickness: 12.59 ft

Anisotropy Ratio ( $K_z/K_r$ ): 1.

### WELL DATA

#### Pumping Wells

#### Observation Wells

Well Name	X (ft)	Y (ft)
32B	0	0

Well Name	X (ft)	Y (ft)
□ 32B	0	0

### SOLUTION

Aquifer Model: Unconfined

Solution Method: Moench

T = 16.21 ft<sup>2</sup>/day

S = 0.001872

Sy = 0.1

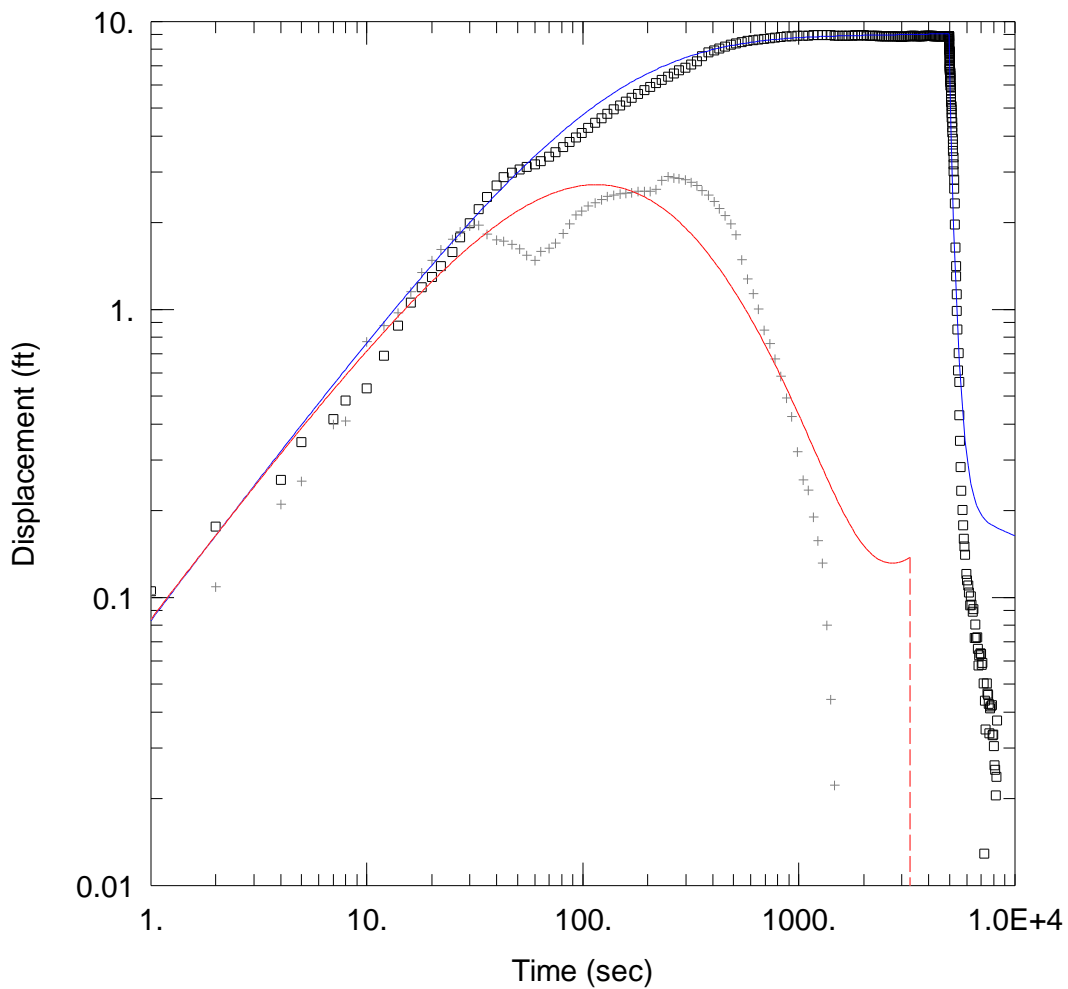
$\beta$  = 0.0003941

Sw = 0.

r(w) = 0.25 ft

r(c) = 0.08612 ft

alpha = 1.0E+30 sec<sup>-1</sup>



### WELL TEST ANALYSIS

Data Set: C:\...\MW-34B\_Pumping\_Test.aqt

Date: 09/22/16

Time: 20:02:29

### PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 34B

Test Date: 8/22/16

### AQUIFER DATA

Saturated Thickness: 16.62 ft

Anisotropy Ratio ( $K_z/K_r$ ): 1.

