

# Location Restrictions for Ash Landfill Expansion

Leland Olds Station
Basin Electric Power Cooperative
Stanton, Mercer County, North Dakota

AECOM Project Number: 60545172

November 20, 2017

# Prepared for:

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# **Executive Summary**

This Locations Restrictions Report for the Basin Electric Power Cooperative Leland Olds Station Ash Landfill Expansion has been prepared in accordance with the requirements specified in 40 Code of Federal Regulations (CFR) §257.60 through §257.64, which states the coal combustion residuals (CCR) Rule requirements for location restrictions<sup>1</sup>. More specifically, the location restrictions sections are as follows:

- §257.60 Placement Above the Uppermost Aquifer
- §257.61 Wetlands
- §257.62 Fault Areas
- §257.63 Seismic Impact Zones
- §257.64 Unstable Areas

Each requirement of the CCR Rule requires the owner or operator to obtain certification from a qualified professional engineer stating that the demonstration meets the requirements of the applicable CCR Rule citation prior to placing CCR in the new unit. The Leland Olds Station CCR Ash Landfill Expansion represents a lateral expansion and meets the location restriction requirements, as outlined by this report.

<sup>&</sup>lt;sup>1</sup> U.S. Environmental Protection Agency. (USEPA). (2015). *Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals From Electric Utilities; Final Rule*, 40 CFR §257. Federal Register, Volume 80, Subpart D, April 17, 2015

#### 1. Introduction

The purpose of the CCR Location Restrictions Report for the Basin Electric Power Cooperative Leland Olds Station Ash Landfill Expansion presented in this report is to document that the requirements in 40 Code of Federal Regulations (CFR) §257.60(a), §257.61(a), §257.62(a), §257.63(a), and §257.64(a) have been met to support certification for the existing active CCR units to remain in operation. These regulations require the owner or operator to obtain certification from a qualified professional engineer stating that the demonstration meets the specified aquifer separation, wetlands, fault distance, seismic acceleration, and unstable area requirements of the CCR Rule prior to placing CCR in the Ash Landfill Expansion area.

# 2. Facility and CCR Unit Description

Basin Electric Power Cooperative (BEPC) owns and operates the Leland Olds Station (LOS) located near Stanton, Mercer County, North Dakota. The station is located approximately four miles southeast of Stanton along the Missouri River (Figure 2.1-Site Location Map, Appendix A). The LOS is a lignite-based electric generating station with two units that generate a combined power of 669 megawatts. The plant first began commercial operation in June 1966.

As part of their continuing operations, BEPC is planning to expand their current operational ash landfill located at the former Glenharold Coal Mine. The location of the operational landfill and proposed Ash Landfill Expansion area are presented in Figure 2.2 (Site Map) included in Appendix A. The Glenharold Coal Mine was a Coal (Lignite) surface mine that ended operations in 1982. After mine closure, the land was reclaimed beginning with soil replacement in 1985. Reclamation operations were completed at the site in 1996, which included reestablishment of native grasslands, native woodlands, and permanent ponds for use as livestock water source and wildlife habitat.

The primary waste type that will be accepted by the proposed Ash Landfill Expansion will consist of CCR as defined by the United States Environmental Protection Agency (EPA), which includes bottom ash/boiler slag, fly ash and flue-gas desulfurization (FGD) waste, which is a synthetic form of gypsum (calcium sulfate). Minor amounts of other solid wastes generated at the power plant will also be accepted, as authorized in North Dakota Department of Health (NDDH) solid waste management facility permit SP-0143 (NDDH, 2017).

# 3. §257.60 Placement Above the Uppermost Aquifer

#### 3.1 §257.60(a) Citation

New CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must be constructed with a base that is located no less than 1.52 meters (five feet) above the upper limit of the uppermost aquifer, or must demonstrate that there will not be an intermittent, recurring, or sustained hydraulic connection between any portion of the base of the CCR unit and the uppermost aquifer due to normal fluctuations in groundwater elevations (including the seasonal high water table).

#### 3.2 Separation of Aquifer to Base of CCR Unit

The LOS Ash Landfill Expansion is subject to Section §257.60 of the CCR Rule concerning the placement of the base of the CCR unit above the uppermost aquifer<sup>2</sup>. As stated on page 21362 of the Preamble of the CCR Rule, the base is considered to be located at the bottom of the liner components:

...the minimum vertical separation be at least three to five feet from the base of the liner components. After additional research, EPA is finalizing a minimum buffer of five feet instead of two feet. EPA's research confirmed the commenter's claims. In addition, EPA determined that several states consider five feet between the base of the surface impoundment and the top of the uppermost aquifer to be the minimum distance that is protective of human health and the environment. These are California, Michigan, Nebraska, New York, West Virginia, and Wisconsin. The Agency has concluded from geographic and climatic spacing of these states that the hydrogeologic conditions within them encompass the range of conditions found in the United States. Therefore, EPA is finalizing a minimum buffer of five feet instead of two feet.

Site subsurface investigations have been performed at the site location in 2011 and 2016. In 2011, BEPC contracted Braun Intertec Corporation to perform a site subsurface investigation that included installation of five (5) monitoring wells. In 2016, a supplemental site subsurface investigation was performed by AECOM under contract with BEPC. As part of the supplemental site subsurface investigation, 10 geotechnical soil borings and 11 site characterization borings were completed by Terracon and Cascade drill crews, respectively. In addition, an extensive laboratory testing program was performed on samples recovered from the geotechnical soil borings. Upon boring completion, the 11 site characterization borings were converted into monitoring wells. Locations of the geotechnical borings and monitoring wells installed at the site are shown on Figure B-1 in Appendix B. Additional information regarding drilling and sampling procedures, well installation procedures, and laboratory test results from the 2016 subsurface investigation can be found in the "Supplemental Site Characterization Report (AECOM, 2017)."

Based on the conditions observed during the subsurface investigations performed in 2011 and 2016, the general encountered soil profile consisted of layers of mine spoils underlain by native hard cohesive soils with layers of lignite. Mine spoils within the proposed Ash Landfill Expansion footprint were encountered near ground surface (+1955.4 to +1891.1 feet NAVD29) to depths ranging between 44.5 and 100 feet below ground surface (+1871.9 to +1835.2 feet NAVD29). Laboratory results from the 2016 supplemental investigation indicate that the underlying mine spoil material and native hard cohesive soils are classified as high plasticity clay (USCS: CH). Boring logs containing soil information and depths explored from the 2016 supplemental investigation are presented in Appendix B.

A review of AECOM's drawings for proposed Ash Landfill Expansion base grades indicate that the minimum base liner elevation is +1886 feet NAVD29. The base liner system for the proposed expansion will consist of a 1-foot drainage layer underlain by a 60-mil High Density Polyethylene (HDPE) liner and 2

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<sup>&</sup>lt;sup>2</sup> Excerpt from the Preamble of the CCR Rule (Page 21362): EPA is revising the definition of "uppermost aquifer" to specify that the measurement of the upper limit of the aquifer must be made at a point nearest to the natural ground surface to which the aquifer rises during the wet season. This definition of "uppermost aquifer" will encompass large seasonal variations, and is more appropriate parameter than "seasonal high groundwater table" as suggested by several commenters and the proposed "natural water table" because it is more clearly defined

feet of compacted clay. When considering the base liner thickness, the minimum subgrade elevation of the proposed Ash Landfill Expansion is +1883 feet NAVD29. The permit drawing of the Ash Landfill Expansion base grades is included in Appendix C.

Of the monitoring wells that have been installed at the site, two (2) of them are within the proposed Ash Landfill Expansion footprint and six (6) are near the footprint perimeter. A quarterly sampling program has been implemented since the installation of the 2011 monitoring wells. In September 2016, water level measurements were performed in the 2011 and in some of the 2016 monitoring wells. The geologic cross sections in Appendix D show the base of the landfill and the piezometric surface derived from water level measurements taken during the September 2016 monitoring event. Groundwater measurements from September 2016 were compared to the minimum subgrade elevation of the proposed Ash Landfill Expansion and are presented in Table 1. In addition, the Ash Landfill Expansion minimum subgrade elevation was also compared to groundwater levels observed since 2011 in monitoring wells within and near the proposed Ash Landfill Expansion footprint and are presented in Figure 3.2 included in Appendix E.

Table 1. Groundwater Elevation Data from September 2016

Monitoring Well	Groundwater Elevation [NAVD29, ft]	Subgrade Elevation [NAVD29, ft]	Separation Distance [ft]
MW-2011-1 <sup>(1)</sup>	1847.4	1883.0 <sup>(2)</sup>	35.6
MW-2011-2	1844.9	1883.0 <sup>(2)</sup>	38.1
MW-2011-3	1844.1	1883.0 <sup>(2)</sup>	38.9
MW-2011-4	1843.8	1883.0 <sup>(2)</sup>	39.3
MW-2011-5	1851.0	1883.0 <sup>(2)</sup>	32.0
MW-2016-1 <sup>(1)</sup>	1836.8	1883.0 <sup>(2)</sup>	46.2
MW-2016-2 <sup>(1)</sup>	1836.0	1883.0 <sup>(2)</sup>	47.0
MW-2016-3	1839.8	1883.0 <sup>(2)</sup>	43.2
MW-2016-4	1843.0	1883.0 <sup>(2)</sup>	40.0
MW-2016-5	1845.3	1883.0 <sup>(2)</sup>	37.7
MW-2016-6	1847.0	1883.0 <sup>(2)</sup>	36.0
MW-2016-7 <sup>(1)</sup>	1862.8	1883.0 <sup>(2)</sup>	20.2
MW-2016-8 <sup>(1)</sup>	1846.2	1883.0 <sup>(2)</sup>	36.8

Note: (1) The locations of these wells are not within or near the proposed Ash Landfill Expansion footprint (2) Lowest elevation based on AECOM design drawings. Subgrade elevation at actual well location may

be greater than +1883 NAVD29 feet; therefore greater separation distance will exist.

Source: Supplemental Site Characterization Report by AECOM

In summary, the comparison of the minimum subgrade elevation of the proposed LOS Ash Landfill Expansion to the unconfined uppermost aquifer indicates a greater than 5 feet separation exists between the upper limit of the uppermost aquifer and the base of the CCR surface impoundment. In addition, the proposed expansion will have an impermeable HDPE liner and low permeable clay liner that will limit the hydraulic interaction between the landfilled material and the in-place site soils. Therefore, the proposed LOS Ash Landfill Expansion meets the requirements of §257.60(a).

# 3.3 Federal Requirement [40 CFR § 257.60]

Certification Statement 40 CFR § 257.60 – Placement of the Lateral Expansion of an Existing CCR Surface Impoundment Above the Uppermost Aquifer

#### **CCR Unit: Leland Olds Station Ash Landfill Expansion**

I, John Cannon, being a Registered Professional Engineer in good standing in the State of North Dakota, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, for the above referenced CCR Units, that the information contained in the Location Restrictions Report dated November 20, 2017 meets the requirements of 40 CFR § 257.60.