### WELL DATA

#### Pumping Wells

#### Observation Wells

Well Name	X (ft)	Y (ft)
34B	0	0

Well Name	X (ft)	Y (ft)
□ 34B	0	0

### SOLUTION

Aquifer Model: Unconfined

Solution Method: Moench

T = 10.88 ft<sup>2</sup>/day

S = 0.0006148

Sy = 0.1

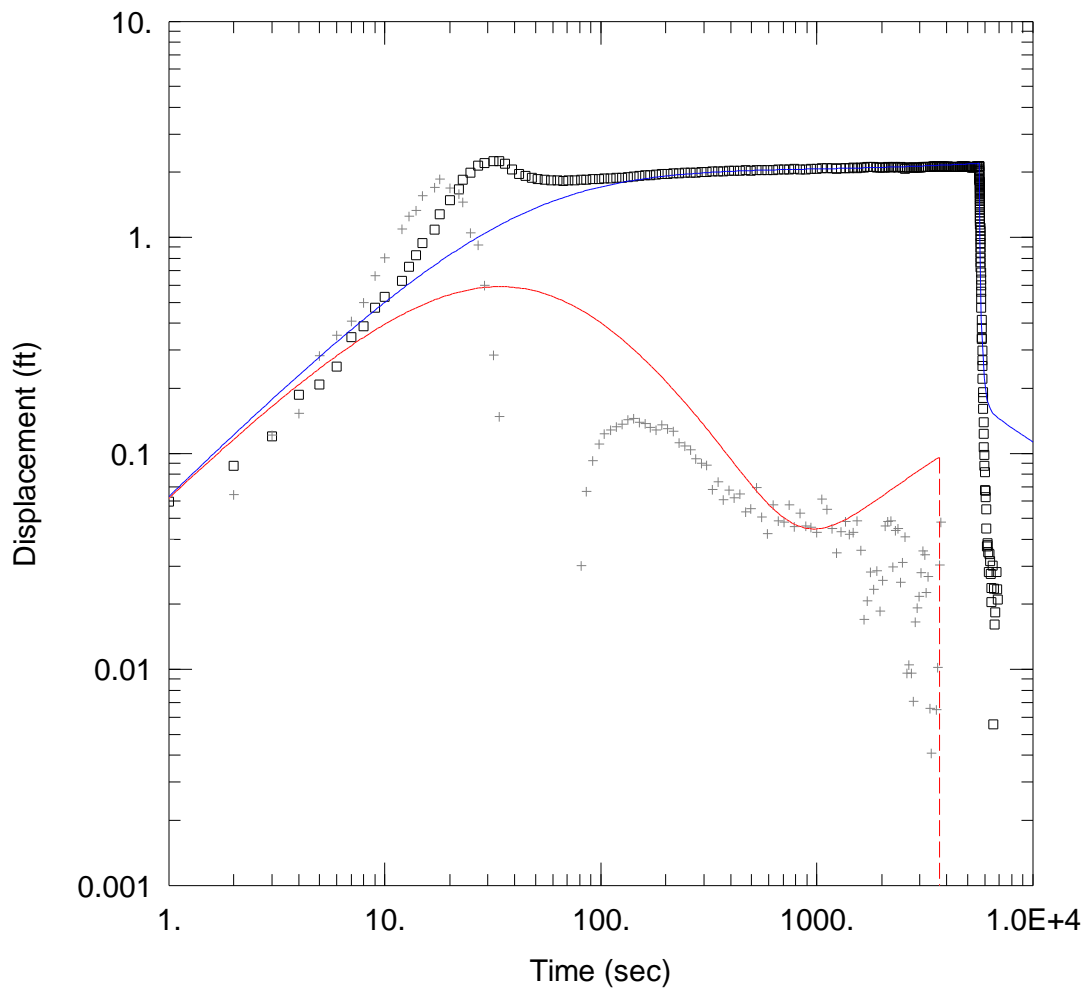
$\beta$  = 0.0002262

Sw = 0.

r(w) = 0.25 ft

r(c) = 0.08612 ft

alpha = 1.0E+30 sec<sup>-1</sup>



WELL TEST ANALYSIS

Data Set: C:\...\MW-36B\_Pumping\_Test.aqt

Date: 09/22/16

Time: 20:06:04

PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 36B

Test Date: 8/22/16

AQUIFER DATA

Saturated Thickness: 14.97 ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA

Pumping Wells

Observation Wells

Well Name	X (ft)	Y (ft)
36B	0	0

Well Name	X (ft)	Y (ft)
□ 36B	0	0

SOLUTION

Aquifer Model: Unconfined

Solution Method: Moench

T = 36.22 ft<sup>2</sup>/day

S = 0.001105

Sy = 0.09859

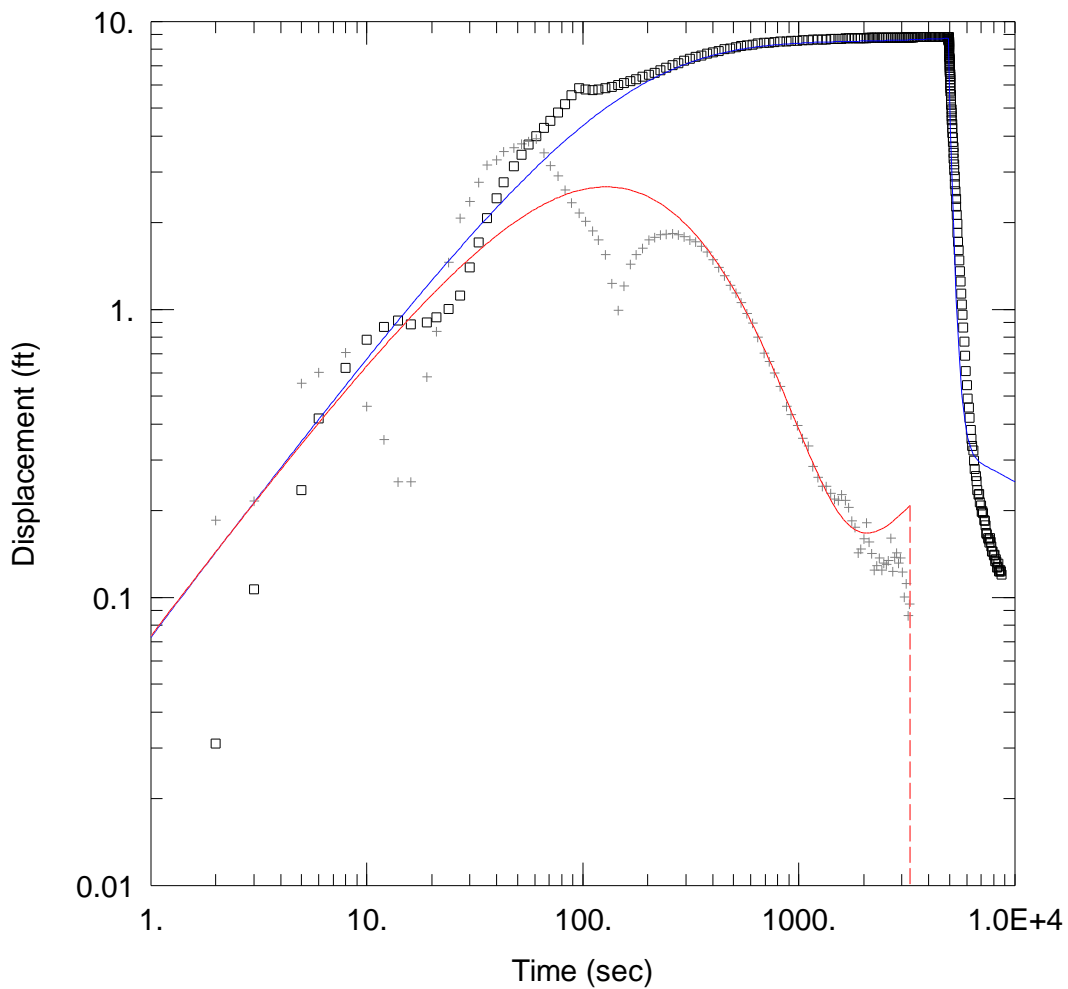
β = 0.000279

Sw = 0.

r(w) = 0.25 ft

r(c) = 0.08612 ft

alpha = 1.0E+30 sec<sup>-1</sup>



### WELL TEST ANALYSIS

Data Set: C:\...\MW-40B\_Pumping\_Test.aqt

Date: 09/22/16

Time: 20:09:17

### PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 40B

Test Date: 8/23/16

### AQUIFER DATA

Saturated Thickness: 11.39 ft

Anisotropy Ratio ( $K_z/K_r$ ): 1.