John Cannon	
Printed Name	
November 20, 2017	
Date	_



# 4. §257.61 Wetlands

#### 4.1 §257.61(a) Wetlands Citation

New CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must not be located in wetlands, as defined in §232.2 of this chapter, unless the owner or operator demonstrates by the dates specified in paragraph (c) of this section that the CCR unit meets the requirements of paragraphs (a)(1) through (5) of this section.

- (1) Where applicable under section 404 of the Clean Water Act or applicable state wetlands laws, a clear and objective rebuttal of the presumption that an alternative to the CCR unit is reasonably available that does not involve wetlands.
- (2) The construction and operation of the CCR unit will not cause or contribute to any of the following:
  - (i) A violation of any applicable state or federal water quality standard;
  - (ii) A violation of any applicable toxic effluent standard or prohibition under section 307 of the Clean Water Act:
  - (iii) Jeopardize the continued existence of endangered or threatened species or result in the destruction or adverse modification of a critical habitat, protected under the Endangered Species Act of 1973; and
  - (iv) A violation of any requirement under the Marine Protection, Research, and Sanctuaries Act of 1972 for the protection of a marine sanctuary.
- (3) The CCR unit will not cause or contribute to significant degradation of wetlands by addressing all of the following factors:
  - (i) Erosion, stability, and migration potential of native wetland soils, muds and deposits used to support the CCR unit;
  - (ii) Erosion, stability, and migration potential of dredged and fill materials used to support the CCR unit:
  - (iii) The volume and chemical nature of the CCR;
  - (iv) Impacts on fish, wildlife, and other aquatic resources and their habitat from release of CCR;
  - (v) The potential effects of catastrophic release of CCR to the wetland and the resulting impacts on the environment; and
  - (vi) Any additional factors, as necessary, to demonstrate that ecological resources in the wetland are sufficiently protected.
- (4) To the extent required under section 404 of the Clean Water Act or applicable state wetlands laws, steps have been taken to attempt to achieve no net loss of wetlands (as defined by acreage and function) by first avoiding impacts to wetlands to the maximum extent reasonable as required by paragraphs (a)(1) through (3) of this section, then minimizing unavoidable impacts to the maximum extent reasonable, and finally offsetting remaining unavoidable wetland impacts through all appropriate and reasonable compensatory mitigation actions (e.g., restoration of existing degraded wetlands or creation of man-made wetlands); and
- (5) Sufficient information is available to make a reasoned determination with respect to the demonstrations in paragraphs(a)(1) through (4) of this section.

#### 4.2 Wetlands Study

BEPC contracted AECOM to perform an environmental and wetland delineation within the proposed Ash Landfill Expansion in Mercer County. The purpose of the delineation was to provide a summary of available desktop data and wetland delineations conducted on August 19, 2016 and an evaluation of potential waters of the United States (WOTUS). In addition, a desktop analysis and literature search were also performed to identify federally listed species of concern with potential to occur within the site area. The executive summary and figures from the AECOM report titled, "Environmental and Wetland Delineation Report for LOS Landfill Expansion" are included in Appendix F.

A desktop analysis and literature search indicated that seven threatened and endangered (T&E) species of concern with potential to occur within the site area. As part of the analysis, each species was assigned a "determination affect." The assigned determinations for the species identified ranged from "no effect" to "may effect, but not likely to occur."

For the wetlands study, four wetlands were delineated within the site area by AECOM. After evaluation, AECOM concluded that the wetlands appeared to be non-relatively permanent waters (non-RPW) that are formed by geomorphic position, are isolated from jurisdictional waters, and appear without significant nexus. In summary, the delineated wetlands were formed following mine land reclamation when soils settled or as a result of road construction.

# 4.3 Federal Requirement [40 CFR §257.61]

Certification Statement 40 CFR § 257.61 – Location of the Lateral Expansion of an Existing CCR Surface Impoundment in Wetlands

#### **CCR Unit: Leland Olds Station Ash Landfill Expansion**

I, John Cannon, being a Registered Professional Engineer in good standing in the State of North Dakota, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR Unit, that the demonstration that the CCR Unit is not located in wetlands, as included in the Location Restrictions Report dated November 20, 2017 meets the requirements of 40 CFR §257.61.

John Cannon	
Printed Name	
November 20, 2017	
Date	



# 5. §257.62 Fault Areas

# 5.1 §257.62(a) Citation

New CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must not be located within 60 meters (200 feet) of the outermost damage zone of a fault that has had displacement in Holocene time unless the owner or operator demonstrates by the dates specified in paragraph (c) of this section that an alternative setback distance of less than 60 meters (200 feet) will prevent damage to the structural integrity of the CCR unit.

#### 5.2 Distance to Holocene Faults

As stated in the CCR Rule, a CCR unit is considered to be in a fault area if it's within 200 feet of the outermost damage zone of a fault that has seen displacement during the Holocene epoch, or within the last 12,000 years. As stated on page 21366 of the Preamble of the CCR Rule:

To investigate active faults, EPA expects owners and operators of CCR units to follow standard engineering and geologic practices. Technical considerations include:

- (1) A geologic reconnaissance of the site to determine the location of active faults. Such a reconnaissance would include utilizing the seismic analysis maps and tools (Quaternary fault maps, earthquake probability maps) of the United States Geological Survey (USGS) Earthquake Hazards Program (http://earthquake.usgs.gov/hazards/apps/); and
- (2) A site fault characterization within 1000 meters of a site to determine whether it is within 60 meters of an active fault. Such characterizations would include subsurface exploration, including drilling or trenching, to locate any fault zones and evidence of faulting, trenching perpendicular to any faults or lineaments found within 60 meters of the site, and determination of the age of any displacements.

AECOM researched the United States Geological Survey (USGS) Geographic Information Systems (GIS) Database for known Holocene faults. Since the Holocene faults are defined within the Quaternary Period, which is the last 2.6 million years to present, a figure presenting a USGS map showing Quaternary faults in proximity to the LOS Ash Landfill Expansion is provided in Appendix G. In addition, the North Dakota Geologic Survey has produced a geologic map of Mercer and Oliver Counties (Appendix G).

Findings from the research performed did not indicate the presence of active faults within 1000 meters of the CCR units. Therefore, no further action (e.g., a site characterization) was performed.

Based on the results of the evaluation described herein, the LOS Ash Landfill Expansion is not located within 60 meters (200 feet) of the outermost damage zone of a fault that has seen displacement during Holocene time.

# 5.3 Federal Requirement [40 CFR §257.62]

Certification Statement 40 CFR § 257.62 – Location of the Lateral Expansion of an Existing CCR Surface Impoundment within 60 Meters of a Fault Area

#### **CCR Unit: Leland Olds Station Ash Landfill Expansion**

I, John Cannon, being a Registered Professional Engineer in good standing in the State of North Dakota, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR Unit, that the demonstration regarding that the CCR Unit is not located within 60 meters (200 feet) of the outermost damage zone of a fault that has had a displacement in Holocene time, as included in the Location Restrictions Report dated November20, 2017, meets the requirements of 40 CFR §257.62.

ohn Cannon
Printed Name
lovember 20, 2017
Date



# 6. §257.63 Seismic Impact Zones

#### 6.1 §257.63(a) Citation

CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must not be located in seismic impact zones unless the owner or operator demonstrates by the dates specified in paragraph (c) of this section that all structural components including liners, leachate collection and removal systems, and surface water control systems, are designed to resist the maximum horizontal acceleration in lithified earth material for the site.

#### 6.2 Seismic Impact Zones

As stated on page 21471, the CCR Rule defines a *seismic impact zone* as "an area having a 2% or greater probability that the maximum expected horizontal acceleration, expressed as a percentage of the earth's gravitational pull (g), will exceed 0.10 g in 50 years". The USGS produced a national map of the two-percent probability of exceedance in 50 years map of peak ground acceleration (Figure 6.1). The LOS Ash Landfill Expansion is in the area of less than 0.1g, and the USGS provides a method to calculate the PGA of specific sites.

The United States Geologic Survey National Seismic Hazards Mapping Project, PSHA Deaggregation program, 2008 version was used to find the PGA for the site location. The results of the Deaggregation program are found in Figure 6.2. The results for the Ash Landfill Expansion are presented in Table 2.

**Table 2. Peak Ground Acceleration at Leland Olds Station** 

Location	Longitude	Latitude	Peak Ground Acceleration
Leland Olds Station	-101.3714	47.2469	0.022 g

The PSHA deaggregation program reports all PGA results for lithified earth materials, which corresponds to seismic site classes A, B, or C. The PGA is below 0.1 g and meets the criteria. Therefore, the LOS Ash Landfill Expansion is not located in a seismic impact zone.

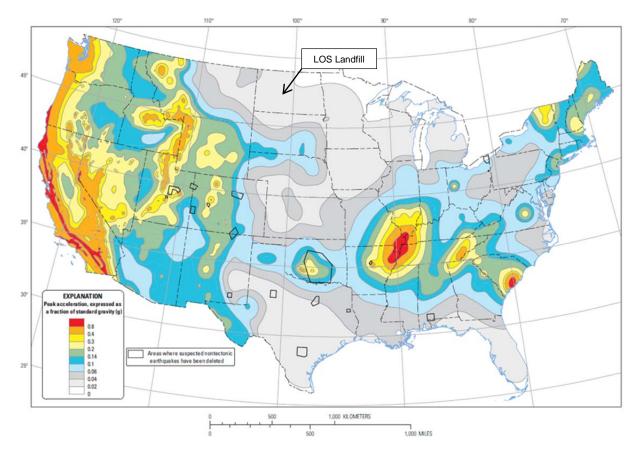


Figure 6.1 Two-Percent Probability of Exceedance in 50 Years Map of Peak Ground Acceleration

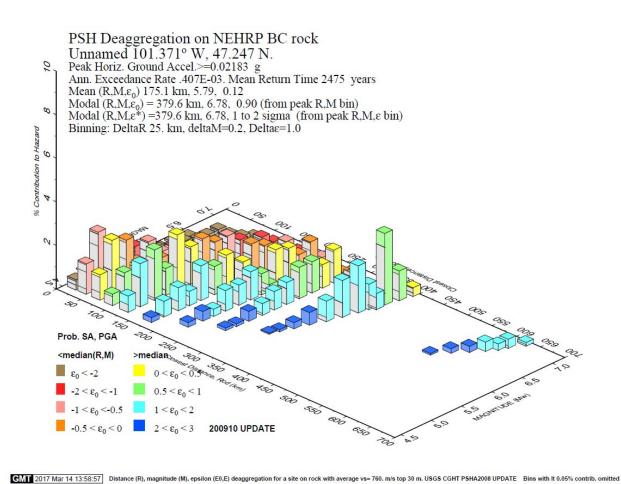


Figure 6.2 The PSHA Deaggregation Program Result (PGA=0.022 g)

# 6.3 Federal Requirement [40 CFR §257.63]

Certification Statement 40 CFR § 257.63 – Location of the Lateral Expansion of an Existing CCR Surface Impoundment in a Seismic Impact Zone

#### **CCR Unit: Leland Olds Station Ash Landfill Expansion**

I, John Cannon, being a Registered Professional Engineer in good standing in the State of North Dakota, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR Unit, that the demonstration that the CCR Unit is not located in a seismic impact zone, as included in the Location Restrictions Report dated November 20, 2017, meets the requirements of 40 CFR §257.63.