### WELL DATA

#### Pumping Wells

#### Observation Wells

Well Name	X (ft)	Y (ft)
40B	0	0

Well Name	X (ft)	Y (ft)
□ 40B	0	0

### SOLUTION

Aquifer Model: Unconfined

Solution Method: Moench

T = 8.988 ft<sup>2</sup>/day

S = 0.0007605

Sy = 0.09996

$\beta$  = 0.0004818

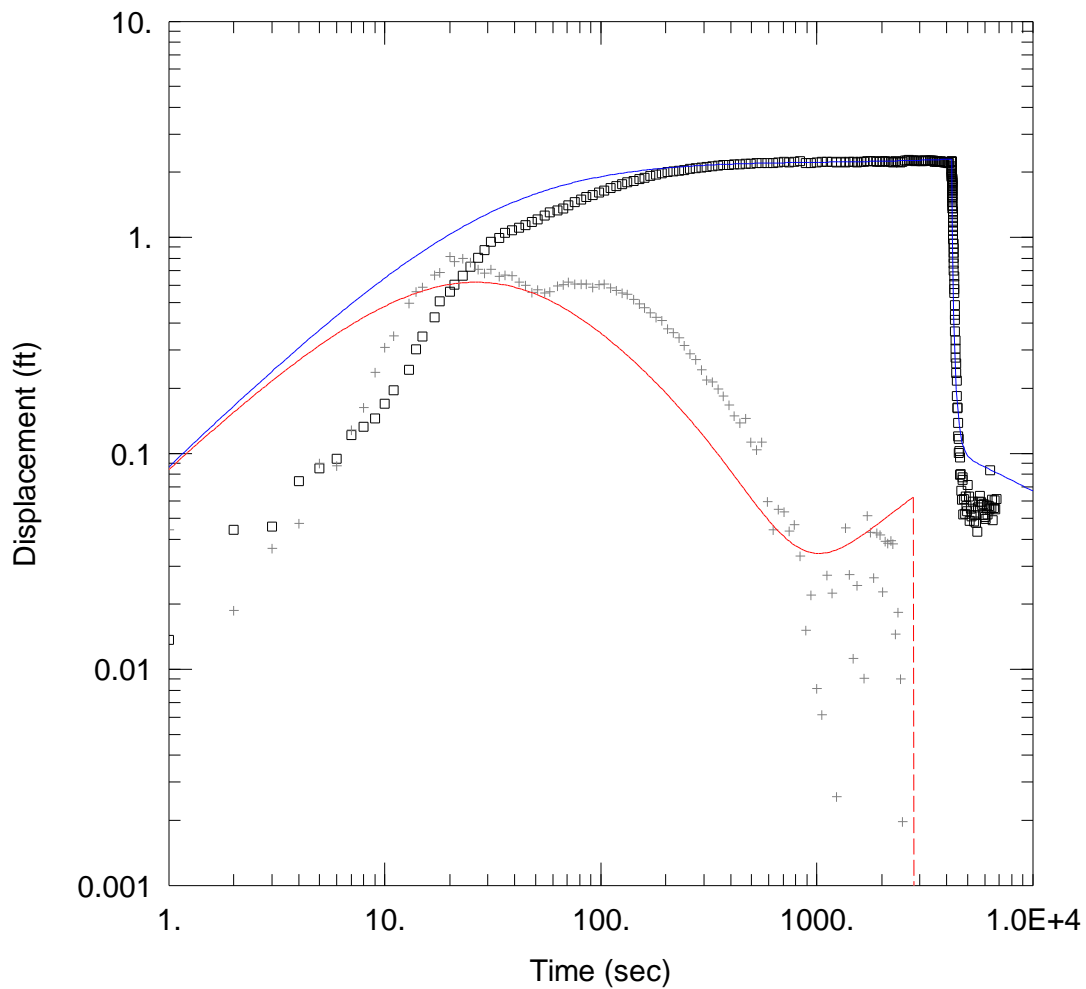
Sw = 0.

r(w) = 0.25 ft

r(c) = 0.08612 ft

alpha = 1.0E+30 sec<sup>-1</sup>





WELL TEST ANALYSIS

Data Set: C:\...\MW-41B\_Pumping\_Test.aqt

Date: 09/22/16

Time: 20:09:57

PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 41B

Test Date: 8/19/16

AQUIFER DATA

Saturated Thickness: 15.03 ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA