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ohn Cannon
Printed Name
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#### 7. §257.64 Unstable Areas

#### 7.1 §257.64(a)-(b) Citation

- (a) An existing or new CCR landfill, existing or new CCR surface impoundment, or any lateral expansion of a CCR unit must not be located in an unstable area unless the owner or operator demonstrates by the dates specified in paragraph (d) of this section that recognized and generally accepted good engineering practices have been incorporated into the design of the CCR unit to ensure that the integrity of the structural components of the CCR unit will not be disrupted.
- (b) The owner or operator must consider all of the following factors, at a minimum, when determining whether an area is unstable:
  - (1) On-site or local soil conditions that may result in significant differential settling;
  - (2) On-site or local geologic or geomorphologic features; and
  - (3) On-site or local human-made features or events (both surface and subsurface).

#### 7.2 Unstable Areas, Settlement, Collapsible Soils

All CCR landfill lateral expansions are subject to the unstable areas location restriction.

Due to the site history, a geotechnical subsurface investigation was completed as part of the design process. The subsurface investigation included drilling 10 geotechnical soil borings within and near the proposed Ash Landfill Expansion footprint. After completion of drilling activities, a laboratory testing program that included direct shear, triaxial shear, and consolidation testing was completed on select recovered samples. Results from geotechnical drilling and laboratory testing were used to analyze the subsurface foundation soils for settlement and overall stability of base grades based on the proposed Ash Landfill Expansion design. Results from the material tests and the methods used for the geotechnical analysis can be found in the "Supplemental Site Characterization Report (AECOM, 2017b)."

Results from the geotechnical analysis indicated that settlement will occur as the Ash Landfill Expansion is constructed. Although settlement will occur, the anticipated amount will be within tolerance of the landfill design. In addition, results from the stability analysis indicate that proposed base grades of inplace site soils should remain stable during construction. Based on the soils encountered and the geotechnical analysis performed, the expansion is considered to be stable based on the factors outlined in §257.64(b).

#### 7.3 Federal Requirement [40 CFR §257.64]

Certification Statement 40 CFR § 257.63 – Location of the Lateral Expansion of an Existing CCR Surface Impoundment in an Unstable Area

#### **CCR Unit: Leland Olds Station Ash Landfill Expansion**

I, John Cannon, being a Registered Professional Engineer in good standing in the State of North Dakota, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR Unit, that the demonstration that the CCR Unit is not located in an unstable area, as included in the Location Restrictions Report, November 20, 2017, meets the requirements of 40 CFR §257.64..

John Cannon
Printed Name
November 20, 2017
Date



#### 8. Limitations

In preparing this report, AECOM has reviewed background information, design basis, and other additional data furnished to AECOM by BEPC, as well as relevant available information from previous and current investigations performed by AECOM and others at the site. AECOM has relied on this information as furnished without independent verification, and is not responsible for the accuracy or completeness of this information. AECOM shall not be held responsible for conditions or consequences arising from relevant facts that were concealed, withheld, or not fully disclosed by BEPC at the time this report was prepared. In addition, the conclusions expressed in this report are subject to certain conditions and assumptions, which are noted in this report and below. Any party reviewing this report must carefully review and consider all such conditions and assumptions.

The conclusions made in this report are based on the assumption that the subsurface soil, rock, and groundwater conditions at the site do not deviate appreciably from those conditions disclosed in the site-specific exploratory borings. The conclusions in this report are also based on AECOM's understanding of current plant operations, maintenance, storm water handling, and ash handling procedures at the station based on information provided by BEPC. The passage of time may result in changes in site conditions and variations, technology, economic conditions, and regulatory provisions, all which could render the report inaccurate.

This report was prepared by AECOM in accordance with generally accepted engineering and scientific practice in effect at the time of AECOM's assessment of the subject property. This report was prepared pursuant to an agreement between AECOM and BEPC and is for the exclusive use of the BEPC. Any reliance on this report shall be at the user's sole risk.

#### 9. References

NDDH (2017). Leland Olds Station Ash Landfill Expansion—Phase 6 Special Waste Landfill Permit SP-143. Prepared for Basin Electric Power Cooperative.

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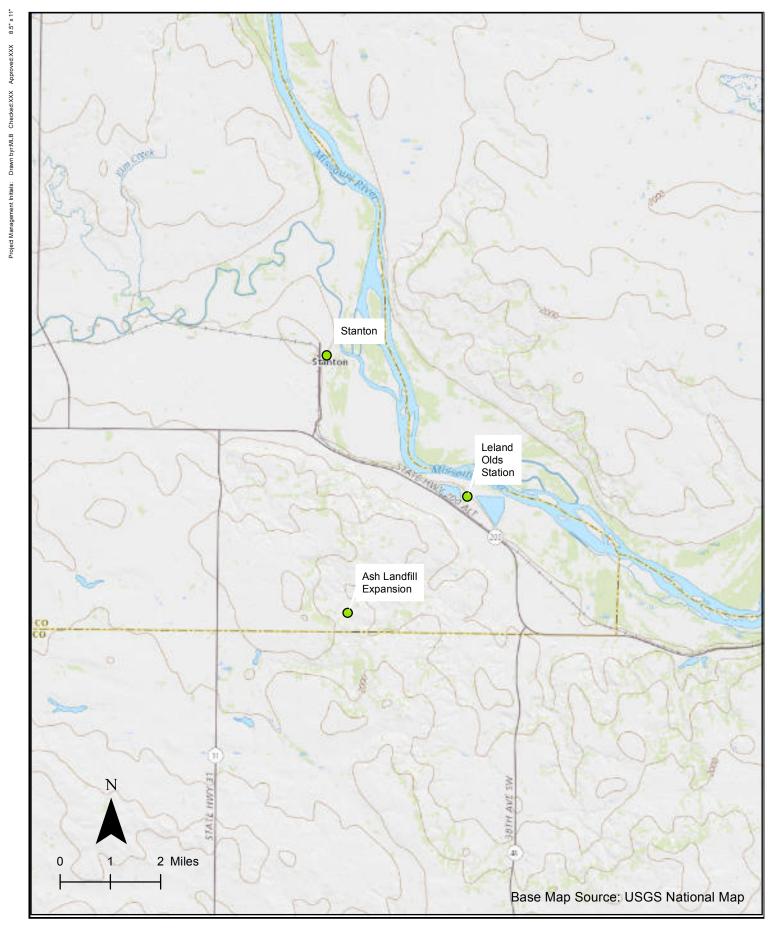
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# **Appendix A – Site Maps**



Location Restrictions Report Basin Electric Power Cooperative Project No.: 60545172 Site Location Map
Ash Landfill Expansion
Leland Olds Station
Mercer County, North Dakota

**AECOM** 

FIGURE 1

558 North Main Street
Oshkosh, WI 54901
920.235.0270
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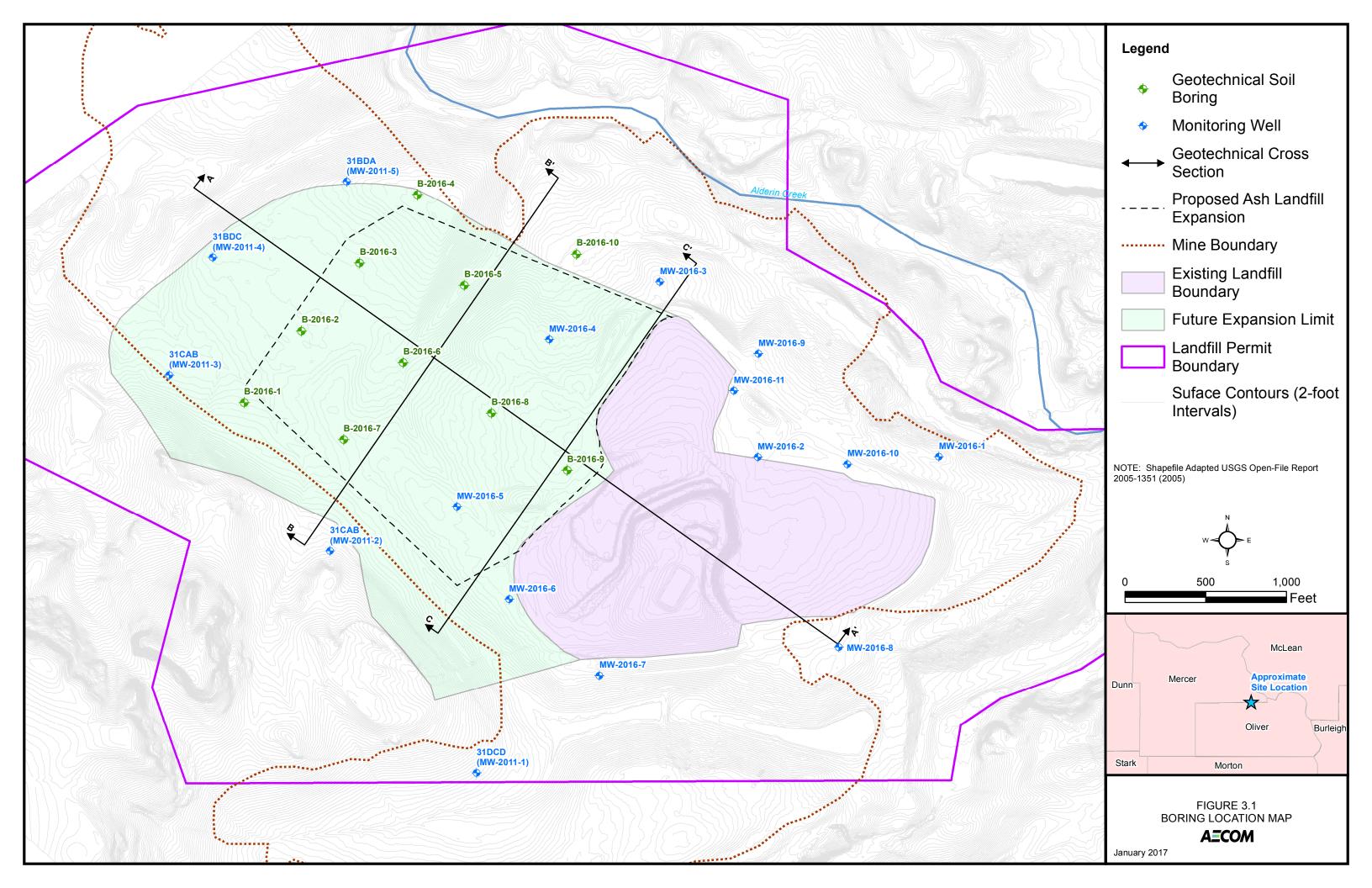
SITE MAP
ASH LANDFILL EXPANSION
BASIN ELECTRIC POWER COOPERATIVE
LELOND OLDS STATION
MERCER COUNTY, NORTH DAKOTA

PROJECT 60545172

FIGURE NUMBER

2.2

# **Appendix B – Boring Location Map, 2016 Boring Logs/Well Diagrams**



CLIENT LOG OF BORING NUMBER B-2016-01 **Basin Electric Power Cooperative AECOM** PROJECT NAME ARCHITECT-ENGINEER LOS ASH Landfill Expansion **AECOM** -O-UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT) SAMPLE TYPE DESCRIPTION OF MATERIAL  $\times$  $\overline{\Delta}$ UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 30 STANDARD  $\otimes$ PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,913.2 FILL - SANDY SILT - little clay - trace plant roots - brown -SS medium dense (ML) FILL - CLAY - little to trace fine sand and silt - gray - very HS stiff to hard (CH) <del>5.0</del> SS HS <del>10.0</del> **,**O 3 SS HS <del>15.0</del> 4 ST 5 SS HS 20.0 6 SS HS **25.0** FILL - SANDY CLAY - gray - stiff (CH) ST 8 SS 29.0 FILL - CLAY - little to trace silt - gray - hard (CH) <del>30.0</del> CURRENT.GDT FILL - CLAY - trace hard clay nodules - intermitent sand 9 SS seams - gray - stiff to hard (CH) HS <del>35.0</del> DATATEMPLATE 10 ST 11 SS HS <del>40.0</del> FILL - CLAY - little to trace sand and silt - gray to dark gray -12 SS hard to very stiff (CH) EXPANSION.GPJ HS 45.0 13 ST trace coal in sample 13 14 SS LOS LANDFILL HS <del>50.0</del> 15 SS trace gravel in sample 15 HS 60494667 **55.0** FILL - CLAY - little to trace sand and silt - trace gravel - gray - hard (CH) 16 ST **\***+ AECOM LOG WSAMPLENOTES 17 SS HS 60.0 \* Calibrated Penetrometer ... continued AECOM JOB NO. **60494667** SHEET NO. The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual.

CLIENT LOG OF BORING NUMBER B-2016-01 **Basin Electric Power Cooperative AECOM** PROJECT NAME ARCHITECT-ENGINEER **LOS ASH Landfill Expansion AECOM** -O-UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota 3 PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT) SAMPLE TYPE  $\times$  $-\!\!\!\Delta$ DESCRIPTION OF MATERIAL UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 50 20 30 STANDARD  $\otimes$ PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,913.2 (Continued) FILL - CLAY - little to trace sand and silt - trace gravel - gray - hard (CH) HS 65.0 53/6" -⊗ ST 19 \*\*\* 20 SS 20A SS FILL - SILTY GRAVEL - light gray - dry - extremely dense (GM) HS FILL - CLAY - little to trace silt - gray - very stiff to hard (CH) <del>70.0</del> **€**3 21 SS FILL - CLAY - little silt - trace fine sand - gray - stiff to very stiff (CH) HS <del>75.0</del> SENTINEL BUTTE FORMATION - CLAY - trace silt - bluish 80 ⊗ gray to gray - hard (CH) Ō 23 SS Shelby tube refusal at 75.5 feet HS 63 ⊗ + 24 SS End of Boring \* Calibrated Penetrometer Boring advanced to 79.5 feet with 3.25-inch hollow-stem Standard Penetration Test performed with automatic hammer WSAMPLENOTES 60494667 LOS LANDFILL EXPANSION.GPJ DATATEMPLATE CURRENT.GDT 1/13/17 Boring backfilled with chipped bentonite The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual. NORTHING BORING STARTED AECOM OFFICE Oshkosh, Wisconsin 577904.547 AECOM LOG BORING COMPLETED 7/25/16 ENTERED BY MLB **EASTING** 1782313.198 RIG/FOREMAN D-90/MR (Terracon) APP'D BY WL AECOM JOB NO. **60494667** Not Encountered WD / cave in @ 75'

CLIENT LOG OF BORING NUMBER B-2016-02 **Basin Electric Power Cooperative AECOM** PROJECT NAME ARCHITECT-ENGINEER LOS ASH Landfill Expansion **AECOM** -O-UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota PLASTIC WATER LIQUID **ELEVATION(FT** SAMPLE DISTANCE LIMIT % CONTENT % LIMIT % DEPTH(FT) SAMPLE TYPE DESCRIPTION OF MATERIAL  $\times$  $\overline{\Delta}$ UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 30 STANDARD  $\otimes$ PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,915.7 FILL - SILTY CLAY - trace coarse sand - dark brown SS (CL-ML) HS 5.0 FILL - CLAY - trace silt, sand, and coal - gray - very stiff to (I) 2 SS hard (CH) HS <del>10.0</del> ф 3 SS HS <del>15.0</del> + 4 ST **\***} 5 SS d<sup>14</sup> HS 20.0 6 SS HS **25.0** 7 ST 8 SS HS <del>30.0</del> CURRENT.GDT **,**O 9 SS HS <del>35.0</del> FILL - CLAY - some to little sand and silt - trace coal - gray -DATATEMPLATE hard (CH) 10 ST 11 SS HS <del>40.0</del> 12 SS EXPANSION.GPJ HS 45.0 13 ST 14 SS LOS LANDFILL HS <del>50.0</del> FILL - CLAY - little silt - trace sand and coal - grayish brown **\_**O 15 SS - very stiff to hard (CH) HS 60494667 **55.0** FILL - CLAY - little sand, silt, - brown - hard (CH) \*\* 16 ST AECOM LOG WSAMPLENOTES 17 SS HS 60.0 FILL - CLAY - trace silt - gray to dark gray - hard (CH) ... continued \* Calibrated Penetrometer AECOM JOB NO. **60494667** SHEET NO. The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual.

CLIENT LOG OF BORING NUMBER B-2016-02 **Basin Electric Power Cooperative AECOM** PROJECT NAME ARCHITECT-ENGINEER **LOS ASH Landfill Expansion AECOM** -O UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota 3 PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT) SAMPLE TYPE  $\times$  $-\!\!\!\Delta$ DESCRIPTION OF MATERIAL UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 50 20 30 STANDARD PENETRATION BLOWS/(FT)  $\otimes$ SURFACE ELEVATION +1,915.7 (Continued) FILL - CLAY - trace silt - gray to dark gray - hard (CH) HS 65.0 FILL - CLAY - little silt - dark gray to brown - very stiff to hard (CH) ST 19 20 SS trace coal in sample 19 HS 70.0 70.5 LIGNITE - dark brown to black SENTINEL BUTTE FORMATION - CLAY - little to trace silt -HS bluish gray to gray - hard (CH) <del>75.0</del> 22 SS Ö HS **5**4 + 23 SS End of Boring \* Calibrated Penetrometer Boring advanced to 79.5 feet with 3.25-inch hollow-stem Standard Penetration Test performed with automatic hammer Boring backfilled with chipped bentonite The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual. NORTHING BORING STARTED AECOM OFFICE Oshkosh, Wisconsin 578347.815 BORING COMPLETED 7/22/16 ENTERED BY MLB **EASTING** 1782669.572 APP'D BY RIG/FOREMAN
D-90/MR (Terracon) AECOM JOB NO. **60494667** WL

WSAMPLENOTES 60494667 LOS LANDFILL EXPANSION.GPJ DATATEMPLATE CURRENT.GDT 1/13/17

AECOM LOG

Not Encountered WD / cave in @ 41'

CLIENT LOG OF BORING NUMBER B-2016-03 **Basin Electric Power Cooperative AECOM** PROJECT NAME ARCHITECT-ENGINEER LOS ASH Landfill Expansion **AECOM** -O-UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT) SAMPLE TYPE DESCRIPTION OF MATERIAL  $\times$  $-\!\!\Delta$ UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 30 50 STANDARD  $\otimes$ PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,918.7 10 FILL - SANDY SILT - trace clay and plant roots - brown - dry SS (ML) HS FILL - CLAY - trace sand and silt - brownish gray to dark <del>5.0</del> brown - very stiff (CH) 2 SS HS 10.0 ST **6** ⊗ 4 SS HS . ⊗ <del>15.0</del> 5 SS HS 20.0 6 ST FILL - CLAY - trace to little silt - intemittent soft clay layers -7 SS  $\overline{\bigcirc}$ gray - soft to hard (CH) HS \* **25.0** 0 8 SS trace coal in sample 8 HS FILL - CLAY - trace sand and silt - gray - hard (CH) <del>30.0</del> CURRENT.GDT 9 ST <del>\*</del> 10 SS HS FILL - CLAY - little to trace silt and fine sand - brownish gray <del>35.0</del> 11 SS DATATEMPLATE to gray - very stiff to hard (CH) HS 40.0 12 ST EXPANSION.GPJ 13 SS HS <del>45.0</del> 14 SS HS LOS LANDFILL <del>50.0</del> 15 ST 16 ss 60494667 HS **55.0** FILL - fine to coarse SILTY GRAVEL - light gray - dense AECOM LOG WSAMPLENOTES FILL - CLAY - little sand and silt - seams of lignite, sand, HS and silt - brown to gray - very stiff to hard (CH) 60.0 ... continued \* Calibrated Penetrometer AECOM JOB NO. **60494667** SHEET NO. The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual.