Pumping Wells

Observation Wells

Well Name	X (ft)	Y (ft)
41B	0	0

Well Name	X (ft)	Y (ft)
□ 41B	0	0

SOLUTION

Aquifer Model: Unconfined

Solution Method: Moench

T = 46.84 ft<sup>2</sup>/day

S = 0.001378

Sy = 0.1972

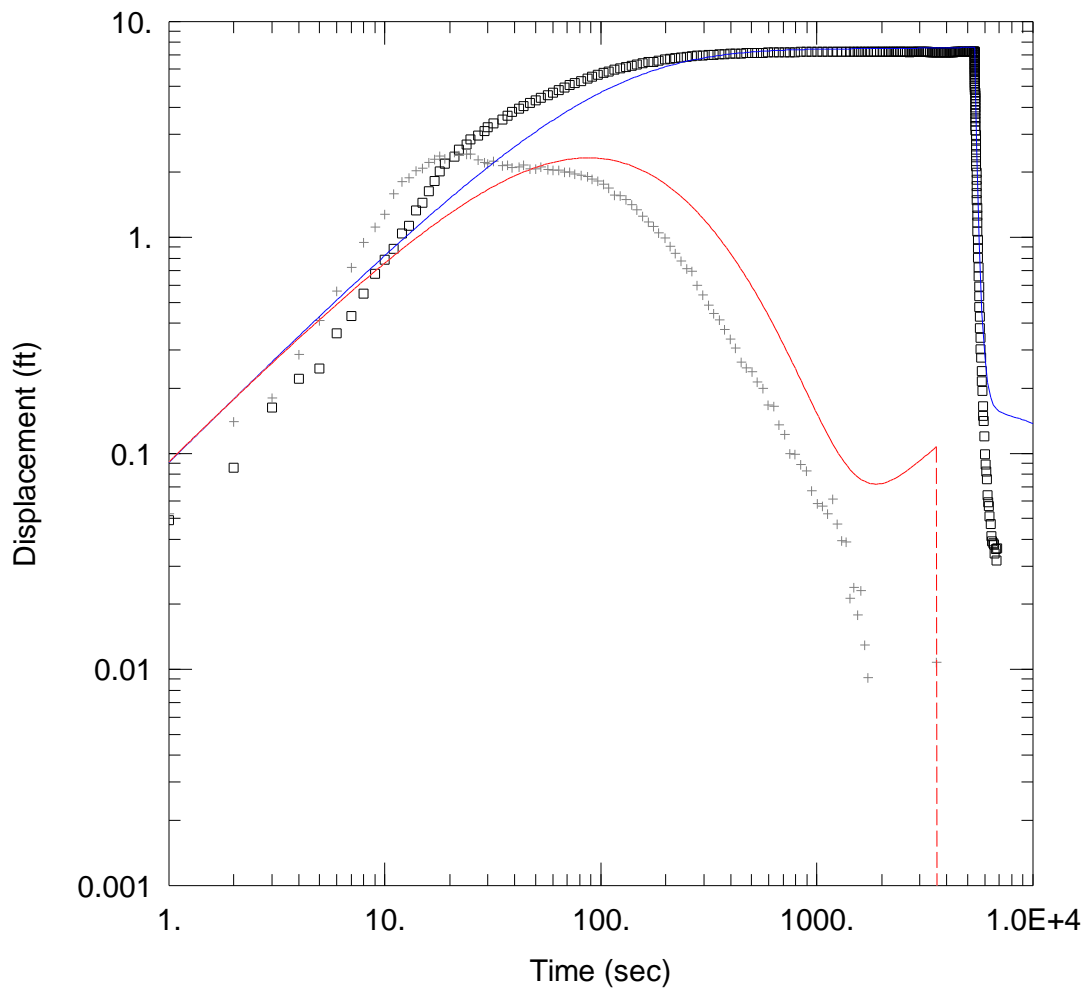
β = 0.0002768

Sw = 0.

r(w) = 0.25 ft

r(c) = 0.08612 ft

alpha = 1.0E+30 sec<sup>-1</sup>



### WELL TEST ANALYSIS

Data Set: C:\...\MW-43B\_Pumping\_Test.aqt

Date: 09/22/16

Time: 20:10:26

### PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 43B

Test Date: 8/19/16

### AQUIFER DATA

Saturated Thickness: 20. ft

Anisotropy Ratio (Kz/Kr): 1.