CLIENT LOG OF BORING NUMBER B-2016-03 **Basin Electric Power Cooperative AECOM** PROJECT NAME ARCHITECT-ENGINEER **LOS ASH Landfill Expansion AECOM** -O-UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT)  $\times$  $-\!\!\Delta$ SAMPLE TYPE DESCRIPTION OF MATERIAL UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 50 20 30 STANDARD ⊗ 10 PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,918.7 (Continued) FILL - CLAY - little sand and silt - seams of lignite, sand, 18 ST Φ and silt - brown to gray - very stiff to hard (CH) SS め 19 HS 65.0 20 SS HS <del>70.0</del> 21 ST X 14 ⊗ trace coal in sample 21 22 SS HS <del>75.0</del> 23 SS LIGNITE - black SENTINEL BUTTE FORMATION - SANDY CLAY - trace HS coal - grayish brown - very stiff (CH) 80.0 24 ST Shelby tube refusal at 81.5 feet 5 ⊗ 25 SS 0 SENTINEL BUTTE FORMATION - CLAY - trace silt - bluish 83.5 gray to gray - hard (CH) \* Calibrated Penetrometer End of Boring Boring advanced to 80.0 feet with 3.25-inch hollow-stem WSAMPLENOTES 60494667 LOS LANDFILL EXPANSION.GPJ DATATEMPLATE CURRENT.GDT 1/13/17 auger Standard Penetration Test performed with automatic Boring backfilled with chipped bentonite The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual. NORTHING BORING STARTED AECOM OFFICE Oshkosh, Wisconsin 578768.181 AECOM LOG BORING COMPLETED 7/22/16 ENTERED BY MLB **EASTING** 1783029.47 RIG/FOREMAN D-90/MR (Terracon) APP'D BY WL AECOM JOB NO. **60494667** Not Encountered WD / cave in @ 74'

LOG OF BORING NUMBER CLIENT B-2016-04 **Basin Electric Power Cooperative AECOM** PROJECT NAME ARCHITECT-ENGINEER LOS ASH Landfill Expansion **AECOM** -O-UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.2 Stanton, Mercer County, North Dakota PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT) SAMPLE TYPE DESCRIPTION OF MATERIAL  $\times$  $-\!\!\Delta$ UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 30 50 STANDARD  $\otimes$ PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,943.7 190 FILL - SILTY CLAY - trace gravel and plant roots - dark SS brown (CL-ML) FILL - CLAY - little to trace silt - trace fine sand - gray to HS brownish gray - very stiff (CH) <del>5.0</del> SS HS <del>10.0</del> 3 SS HS <del>15.0</del> 4 SS HS 20.0 5 SS trace coal in sample 5 HS **25.0** SS 6 trace coal in sample 6 HS FILL - CLAY - trace silt and fine sand - gray - hard (CH) <u> 30.0</u> CURRENT.GDT SS Ø HS <del>35.0</del> 8 ď. SS DATATEMPLATE HS <del>40.0</del> FILL - LIGNITE and SHALE fragments EXPANSION.GPJ SENTINEL BUTTE FORMATION - CLAY - little to trace silt -HS gray - hard (CH) 45.0 10 SS € HS LOS LANDFILL <del>50.0</del> SS 11 coal seam in sample 11 HS <del>55.0</del> 12 SS AECOM LOG WSAMPLENOTES HS <del>60.0</del> \* Calibrated Penetrometer ... continued AECOM JOB NO. **60494667** SHEET NO. The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual.

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<b>1783387.04</b> NL				RIG/FOREMAN	7/21/16	A	MLB         2         2           APP'D BY         AECOM JOB NO.					1				
65.5' WS / 64.0 @ 24 hr. / cave in @ 7			r. / cave in @ 77'		90/MR (Terracon)		BH 60494667						1			

CLIENT LOG OF BORING NUMBER B-2016-05 **Basin Electric Power Cooperative** A=COM PROJECT NAME ARCHITECT-ENGINEER LOS ASH Landfill Expansion **AECOM** -O-UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT) DESCRIPTION OF MATERIAL  $\times$  $\overline{\Delta}$ SAMPLE TYPE UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 30 STANDARD  $\otimes$ PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,891.1 FILL - CLAY - little to trace silt - trace plant roots - brownish SS gray - very stiff (CH) HS FILL - CLAY - little to trace silt - trace coal - gray - hard (CH) <del>5.0</del> 2 SS HS <del>10.0</del> FILL - CLAY - little to trace silt and coal - grayish brown to 3 SS brown - soft to medium (CH) HS <del>15.0</del> 4 ST 5 SS HS FILL - CLAY - little silt - trace coal and clinker - grayish 20.0 6 SS brown - very stiff (CH) HS FILL - CLAY - little sand and silt - trace coal - gray - very stiff **25.0** to hard (CH) 7 ST 8 SS HS FILL - CLAY - little to trace silt, sand, coal, and clinker - grayish brown to brown - very stiff to hard (CH) <del>30.0</del> CURRENT.GDT 9 SS HS FILL - CLAY - little sand and silt - trace coal - gray - very stiff <del>35.0</del> to hard (CH) DATATEMPLATE 10 ST 11 SS  $\bigcirc$ HS <del>40.0</del> FILL - CLAY - little to trace silt and coal - dark gray - very 12 SS EXPANSION.GPJ coal seam from 40.1 to 40.3 feet HS <del>45.0</del> LIGNITE SENTINEL BUTTE FORMATION - CLAY - little to trace silt bluish gray to gray - hard (CH) HS LOS LANDFILL <del>50.0</del> ф 15 SS HS 60494667 <del>55.0</del> 16 SS AECOM LOG WSAMPLENOTES HS 60.0 \* Calibrated Penetrometer ... continued AECOM JOB NO. **60494667** SHEET NO. The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual.

CLIENT LOG OF BORING NUMBER B-2016-05 **Basin Electric Power Cooperative AECOM** PROJECT NAME ARCHITECT-ENGINEER **LOS ASH Landfill Expansion AECOM** -O UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota 3 PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT) SAMPLE TYPE  $\times$  $-\!\!\!\Delta$ **DESCRIPTION OF MATERIAL** UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 50 20 30 STANDARD ⊗ 10 PENETRATION BLOWS/(FT) 20 30 40 + 4570 SURFACE ELEVATION +1,891.1 (Continued) SENTINEL BUTTE FORMATION - CLAY - little to trace silt bluish gray to gray - hard (CH) HS 65.0 +44 18 SS LIGNITE HS \\_100/5" ⊗ <del>70.0</del> HS SENTINEL BUTTE FORMATION - CLAY - dark gray - hard ,<sub>79</sub> <del>75.0</del> ţ0 20 SS HS SENTINEL BUTTE FORMATION - fine CLAYEY SAND -35., little silt - bluish gray - dense (SC) SS End of Boring \* Calibrated Penetrometer Boring advanced to 79.5 feet with 3.25-inch hollow-stem Standard Penetration Test performed with automatic hammer Boring backfilled with chipped bentonite The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual. NORTHING BORING STARTED AECOM OFFICE Oshkosh, Wisconsin 578631.494 BORING COMPLETED 7/27/16 ENTERED BY MLB **EASTING** 1783677.343 APP'D BY RIG/FOREMAN D-90/MR (Terracon) AECOM JOB NO. **60494667** WL

WSAMPLENOTES 60494667 LOS LANDFILL EXPANSION.GPJ DATATEMPLATE CURRENT.GDT 1/13/17

AECOM LOG

45.0' WS / cave in @ 74.5'

LOG OF BORING NUMBER CLIENT B-2016-06 **Basin Electric Power Cooperative** A=COM PROJECT NAME ARCHITECT-ENGINEER LOS ASH Landfill Expansion **AECOM** -O-UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT) SAMPLE TYPE DESCRIPTION OF MATERIAL  $\overline{\Delta}$ UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 30 50 STANDARD  $\otimes$ PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,909.8 FILL - SILTY CLAY - trace sand, coal, and plant roots -Ø SS brown - hard to very stiff (CL-ML) HS <del>5.0</del> FILL - CLAY - little to trace silt, sand, and coal - brownish 2 SS gray to gray - medium to very stiff (CH) HS <del>10.0</del> 3 SS HS <del>15.0</del> ST 5 SS HS 20.0 6 SS hard 4-inch clay seem in sample 6 HS **25.0** ST 8 SS trace clinker in samples 8 and 9 HS <del>30.0</del> CURRENT.GDT 9 SS HS <del>35.0</del> DATATEMPLATE 10 ST hard clay seam in sample 10 11 SS HS <del>40.0</del> 12 SS EXPANSION.GPJ HS 45.0 13 ST 14 SS hard clay seam in sample 14 LOS LANDFILL HS <del>50.0</del> 15 SS HS 60494667 **55.0** 16 ST AECOM LOG WSAMPLENOTES FILL - CLAY - little to trace silt, sand, and coal - brown - very 17 SS stiff (CH) HS 60.0 \* Calibrated Penetrometer ... continued AECOM JOB NO. **60494667** SHEET NO. The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual.

CLIENT LOG OF BORING NUMBER B-2016-06 **Basin Electric Power Cooperative** A=COM PROJECT NAME ARCHITECT-ENGINEER **LOS ASH Landfill Expansion AECOM** -O UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota 3 PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT) SAMPLE TYPE  $\times$  $-\!\!\!\Delta$ **DESCRIPTION OF MATERIAL** UNIT DRY WT. SAMPLE NO. 10 50 20 30 STANDARD ⊗ 10 PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,909.8 (Continued) FILL - CLAY - little to trace silt, sand, and coal - brown - very stiff (CH) hard clay seam in sample 18 HS 65.0 LIGNITE - coarse sand to fine gravel sized grains  $\bigcirc$ SENTINEL BUTTE FORMATION - CLAY - trace silt - bluish HS gray to gray - hard (CH) <del>70.0</del> \*#4 21 SS HS <del>75.0</del> + 22 SS HS + 23 SS End of Boring \* Calibrated Penetrometer Boring advanced to 79.5 feet with 3.25-inch hollow-stem Standard Penetration Test performed with automatic hammer Boring backfilled with chipped bentonite The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual. NORTHING BORING STARTED AECOM OFFICE Oshkosh, Wisconsin 578151.055 BORING COMPLETED 7/26/16 ENTERED BY MLB **EASTING** 1783299.158 RIG/FOREMAN D-90/MR (Terracon) AECOM JOB NO. **60494667** APP'D BY WL 65.0' WS / cave in @ 54'

WSAMPLENOTES 60494667 LOS LANDFILL EXPANSION.GPJ DATATEMPLATE CURRENT.GDT 1/13/17

AECOM LOG

CLIENT LOG OF BORING NUMBER B-2016-07 **Basin Electric Power Cooperative** A=COM PROJECT NAME ARCHITECT-ENGINEER LOS ASH Landfill Expansion **AECOM** -O-UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT) SAMPLE TYPE DESCRIPTION OF MATERIAL  $\times$  $\overline{\Delta}$ UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 30 50 STANDARD  $\otimes$ PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,924.8 FILL - SILTY CLAY - trace sand and plant roots - dark brown SS - dry to moist - hard (CL-ML) HS <del>5.0</del> \* FILL - CLAY - little to trace silt, sand, and coal - dark gray to 2 SS gray - stiff to hard (CH) HS <del>10.0</del> ⊗ 7 0 3 SS HS <del>15.0</del> 0 ST trace hard clay nodules in sample 4 SS 5 HS 20.0 6 SS trace hard clay nodules in sample 6 FILL - CLAY - some sand and silt - gray to dark gray - very HS stiff to stiff (CH) **25.0** ST 8 SS HS <del>30.0</del> CURRENT.GDT 9 SS HS <del>35.0</del> DATATEMPLATE 10 ST 11 SS HS <del>40.0</del> FILL - CLAY - little to trace silt, sand, and coal - brownish ~ • 12 SS gray to gray - very stiff to hard (CH) EXPANSION.GPJ HS 45.0 13 ST Ð 0 14 SS LOS LANDFILL HS <del>50.0</del> (D 15 SS HS 60494667 **55.0** FILL - CLAYEY to SANDY SILT - little to trace coal - dark + brown to brown - hard (CL-ML) 16 ST AECOM LOG WSAMPLENOTES Ø 17 SS HS 60.0 \* Calibrated Penetrometer ... continued AECOM JOB NO. **60494667** SHEET NO. The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual.