### WELL DATA

#### Pumping Wells

#### Observation Wells

Well Name	X (ft)	Y (ft)
43B	0	0

Well Name	X (ft)	Y (ft)
□ 43B	0	0

### SOLUTION

Aquifer Model: Unconfined

Solution Method: Moench

T = 14.9 ft<sup>2</sup>/day

S = 0.0003493

Sy = 0.1007

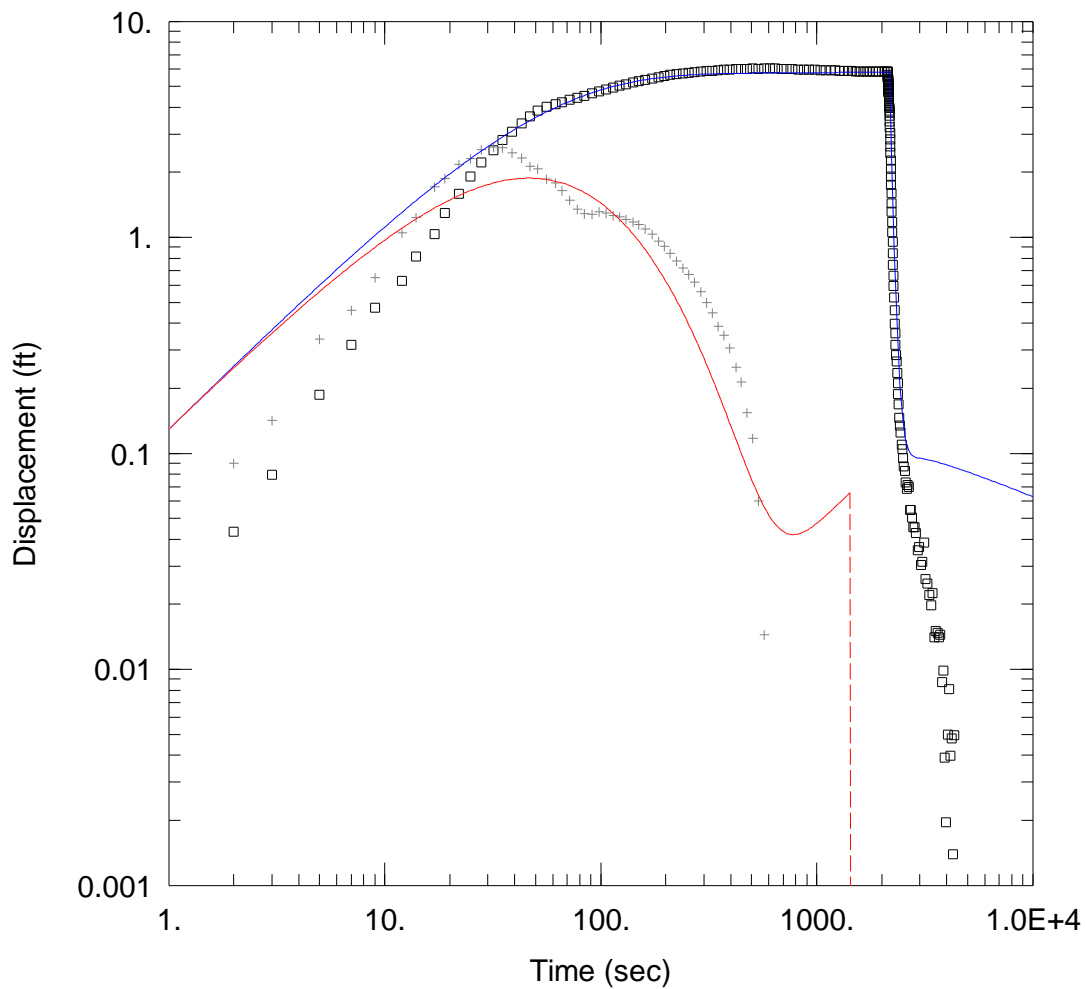
β = 0.0001563

Sw = 0.

r(w) = 0.25 ft

r(c) = 0.08612 ft

alpha = 1.0E+30 sec<sup>-1</sup>



WELL TEST ANALYSIS

Data Set: C:\...\MW-44B\_Pumping\_Test.aqt

Date: 09/22/16

Time: 20:11:01

PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 44B

Test Date: 8/18/16

AQUIFER DATA

Saturated Thickness: 19.69 ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA

Pumping Wells

Observation Wells

Well Name	X (ft)	Y (ft)
44B	0	0

Well Name	X (ft)	Y (ft)
□ 44B	0	0

SOLUTION

Aquifer Model: Unconfined

Solution Method: Moench

T = 27.59 ft<sup>2</sup>/day

S = 0.0002211

Sy = 0.1007

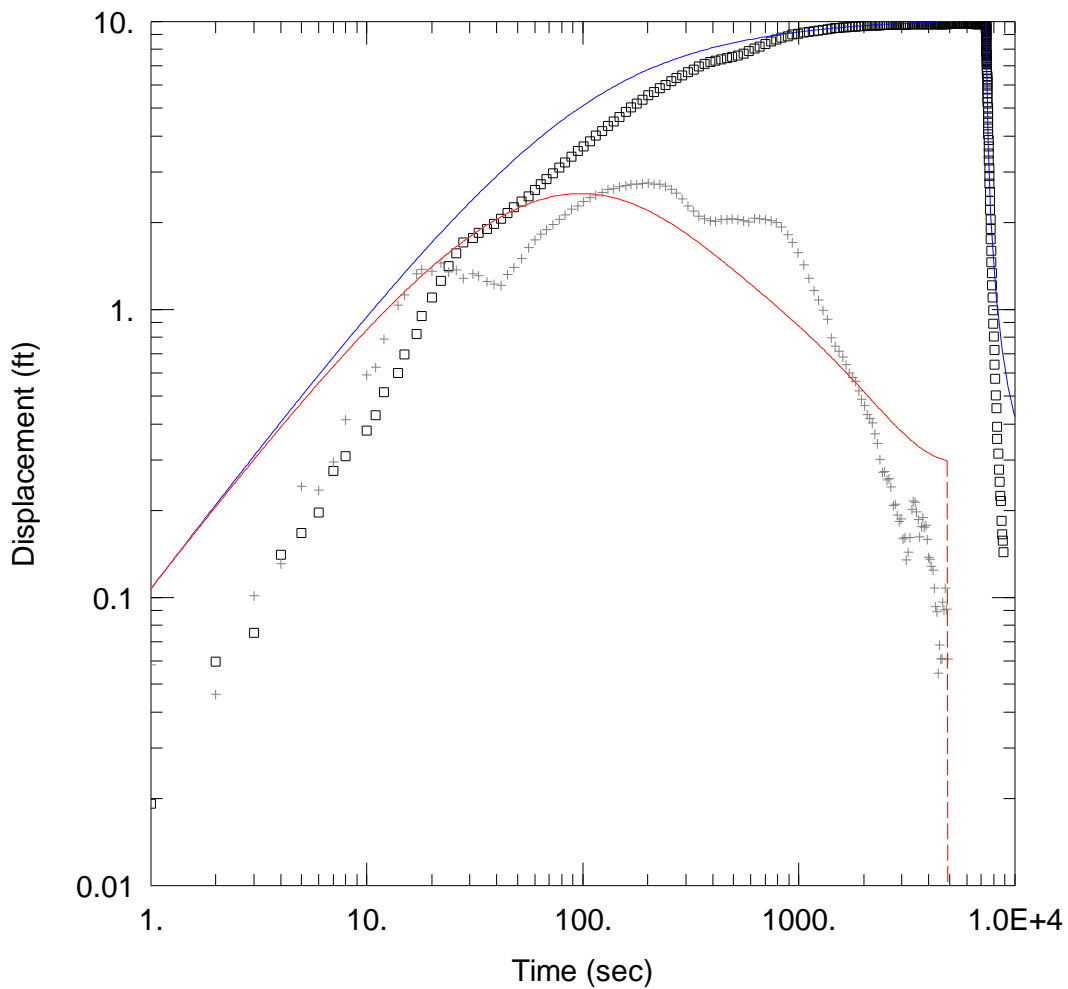
β = 0.0001612

Sw = 0.

r(w) = 0.25 ft

r(c) = 0.08612 ft

alpha = 1.0E+30 sec<sup>-1</sup>



### WELL TEST ANALYSIS

Data Set: C:\...\MW-46B\_Pumping\_Test.aqt

Date: 09/22/16

Time: 20:13:30

### PROJECT INFORMATION

Company: AECOM

Client: Basin Electric

Project: 60506860

Test Well: 43B

Test Date: 8/19/16

### AQUIFER DATA

Saturated Thickness: 17.1 ft

Anisotropy Ratio ( $K_z/K_r$ ): 1.