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	١	HS			<b>****</b>	gray - very suir i	to still (Cri)						i	. /		
S5.0				_										\		
<u> </u>	9	ST			$\bowtie$								45 X	<b>*</b>		-++
20		SS										]00	<b>3</b>			
70.0	$\overline{}$	HS SS	$\mathbf{T}$	$\top$								]	10/			
	+	55	+	4									*	*		
		HS											ij			
<b>'5.0</b>	_		$\downarrow$	_									1			
2:	_	ST SS	H	+	76.5	SENTINEL BLIT	TE FORMATIO	ON - CLAY - little	to trace silt	· _			1		+	) § <del>54</del>
	-	HS	4	4		bluish gray - har		ort object made	to trace one				Ĭ		*	
3 <b>0.0</b> 24	_	SS	T	T	81.0										+	51 ⊗
			1		E	End of Boring	d to 70 E foot w	uith 2 25 inch halle	au atam		* Calib	rated Pen	etrom	eter	*	
					á	auger		vith 3.25-inch hollo								
						Standard Peneti hammer	ration Test perf	formed with autom	natic							
						Boring backfilled	d with chipped I	bentonite								
	TI	he s	tra	tific	cation lines re	epresent the app	oroximate boun	dary lines betwee	n soil types	: in s	itu, th	e transitio	n may	be gradu	ıal.	
RTHING	_	770					BORING START	ED TIDEKS	-	AECO	M OFFI	CE C	)shko	sh, Wisco	nsin	
STING		776					BORING COMPI	<b>7/25/16</b> LETED		ENTER	RED BY		SHEET	NO.	OF	
	1	7829	930	.33	37			7/25/16			MLE	3		2	2	
L	N	ot E	nc	ou	ntered WD / c	cave in @ 78'	RIG/FOREMAN D-9	90/MR (Terracon)		APP'D	BH		AECOM JOB NO. <b>60494667</b>			

CLIENT LOG OF BORING NUMBER B-2016-08 **Basin Electric Power Cooperative** A=COM PROJECT NAME ARCHITECT-ENGINEER LOS ASH Landfill Expansion **AECOM** -O-UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT) SAMPLE TYPE DESCRIPTION OF MATERIAL  $\times$  $-\!\!\Delta$ UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 30 50 STANDARD  $\otimes$ PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,944.6 10 FILL - SILTY CLAY - trace sand, coal, and plant roots - dark SS brown (CL-ML) FILL - CLAY - little to trace silt and coal - grayish brown to HS brown - very stiff to hard (CH) <del>5.0</del> 0 2 SS HS collected bulk sample of auger cuttings from 2.0 to 9.5 feet <del>10.0</del> 3 SS HS <del>15.0</del> 4 SS collected bulk sample of auger cuttings from 9.5 to 19.5 feet HS 20.0 **\_**O 0 5 SS HS 25.0 FILL - CLAYEY SILT to SILTY CLAY - trace fine sand - gray # - medium to stiff (CL-ML) ST 6 7 SS HS <del>30.0</del> CURRENT.GDT 8 SS HS FILL - CLAY - little to trace silt - gray - hard to very stiff (CH) <del>35.0</del> DATATEMPLATE ST 10 SS HS .13 ⊗ <del>40.0</del> 11 SS EXPANSION.GPJ HS 45.0 12 ST 13 SS LOS LANDFILL HS FILL - CLAY - some sand and silt - trace coal - intermittent <del>50.0</del> 14 SS sand and silt seams - brown - very stiff to hard (CH) HS 60494667 **55.0** 15 ST AECOM LOG WSAMPLENOTES 16 SS HS 60.0 \* Calibrated Penetrometer ... continued AECOM JOB NO. **60494667** SHEET NO. The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual.

CLIENT LOG OF BORING NUMBER B-2016-08 **Basin Electric Power Cooperative** A=COM PROJECT NAME ARCHITECT-ENGINEER **LOS ASH Landfill Expansion AECOM** -O UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT) SAMPLE TYPE  $\times$  $-\!\!\!\Delta$ **DESCRIPTION OF MATERIAL** UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 50 20 30 STANDARD  $\otimes$ PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,944.6 (Continued) 10 FILL - CLAY and SILT - little to trace sand - brownish gray stiff (CL-ML) HS 65.0 ST 18 FILL - CLAY - little to trace silt - gray - hard (CH) ,34 ⊗ 19 SS HS <del>70.0</del> FILL - fine SILTY SAND - trace clay - light brown - medium dense (SM) FILL - SANDY CLAY - some silt - trace coal - brown - hard HS (CH) <del>75.0</del> 21 ST |⊗<sup>32</sup> 22 SS HS FILL - fine CLAYEY SAND - intermitent hard clay layers -23 SS gray - dense (SC) \* Calibrated Penetrometer End of Boring Boring advanced to 79.5 feet with 3.25-inch hollow-stem Standard Penetration Test performed with automatic hammer WSAMPLENOTES 60494667 LOS LANDFILL EXPANSION.GPJ DATATEMPLATE CURRENT.GDT 1/13/17 Boring backfilled with chipped bentonite The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual. NORTHING BORING STARTED AECOM OFFICE Oshkosh, Wisconsin 577839.047 AECOM LOG BORING COMPLETED 7/27/16 ENTERED BY MLB **EASTING** 1783845.503 RIG/FOREMAN D-90/MR (Terracon) APP'D BY
BH AECOM JOB NO. **60494667** WL Not Encountered WD / cave in @ 76'

CLIENT LOG OF BORING NUMBER B-2016-09 **Basin Electric Power Cooperative** A=COM PROJECT NAME ARCHITECT-ENGINEER LOS ASH Landfill Expansion **AECOM** -O-UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT) DESCRIPTION OF MATERIAL  $\times$  $-\!\!\Delta$ SAMPLE TYPE UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 30 STANDARD  $\otimes$ PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,955.4 190 FILL - SILTY CLAY - trace sand, coal, and plant roots - dark SS brown - hard (CL-ML) FILL - CLAY - little sand and silt - trace coal - grayish brown HS - stiff to very stiff (CH) <del>5.0</del> SS collected bulk sample of auger cuttings from 1.5 to 9.5 feet HS \$ <del>10.0</del> FILL - fine CLAYEY SAND - little silt - gray - moist - loose 3 SS HS FILL - CLAY - little to trace silt and coal - trace hard clay <del>15.0</del> nodules - gray - stiff (CH) 4 SS collected bulk sample of auger cuttings from 9.5 to 20.0 feet HS FILL - SANDY CLAY - trace clay - gray - moist (CH) 20.0 5 ST FILL - CLAY - little to trace silt and sand - gray - very stiff 6 SS (CH) HS **25.0** FILL - fine CLAYEY SAND - little silt - gray - moist - medium 7 SS dense (SC) HS FILL - CLAY - trace silt and coal - gray - hard (CH) <del>30.0</del> CURRENT.GDT 8 ST 10 ⊗ -Ф 9 SS HS FILL - SANDY CLAY - little silt - trace coal - gray - hard (CH) <del>35.0</del> Φ 10 SS DATATEMPLATE HS FILL - CLAY - little to trace silt - dark gray to gray - hard to 40.0 very stiff (CH) † 11 ST EXPANSION.GPJ 12 SS \* l⊗<sup>12</sup> HS <del>45.0</del> 13 SS HS LOS LANDFILL <del>50.0</del> 14 ST 15 SS 60494667 HS .13 <del>55.0</del> 16 SS AECOM LOG WSAMPLENOTES HS 60.0 \* Calibrated Penetrometer ... continued AECOM JOB NO. **60494667** SHEET NO. The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual.

CLIENT LOG OF BORING NUMBER B-2016-09 **Basin Electric Power Cooperative AECOM** PROJECT NAME ARCHITECT-ENGINEER LOS ASH Landfill Expansion **AECOM** -O UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota PLASTIC WATER LIQUID **ELEVATION(FT** SAMPLE DISTANCE LIMIT % CONTENT % LIMIT % DEPTH(FT) SAMPLE TYPE  $\times$  $\overline{\Delta}$ **DESCRIPTION OF MATERIAL** UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 50 20 30 STANDARD ⊗ 10 PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,955.4 (Continued) FILL - CLAY - little to trace silt - dark gray to gray - hard to 17 ST very stiff (CH) SS Ď 18 13<u>.</u> HS 65.0 19 SS HS <del>70.0</del> 20 ST 21 SS FILL - SILTY CLAY - gray - hard (CL-ML) HS ; \_ \_ <del>75.0</del> 22 SS HS 80.0 ST 23 FILL - CLAY - little to trace silt, sand, and coal - brownish 24 SS gray to gray - hard (CH) 83.5 End of Boring \* Calibrated Penetrometer Boring advanced to 80.0 feet with 3.25-inch hollow-stem WSAMPLENOTES 60494667 LOS LANDFILL EXPANSION.GPJ DATATEMPLATE\_CURRENT.GDT 1/13/17 Standard Penetration Test performed with automatic Boring backfilled with chipped bentonite The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual. NORTHING BORING STARTED AECOM OFFICE Oshkosh, Wisconsin 577484.589 AECOM LOG BORING COMPLETED 7/28/16 ENTERED BY MLB **EASTING** 1784314.822 APP'D BY RIG/FOREMAN D-90/MR (Terracon) AECOM JOB NO. **60494667** WL

Not Encountered WD / cave in @ 77'