### WELL DATA

#### Pumping Wells

#### Observation Wells

Well Name	X (ft)	Y (ft)
46B	0	0

Well Name	X (ft)	Y (ft)
□ 46B	0	0

### SOLUTION

Aquifer Model: Unconfined

Solution Method: Moench

T = 13. ft<sup>2</sup>/day

S = 0.002151

Sy = 0.1007

$\beta$  = 0.0002138

Sw = 0.

r(w) = 0.25 ft

r(c) = 0.08612 ft

alpha = 1.0E+30 sec<sup>-1</sup>

# SOP NUMBER 18.0

## Aquifer Pumping Tests

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### Attachment

Attachment 18-1      Example of Pumping Test Data Form

## SOP NUMBER 18.0

## Aquifer Pumping Tests

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This Standard Operating Procedure (SOP) provides technical guidance and methods that will be used for performing aquifer pumping tests on groundwater monitoring wells. Pumping tests are conducted to determine aquifer transmissivity, hydraulic conductivity, storativity (or specific yield), anisotropy, and assess aquifer hydraulic connectedness. This SOP provides procedures for a step-discharge test to estimate the optimum pumping rate for the extraction well(s); a constant-rate pumping test (conducted at the rate selected from the step-discharge test); and a recovery test. The pumping tests will be run consecutively to reuse the test/monitoring equipment.

This SOP will provide descriptions of equipment, field procedures and documentation necessary to estimate the above hydraulic properties from step, constant rate, and recovery tests.

All activities will be conducted in accordance with the site-specific Health and Safety Plan (HASP).

### 1.0 EQUIPMENT AND MATERIALS

General equipment and materials used when performing pumping tests include:

- Boring logs, well construction and development records
- Pressure transducers of appropriate range and data logger
- Laptop computer for data logger
- Weather station with thermometer and barometer
- Electric water level meter
- Pumping test data forms (Attachment 18-1)
- Pump capable of pumping variable rates
- Associated pump control box and suspension cable or rope
- Generator or other appropriate power source for the pump
- Appropriately sized polyethylene discharge pipe, ball/gate valves, and check valve
- In-line flow meter with totalizer and flow measurements in gpm range
- Calibrated measuring volume and stopwatch
- Purge water collection system, as needed
- Tool box, hand tools (pliers, screwdrivers, cutting tools, duct tape etc.)
- Keys to well locks
- Decontamination equipment
- Appropriate health and safety equipment as required by the HASP
- Paper towels

## SOP NUMBER 18.0

## Aquifer Pumping Tests

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- Field log book

### 2.0 PUMPING TEST METHOD

An aquifer pumping test is a hydraulic well testing method in which groundwater is removed from an extraction (pumping) well to create a hydraulic stress on a water-bearing geologic unit, followed by monitoring of the changing hydraulic head in the pumping well and nearby observation wells. Pumping tests also commonly include a recovery phase where recharge is monitored in the test wells. Pumping tests are normally used to measure hydraulic conductivity as well as specific yield and other aquifer properties that are beyond the scope of less complicated slug tests.

Pumping tests may be performed on a single extraction well, however, only transmissivity and hydraulic conductivity values can be obtained from a single well test. The addition of one or more observation wells allows for the computation of specific yield or storativity of the aquifer and possibly for determination of anisotropy. Ideal testing conditions for determination of anisotropy include at least two pairs of in-line observation wells oriented perpendicularly to their radial offset from the extraction well. Constant-head or barrier boundaries within or close to the area affected by groundwater pumping can influence the drawdown and recovery observed in an aquifer pumping test, and may need to be addressed in the analysis.

Three types of aquifer tests may be conducted at each well selected for pumping. The three types of tests are step-drawdown, constant-rate, and recovery. Step-drawdown tests are conducted at successively greater discharges for relatively short periods to collect data that will be used to assess aquifer response at various pumping rates. These tests are usually conducted prior to constant-rate tests in order to estimate the maximum sustainable pumping rates.

Constant-rate tests involve pumping a well for a significant length of time at an approximately constant-rate. Constant rates are typically selected based on step-discharge testing results and/or well development information.

Recovery tests involve monitoring the recharge of groundwater to the test wells following the conclusion of the constant rate test. The following procedures will be implemented for conducting the aquifer tests.

### 2.1 PUMPING TEST PROCEDURES

#### 2.1.1 Pre-Test Data Recording

A Pumping Test Data Form will be completed for each well and each test as described in Section 3.

#### 2.1.2 Instrument Check

The flow meter, transducers, and electronic water level meters will be calibrated or checked to make sure they are working properly before commencement of the aquifer tests. Copies of instrument calibration documents will be filed with the records of the test data. The following checks and calibrations will be performed for pumping test equipment:

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## Aquifer Pumping Tests

---

- 1) Pressure transducers are rated to specific pressure heads. When selecting pressure transducers, verify pressure head ranges and associated maximum water column heights. Select an appropriate transducer for the range of water level change anticipated in the aquifer test (see operations manual). Record any pertinent information that may have a bearing on test quality.
- 2) The in-line flow meter will be checked on-site using a calibrated volume and stopwatch.
- 3) The accuracy of the transducers will be checked by moving the transducer up and down in the well a known vertical distance and reading the pressure (or feet of water) values recorded at the data logger. The known amount that the transducer is moved up or down should match the value displayed on the data logger. Also, the sign of the value on the data logger will be checked to verify the direction of transducer movement.
- 4) The water level meter will be checked to make sure that there are no lengths of cable cut off, and that the footages are accurate. The probes will be submerged into water to verify that the tone and/or indicator light are functional.

### 2.1.3 General Setup

- 1) Adequate fuel will be kept on-site to maintain a generator, if used for power, for the duration of the test, and all refuel times will be noted in field notebook.
- 2) The oil level in the generator (if used for power) will be checked periodically (at least twice daily).
- 3) Locate, open, and vent all wells to be tested on that day, unless prohibited by access restrictions. This will allow the water level in the test well to equilibrate with the prevailing barometric pressure. Equilibration of static water levels should be measured with the electronic water level indicator and/or pressure transducer as appropriate. The test wells should equilibrate for at least 30 minutes prior to beginning an aquifer test, and may require more time depending on aquifer characteristics.
- 4) Measure the static water level and total depth of the well to the nearest 0.01 foot with an electronic water level indicator before the test begins. The measuring point shall be the survey point where the surface elevation was measured; otherwise the point of reference will be the rim of the top of casing on the north side of the well. The well must not be recovering or receding as a result of sampling, development, pumping of nearby wells, or related activities. The test wells will be allowed to recover from these activities for a minimum of 24 hours before the start of the aquifer test.
- 5) Install pump and discharge lines in pumping well. The pump will be equipped with a check valve on the discharge line to prevent water in the discharge pipe from reentering the well once pumping ceases. Connect the discharge lines to purge containers, and pump control box to pump cable. Allow the water level in the well equilibrate to static conditions.
- 6) Measure the static water level and total depth in pumping well and observation wells from the surveyed reference point with an electric water level meter.
- 7) Install pressure transducers in pumping well and observation wells at a depth below the maximum drawdown expected during the test. The pumping well transducer may be installed



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## Aquifer Pumping Tests

inside a sounding tube to limit noise in the transducer readings from potential turbulence in the well. If a sounding tube is present, install pressure transducer approximately 6 inches from the bottom of the tube. Transducers are usually installed above the pump. Do not exceed the specified depth range of the transducer. The transducer should be secured so that it does not move during the test.

- 8) The transducers should equilibrate for 5 to 10 minutes before initiating the aquifer test.
- 9) The transducer cable will be connected to the data logger and the data logger turned on. The transducer probe pressure readout (reference level) will be set to zero while the probe is in the water. The depth interval from the static water level will be compared to the transducer probe readout on the data logger to verify that the transducer probe is working properly. The probe may then be referenced to the "appropriate datum" within the data logger. The appropriate datum may be the water level elevation as referenced to mean sea level or the depth of groundwater below the monitoring point.
- 10) A pre-run checkout test will be performed as specified in Section 2.1.2.
- 11) Care must be taken to ensure that the elevation of the transducer does not change once the test has begun. Readings from the transducer may be utilized to determine when the test should be stopped.
- 12) All water generated during the test shall be properly containerized or otherwise disposed of.
- 13) At the conclusion of any test, be sure to "stop", "save", and "download" all data from the transducers and/or data logger prior to removing a transducer from the well.
- 14) Remove the transducer and decontaminate all equipment.
- 15) Aquifer test data acquired from wells will be downloaded from the data logger onto a computer and backup copies created.

### 2.1.4 Conducting a Step-Discharge Test

A series of 2-hour step-discharge tests may be conducted at each selected test well at pre-selected rates based on well development records. The purpose of these tests is to estimate the optimum sustainable pumping rate for the constant-rate test, and to assess how specific capacity varies with increasing pumping rates. The step-discharge test will involve pumping the test well up to 4 successively increasing discharge rates. Each pumping rate (step) will continue for at least 2 hours, or until water levels generally stabilize.

- 1) Pumping rates for each step may be adjusted in the field.
- 2) Water-level data from select observation wells and the pumping well will be collected continuously on a logarithmic time schedule using a data logger. Water levels will be measured according to the following time schedule for each step:
  - a) 0-10 minutes (min): 1 second (sec) intervals
  - b) 10-15 min: 10 sec intervals
  - c) 15-100 min: 2 min intervals

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- d) 100-120 min: 5 min intervals
  - e) >120 min: 10 min intervals
- 3) The start time of the data logger will be synchronized with that of the pump. This can easily be done with hand signals or with the delayed start feature on the data logger. Ensure that the pump does not start before the data logger so that the initial water level,  $H_0$ , is recorded.
  - 4) Start the step test, recording the time the pump is started as test “zero time.”
  - 5) Monitor the pumping well discharge rate and maintain a constant flow rate by regulating the valve. Monitor the pumping rate approximately every 15 minutes during the step test. Record data on the Aquifer Test Data Forms, or in the field notebook.
  - 6) Water levels in the pumping well and observation wells will be measured and recorded to back up the electronic data collected by the pressure transducers and data logger. Manual water-level measurements of the pumping well will be made at 5-minute intervals during the first hour, at 15 minute intervals through the remainder of the test. Measurements at the observation wells may be made every 30 minutes. Measurements will be recorded on the Pumping Test Data Forms.
  - 7) At the end of a 2-hour interval (or sooner, if equilibrium conditions are reached early), the pump will be advanced to the next higher rate and the next step will begin. The water level measurement schedule will start over from time = 0.
  - 8) The data logger will be downloaded to a laptop computer after step- testing is completed.

### 2.1.5 Conducting a Constant-Rate Test

A constant-rate test will be conducted to estimate aquifer parameters. The constant-rate test will begin only after the aquifer has recovered to within 95% of pre-step test static conditions. Water levels will be measured at least 3 times, approximately 10-15 minutes apart, to verify that static conditions have been re-established.

The constant-rate test will involve pumping the aquifer at a constant discharge rate for a specified duration and measuring water level drawdown. The pumping rate at which the constant-rate test is conducted will be determined from the results of step-discharge test or from previous site knowledge. Barometric pressure will be recorded several times daily to document changes that may influence groundwater elevations. A detailed list of activities to be performed during the constant-rate test follows:

- 1) Prior to starting the constant-rate test, static water level will be measured in the observation wells and in the test well (to nearest 0.01 foot). Measurements will be made from a surveyed reference point on the well.
- 2) The pumping well and observation wells located within 100 feet of the pumping well will be monitored with a data logger. The data logger will be programmed to record data logarithmically from the test well and observation wells in which transducers have been placed on the following schedule:
  - a) 0-10 min: 1 sec intervals
  - b) 10-15 min: 10 sec intervals