LOG OF BORING NUMBER CLIENT B-2016-10 **Basin Electric Power Cooperative Boring offset 50 feet NW AECOM** PROJECT NAME ARCHITECT-ENGINEER LOS ASH Landfill Expansion **AECOM** -O-UNCONFINED COMPRESSIVE STRENGTH SITE LOCATION TONS/FT.<sup>2</sup> Stanton, Mercer County, North Dakota 3 PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT) SAMPLE TYPE DESCRIPTION OF MATERIAL  $\times$  $\overline{\Delta}$ UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 30 STANDARD  $\otimes$ PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,910.5 FILL - CLAYEY SILT - little sand - trace plant roots - light SS brown - dry to moist (ML) HS *7* <del>5.0</del> 2 SS FILL - CLAY - little to trace silt and coal - grayish brown to brownish gray - stiff to very stiff (CH) HS |×12 <del>10.0</del>  $\bigcirc$ 3 SS HS FILL - CLAY - trace to little silt and coal - gray - medium <del>15.0</del> (CH) 4 SS ST HS <del>20.0</del> 8 0 5 SS FILL - SILTY CLAY - trace coal - gray - stiff to very stiff (CL-ML) HS **25.0** 6 SS FILL - fine CLAYEY SAND - little silt - trace coal - gray to HS bluish gray - medium dense to loose (SC) <del>30.0</del> CURRENT.GDT 7 SS HS <del>35.0</del> 8 SS DATATEMPLATE HS <del>40.0</del> 9 SS EXPANSION.GPJ HS FILL - CLAY - little to trace sand, silt, and coal - grayish 45.0 brown - medium to stiff (CH) 10 10 SS FILL - fine CLAYEY SAND - little silt - gray to bluish gray -HS LOS LANDFILL loose to medium dense (SC) <del>50.0</del> 11 SS HS TV 55.0 12 SS AECOM LOG WSAMPLENOTES FILL - CLAY - little silt - trace coal - grayish brown - stiff to HS very stiff (CH) <del>60.0</del> \* Calibrated Penetrometer ... continued AECOM JOB NO. **60494667** SHEET NO. The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual.

CLIENT LOG OF BORING NUMBER B-2016-10 **Basin Electric Power Cooperative** Boring offset 50 feet NW **AECOM** PROJECT NAME ARCHITECT-ENGINEER **LOS ASH Landfill Expansion AECOM** -O- UNCONFINED COMPRESSIVE STRENGTH TONS/FT.<sup>2</sup> 1 2 3 4 5 SITE LOCATION Stanton, Mercer County, North Dakota PLASTIC WATER LIQUID SAMPLE DISTANCE **ELEVATION(FT** LIMIT % CONTENT % LIMIT % DEPTH(FT) SAMPLE TYPE  $\times$  $-\!\!\!\Delta$ **DESCRIPTION OF MATERIAL** UNIT DRY WT. LBS./FT.³ SAMPLE NO. 10 50 20 30 STANDARD  $\otimes$ PENETRATION BLOWS/(FT) SURFACE ELEVATION +1,910.5 (Continued) FILL - CLAY - little silt - trace coal - grayish brown - stiff to very stiff (CH) HS 65.0 14 SS HS <del>70.0</del> 15 SS HS SENTINEL BUTTE FORMATION - CLAY - trace silt - dark <del>75.0</del> gray - hard (CH) 16 SS D HS .54 ⊗ + 17 SS End of Boring \* Calibrated Penetrometer Boring advanced to 79.5 feet with 3.25-inch hollow-stem Standard Penetration Test performed with automatic hammer WSAMPLENOTES 60494667\_LOS LANDFILL EXPANSION.GPJ DATATEMPLATE\_CURRENT.GDT 1/13/17 Boring backfilled with chipped bentonite The stratification lines represent the approximate boundary lines between soil types: in situ, the transition may be gradual. NORTHING BORING STARTED AECOM OFFICE Oshkosh, Wisconsin 578825.726 AECOM LOG BORING COMPLETED 7/28/16 ENTERED BY MLB **EASTING** 1784372.785 APP'D BY RIG/FOREMAN D-90/MR (Terracon) AECOM JOB NO. **60494667** WL Not Encountered WD / cave in @ 77'

AECOM	A				WELL NUM	/IBEF	R MW-2016-1 PAGE 1 OF 3
CLIENT Basi	n Elec	tric			PROJECT NAME Lelands Olds Landfill		
PROJECT NU	MBER	6051	<u>4340</u>		PROJECT LOCATION Stanton, ND		
DATE STARTI	ED <u>8/</u>	7/2016	<u>;                                    </u>		COMPLETED 8/7/2016 GROUND ELEVATION 1929.2 ft HAI	MMER T	YPE Not Applicable
DRILLING CO	NTRAC	CTOR	Caso	ade D	rilling GROUND WATER LEVELS:		
ORILLING ME	THOD	Rota	ry Sor	nic	AT TIME OF DRILLING		
OGGED BY	Ryan	Klutes	′	CHEC	KED BY A. Lanning AT END OF DRILLING		
COORDINATE	S _57	7563.4	N	17866	605.09 E	1.33 ft	
SAMPLE TYPE NUMBER	OVERY	r PENE- ER, TSF	C.S.	PHIC OG	MATERIAL RECORDITION	Cas Cas	sing Top Elev: 1.93 (ft) sing Type: 2" PVC Pipe WELL DIAGRAM
SAMPLI	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION		Top of Casing (estimated 1.93' ags)
5 SONIG	C 100		CL		CLAY, trace gravel, reworked material; brown to light brown	09.2	Grout (0' - 78' bgs) PVC Pipe (1.93' ags - 96' bgs)
25 SONIG	2 100		CL		35.0	94.2	

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:43 - C:\CAROL B GINTLOS\LOS\_082316.GPJ

AE	CON	1				WELL NUMB	ER MW-2016-1 PAGE 2 OF 3
	T Basir					PROJECT NAME Lelands Olds Landfill	
PROJE	CT NUN	/IBER	6051	4340	1	PROJECT LOCATION Stanton, ND	
DEPTH (ff)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
  40				CL		CLAY, sticky, reworked material; brown 40.0 1889.2	Grout (0' - 78' bgs) PVC Pipe (1.93' ags - 96' bgs)
  45	SONIC	100		CL		SILTY CLAY, reworked material; light brown 45.0 1884.2	bgs)
   _ 50	SONIC	100				SANDY CLAY, very hard, crumbly; red	
   55	SONIC	100					
LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:43 - C:\CAROL B GINT\LOS\LOS_082316.GPJ  24  25  26  27  28  29  29  20  20  20  20  20  20  20  20	SONIC	100		CL			
LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/7	SONIC	100		CL		CLAY, very hard, native material; gray   T  75.0	

ROJEC							PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton, ND			
							GROUND ELEVATION 1954.7 ft	HAMME	R TY	PE Not Applicable
							GROUND WATER LEVELS:			
	G MET					(ED D)( A				
						<b>(ED BY</b> <u>A. Lanning</u> 497.98 E				
								2.07 10 11.0	1	ng Top Elev: 1.79 (ft)
	吊	ERY	-JSF	, i	ပ				Casi	ng Type: 2" PVC Pipe
(H)	LE T MBE	200	ET PE	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION			WELL DIAGRAM
)   !	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	0.0	GR/					Top of Casing (estimated 1.7 ags)
5	SONIC	100		CL		20.0 CLAY, trace silt, re	eworked material; brown to light brown	1934.7		Grout (0' - 119' bgs)  PVC Pipe (1.79' ags - 1: bgs)
30 - - -	SONIC	100	_	CL		SILTY CLAY, rewo	orked material; gray	1924.7		

## **WELL NUMBER MW-2016-2 AECOM** CLIENT Basin Electric PROJECT NAME Lelands Olds Landfill PROJECT NUMBER 60514340 PROJECT LOCATION Stanton, ND SAMPLE TYPE NUMBER POCKET PENE-TROMETER, TSF % RECOVERY GRAPHIC LOG U.S.C.S. DEPTH (ft) WELL DIAGRAM MATERIAL DESCRIPTION 35 SILTY CLAY, reworked material; gray CL 37.0 1917.7 Grout CLAY, sticky, reworked; brown (0' - 119' bgs) CL PVC Pipe (1.79' ags - 136' 40 1914.7 SONIC 100 S.A.A., brown to light brown CL 45 SILTY CLAY, reworked material; light brown to gray 50 SONIC 100 CL 1900.7 SILTY CLAY, reworked material; gray 55 LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:44 - C.\CAROL B GINT\LOS\LOS\_082316.GPJ CL 58.0 1896.7 CLAY, reworked material; brown to gray CL SONIC 100 CLAYEY SILT, crumbly, reworked material; gray

CLAY, very sticky, reworked material; brown

1882.7

65

70

SONIC 100

ML

CL

72.0

### **WELL NUMBER MW-2016-2 AECOM** PAGE 3 OF 4 CLIENT Basin Electric PROJECT NAME Lelands Olds Landfill PROJECT NUMBER 60514340 PROJECT LOCATION Stanton, ND SAMPLE TYPE NUMBER POCKET PENE-TROMETER, TSF % RECOVERY GRAPHIC LOG U.S.C.S. DEPTH (ft) WELL DIAGRAM MATERIAL DESCRIPTION 75 CLAY, very sticky, reworked material; brown (0' - 119' bgs) PVC Pipe (1.79' ags - 136' CL 78.0 1876.7 CLAY, reworked material; gray CL 80 80.0 1874.7 SONIC 100 CLAY, stiff, reworked material; gray CL 82.0 1872.7 LIGNITE; brown COA 1870.7 CLAY, reworked material; gray with orange clay fragments 85 CL 90 SONIC 100 CLAY, with lignite fragments, reworked material; brown to light brown CL 95 LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:44 - C.\CAROL B GINT\LOS\LOS\_082316.GPJ 97.0 1857.7 CLAY, hard, trace silt, native material; gray Slow drilling CL SONIC 100 100 100.0 CLAY, very hard; gray

105

110

SONIC 100

SONIC 100

 $ar{m{\Lambda}}$ 

CL

**WELL NUMBER MW-2016-2 AECOM** PAGE 4 OF 4 CLIENT Basin Electric PROJECT NAME Lelands Olds Landfill PROJECT NUMBER 60514340 PROJECT LOCATION Stanton, ND SAMPLE TYPE NUMBER POCKET PENE-TROMETER, TSF % RECOVERY GRAPHIC LOG DEPTH (ft) U.S.C.S. WELL DIAGRAM MATERIAL DESCRIPTION 115 CLAY, very hard; gray Grout (0' - 119' bgs) **PVC Pipe** (1.79' ags - 136' bgs) 120 CL ■Bentonite Seal (119'-124' bgs) SONIC 100 125 127.0 1827.7 LIGNITE, dry, crumbly; brown to black 130 #40 Sand (124' - 137' bgs) 0.010 Slotted SONIC 100 COAL Pipe (126' - 136' bgs) 135 LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:45 - C:\CAROL B GINT\LOS\LOS 082316.GPJ 1818.7 136.0 Total Depth of CLAY, very hard; gray Well 138.79' BTOC SONIC 100 CL Bentonite Chip Fill Below Well Bottom of borehole at 140.0 feet.