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- c) 15-100 min: 2 min intervals
  - d) 100-1,000 min: 30 min intervals
  - e) 1,000-10,000 min: 200 min intervals
- 3) Water levels may be monitored manually with an electric water level meter at observation wells located within 300 feet of the pumping well at the following approximate intervals:
- a) 0-10 min: 1 min intervals
  - b) 10-100 min: 10 min intervals
  - c) 100-1,000 min: 100 min intervals
  - d) >1,000 min: 1,000 min intervals
- Observation wells greater than 300 feet from the test well may be monitored manually less frequently.
- 4) The start time of the data logger will be synchronized with that of the pump. This can easily be done with hand signals or with the delayed start feature on the data logger. Ensure that the pump does not start before the data logger so that the initial water level,  $H_0$ , is recorded.
  - 5) Start the constant-rate test, recording the time the pump is started as test “zero time.”
  - 6) If the initial discharge rate exceeds the predetermined discharge rate, reduce flow by partially closing the valve on the discharge pipe and note the time in the field notebook.
  - 7) Monitor the pumping well discharge rate and maintain a constant flow rate by regulating the valve. Monitor the pumping rate every 10 minutes during the first two hours. It is recommended to then monitor the pumping rate at 30-minute to 1-hour intervals, as appropriate, throughout the remainder of the test. Record data on the Pumping Test Data Forms, or in the field notebook.
  - 8) During pumping, plot the data (time versus drawdown) on log-log and/or semi-log graph paper or with computer software to assess the progress of the test and to determine when sufficient data have been collected.
  - 9) Water levels in the pumping well will be measured and recorded to back up the electronic data collected by the pressure transducers and data logger. Manual water-level measurements in the pumping well are recommended at approximately 5-minute intervals during the first hour, at 15 minute intervals from 1 to 4 hours, and at 1 hour intervals through the remainder of the test. Measurements will be recorded on the Aquifer Test Data Forms.
  - 10) Manual water-level measurements in the observation wells are recommended at 15 minute intervals during the first 4 hours, and then at 2 hour intervals through the conclusion of the test. Measurements will be recorded on the Pumping Test Data Forms.
  - 11) Samples of groundwater may be collected from the pumping well during the test.
  - 12) The data logger will be downloaded to a laptop computer after the constant-rate test is completed.

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There is generally no need to continue a test if water levels have sufficiently stabilized. This normally indicates that sufficient data have been collected. Additional useful information generally will not be gained by continued pumping. When the time versus drawdown data for the most distant observation well begins to plot as a straight line (constant slope) on the semi-log graph paper, the test can be terminated unless delayed yield conditions are anticipated.

Delayed yield conditions may be expected in unconfined aquifers. Pumping tests in unconfined aquifers should be continued until the effects of delayed yield are no longer present and a second Theis-type drawdown begins, if practical.

### 2.1.6 Conducting a Recovery Test

When the constant-rate test is terminated, the data logger cycle will be terminated and started again to record recovery data. The data logger will be programmed to collect recovery data in a logarithmic mode at the same intervals as those used for the constant-rate test. The start of the data recording will be timed precisely to the shutdown of the pump. The pump will be equipped with a check valve on the discharge line to prevent water in the discharge pipe from reentering the well once pumping ceases.

The recovery test will be terminated when water levels in the observation wells have recovered to within 90% of pre-test static levels or a specified duration. Recorded data will be downloaded from the data logger to a computer disk with file names that reflect the well name and test type (step-discharge, constant-rate, or recovery). Backup disks will also be created for contingency purposes.

## 2.2 PUMPING TEST DATA ANALYSIS

Data analyses and interpretations from the aquifer tests will be included in the investigation report. Drawdown and recovery data will be compiled and analyzed to:

- Determine hydraulic conductivity, transmissivity, and specific yield or storativity
- Estimate the radius of influence
- Assess whether any hydrogeologic boundaries were encountered (i.e., barrier or recharge boundaries)
- Assess whether any hydraulic communication between aquifer units exists
- Determine the nature and extent of aquifer anisotropy, if appropriate

All analyses will be performed using AQTESOLV<sup>®</sup> for Windows software (Duffield, 2007), Microsoft Excel<sup>®</sup>, or similar software. The aquifer test data will be analyzed using the appropriate analytical method(s). Methods may include, but are not limited to, Theis (1935) and Cooper-Jacob (1946). If the hydrogeologic conditions and pumping test data satisfy more than one method of analysis, then results will be presented for each method used.

If hydrogeologic conditions at the site prove to be more complicated than is appropriate for standard modeling methods, a more detailed numerical modeling approach may be undertaken. All numerical modeling results should contain an adequate description of the method or methods utilized.

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### 2.3 REPORTING

Aquifer test data analyses and interpretations will be presented in the investigation report. At a minimum, this portion of the report will include:

- A description of the procedures implemented during testing
- Interpretations of pumping test data
- Tables containing well completion information (e.g., well elevations and screened intervals) and water level data (e.g., initial and final pumping water levels)
- Tables summarizing estimated aquifer property values and water quality parameters collected during the pumping tests
- AQTESOLV<sup>®</sup> reports and graphs, as well as any manually produced graphs and calculations

### 3.0 DOCUMENTATION

Documentation of the observations and data acquired in the field will provide information on the activities conducted and also provide a permanent record of field activities. Observations and data will be recorded on a Pumping Test Data Form (Attachment 18-1) and in the field logbook.

#### 3.1 FIELD NOTES

The following aquifer test information will be recorded in a bound field logbook using indelible ink:

- Names of test personnel
- Weather conditions (including barometric pressure)
- Date and time of testing
- Test locations, specifying pumping wells and observation wells
- Start and stop time for each test or step conducted
- Equipment used
- Any other pertinent information that may have a bearing on test quality

#### 3.2 FIELD FORMS

A Pumping Test Data Form (Attachment 18-1) will be completed for each well and each test. The following information will be recorded:

- Date of test
- Aquifer test personnel
- Pumping/extraction or observation well identification number
- Location and elevation (if known) of the reference point from which water depth measurements are made (i.e., top of PVC well casing) for each well

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- Static water level
- Well depths, screened intervals, well casing diameters, borehole diameters, and filter pack intervals (from well construction logs)
- Aquifer or groundwater zone (lithology) being tested (from well construction logs)
- Start time of test or step
- End time of test or step
- Type of test (step test, constant-rate, or recovery). If a step test is run, specify which step in the series.
- Pumping rate
- Data logger test number
- Manual water level readings and associated times
- Data collected during the test will not be hand copied from the data logger, but will be downloaded onto a computer and backup copies created

### 4.0 REFERENCES

Cooper, H.H. and C.E. Jacob, 1946. A generalized graphical method for evaluating formation constants and summarizing well field history, *Am. Geophys. Union Trans.*, vol. 27, pp. 526-534.

Duffield, Glenn M. 1996. AQTESOLV for Windows™, User's Guide. HydroSOLVE, Inc.

Theis, C.V., 1935. The relation between the lowering of the piezometric surface and the rate and duration of discharge of a well using groundwater storage, *Am. Geophys. Union Trans.*, vol. 16, pp. 519-524.

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### Attachment 18-1 Example of Pumping Test Data Form