#### WELL NUMBER MW-2016-3 **AECOM** PAGE 1 OF 4 CLIENT Basin Electric PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton, ND PROJECT NUMBER 60514340 **DATE STARTED** <u>8/5/2016</u> **COMPLETED** <u>8/5/2016</u> GROUND ELEVATION 1937.1 ft HAMMER TYPE Not Applicable DRILLING CONTRACTOR Cascade Drilling **GROUND WATER LEVELS:** DRILLING METHOD Rotary Sonic AT TIME OF DRILLING \_---LOGGED BY Ryan Klutes CHECKED BY A. Lanning AT END OF DRILLING \_---**▼ AFTER DRILLING** 93.14 ft / Elev 1843.96 ft COORDINATES 578652.16 N 1784880.82 E Casing Top Elev: 1.72 (ft) Casing Type: 2" PVC Pipe SAMPLE TYPE NUMBER POCKET PENE-TROMETER, TSF RECOVERY GRAPHIC LOG U.S.C.S. DEPTH (ft) WELL DIAGRAM MATERIAL DESCRIPTION Top of Casing (estimated 1.72' 0 ags) CLAY, with fragments of lignite, reworked material; brown to light brown SONIC 100 5 CL Grout (0' - 109' bgs) 10 SONIC 100 CLAY, trace silt, reworked material; brown PVC Pipe (1.72' ags - 126' bgs) 15 CL SONIC 100 1913.1 SILTY CLAY, reworked material; gray 25 CL 30 SONIC 100 32.0 1905.1 CLAY, trace gravel, very sticky, reworked material; brown CL

GE GHENT SOIL-WELL LOG - GHENT GDT - 8/23/16 14:45 - C.:CAROL B GINTLOS/LOS 082316.GPJ

## **WELL NUMBER MW-2016-3 AECOM** PAGE 2 OF 4 CLIENT Basin Electric PROJECT NAME Lelands Olds Landfill PROJECT NUMBER 60514340 PROJECT LOCATION Stanton, ND SAMPLE TYPE NUMBER POCKET PENE-TROMETER, TSF % RECOVERY GRAPHIC LOG U.S.C.S. DEPTH (ft) WELL DIAGRAM MATERIAL DESCRIPTION 35 CLAY, trace gravel, very sticky, reworked material; brown Grout (0' - 109' bgs) PVC Pipe (1.72' ags - 126' CL 40 SONIC 100 bgs) CLAY, with gray silt, reworked material; dark brown 45 50 SONIC 100 CL 55 SONIC 100 CLAY, very sticky, reworked material; dark brown CL 1874.6 SILTY CLAY, hard, reworked material; gray 65 CL CLAY, reworked material; brown to orange 70 SONIC 100 CL

CLAY, sticky, reworked material; brown

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:45 - C.\CAROL B GINT\LOS\LOS\_082316.GPJ

A	COM	1				WELL NUME	BER I	<b>MW-2016-3</b> PAGE 3 OF 4
	NT Basir					PROJECT NAME Lelands Olds Landfill		
PROJ	IECT NUN	/IBER	6051	4340		PROJECT LOCATION Stanton, ND		
DEPTH (#)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	W	ELL DIAGRAM
80	SONIC			CL		CLAY, sticky, reworked material; brown  84.0  CLAY, trace silt, very hard, native soil; gray Very hard drilling		Grout (0' - 109' bgs) PVC Pipe (1.72' ags - 126' bgs)
90	SONIC	100		CL		Ā		
NTLOSILOS 082316.GP, 001	SONIC	100				100.0		
16 14:45 - C:\CAROL B GII 10	SONIC	100				CLAY, very hard; gray Very hard drilling		Grout (0' - 109' bgs) PVC Pipe (1.72' ags - 126' bgs)
ENT.GDT - 8/23/1	SONIC	100		CL				
LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:45 - C.\CAROL B GINTLOSILOS_082316.GPJ  10	SONIC	100				115.0 1822.1		■Bentonite Seal (109'-113')

## **WELL NUMBER MW-2016-3 AECOM** PAGE 4 OF 4 CLIENT Basin Electric PROJECT NAME Lelands Olds Landfill PROJECT NUMBER 60514340 PROJECT LOCATION Stanton, ND SAMPLE TYPE NUMBER POCKET PENE-TROMETER, TSF % RECOVERY GRAPHIC LOG DEPTH (ft) U.S.C.S. WELL DIAGRAM MATERIAL DESCRIPTION 115 LIGNITE, dry, very crumbly; brown SONIC 100 #40 Sand (113'-127' bgs) 120 0.010 Slotted COAL Pipe (116' - 126' bgs) 125 SONIC 100 Total Depth of Well 128.72' BTOC CLAY, very hard; gray 130 Bentonite Chip Fill Below Well CL SONIC 100 Bottom of borehole at 134.0 feet.

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:45 - C.\CAROL B GINT\LOS\LOS\_082316.GPJ

ΑĒ	CON							·	PAGE 1 OF 4
CLIEN	IT Basir	Elect	tric			PROJECT NAME Lelands Olds Landfill			
PROJ	ECT NUN	IBER	6051			PROJECT LOCATION Stanton, ND			
DATE	STARTE	<b>D</b> <u>8/</u> 2	2/2016	6		COMPLETED _8/4/2016         GROUND ELEVATION _ 1937.1 ft	HAMME	R TYP	PE Not Applicable
DRILL	ING CON	ITRAC	CTOR	Caso	ade D	illing GROUND WATER LEVELS:			
DRILL	ING MET	HOD	Rota	ry Sor	nic	AT TIME OF DRILLING			
LOGG	ED BY _	Ryan	Klutes	(	CHEC	KED BY A. Lanning AT END OF DRILLING			
COOF	RDINATES	578	8282.6	2 N	1784	229.27 E	ev 1861.69	ft	
т	YPE :R	RECOVERY	ENE-	(vi	೦			Casin Casin	g Top Elev: 1.93 (ft) g Type: 2" PVC Pipe
DEPTH (ft)	LET	200	IT PE	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION		,	WELL DIAGRAM
0 0	SAMPLE TYPE NUMBER	% RE	POCKET PENE- TROMETER, TSF	) 0.	GR,				Top of Casing (estimated 1.93' ags)
0				OL	7////	0.5 ORGANIC SILT, top soil; black	1936.6		Sign,
-						CLAY, reworked material; red to brown			
_	SONIC	100							
_				CL					
5									
			1			5.5 CLAYEY SILT, reworked material; light brown to gray	1931.6		
_						OLATET SILT, Teworked material, light brown to gray			
_									
_									
10		400							Grout (0' - 106' bgs)
	SONIC	100		ML					
_				""				<b>M</b> .	PVC Pipe (1.93' ags - 127' bgs)
_									bgs)
_									
15									
			1			16.0	1921 1		
-						CLAY, sticky, reworked material; brown to light brown	1021.1		
_									
_									
20									
	SONIC	100							
-									
_									
-				CL					
25									
23_			1						
-									
-									
-									
30									
JU _	SONIC	100				31.0	1906.1		
-						SILTY CLAY, reworked material; light brown	1900.1		
-						Lenses of sticky brown clay			
-				CL					
-									

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:46 - C:\CAROL B GINTLOS\LOS\_082316.GPJ

AECOA	A				WELL NUMB	SER MW-2016-4 PAGE 2 OF 4
CLIENT Basi			10.10		PROJECT NAME Lelands Olds Landfill	
PROJECT NU	MBEK	6051	4340		PROJECT LOCATION Stanton, ND	
SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
			CL		SILTY CLAY, reworked material; light brown Lenses of sticky brown clay	Grout
					38.0	(0' - 106' bgs)
  	100		ML			PVC Pipe (1.93' ags - 127' bgs)
45					45.0	
	C 100		CL		51.0	
	C 100		ML		64.0	
65	C 100		CL		CLAY, sticky, reworked material; moist, brown to light brown  73.0 LIGNITE, crumbly; brown to black  1864.1	
75			CL		CLAY, sticky, reworked material; brown to gray	

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:46 - C:\CAROL B GINTLOS\LOS\_082316.GPJ

A5	CON					WELL NUM	BER MW-2016-4 PAGE 3 OF 4
	T Basin			4340		PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton, ND	
DEPTH (#)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
80	SONIC	100				¥ CLAY, sticky, reworked material; brown to gray	Grout (0' - 106' bgs) PVC Pipe (1.93' ags - 127' bgs)
90	SONIC	100		CL			
 	SONIC	100		CL COAL		96.0 1841 97.0 CLAY, very hard, native material; gray 1840 97.5 LIGNITE, very hard; brown CLAY, very hard; gray	
100	SONIC	100				CLAY, very hard, trace silt; gray	
   110	SONIC	100		CL		110.0 1827	7.1 ■■Bentonite Seal
   115	SONIC	100		CL		SILTY CLAY, with small lignite horizons; gray	■Bentonite Seal (106'-114' bgs)

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:46 - C:\CAROL B GINTLOS\LOS\_082316.GPJ

ΑΞ	COM										WELL	NUMB	BER		<b>V-2016-5</b> AGE 1 OF 3
CLIEN	I <b>T</b> Basin	Elect	ric					_ PROJE	ECT NAME	Lelands O	lds Landfill				
PROJ	ECT NUM	IBER	6051	4340				PROJE	ECT LOCAT	TION Stant	on, ND				
DATE	STARTE	D <u>8/</u>	10/201	6		COMPLETED	8/10/2016	(	GROUND E	LEVATION	1935.2 ft	HAMME	ER TYI	PE <u>N</u>	ot Applicable
DRILL	ING CON	TRAC	TOR	Casc	ade D	rilling									
DRILL	ING MET	HOD	Rotar	y Son	ic				AT TI	ME OF DRIL	LING				
LOGG	ED BY _	Ryan	Klutes	(	CHEC	KED BY A. La	nning		AT EI		LING				
						618.06 E			▼ AFTE	R DRILLING	49.81 ft / E	lev 1885.39	ft		
Ŧ	TYPE ER	VERY	PENE- R, TSF	ο.	HIC										Elev: 1.11 (ft) : 2" PVC Pipe
DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG			MATER	RIAL DESC	RIPTION				_	DIAGRAM  Top of Casing (estimated 1.11'
0	()	^			//////									\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	(estimated 1.11 ags)
5 10 15	SONIC			CL		CLAY	, reworked m	naterial; b	rown						Grout (0' - 97' bgs) PVC Pipe (1.11' ags - 118' bgs)
	SONIC	100		CL		31.0	, with lignite				rown				

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:47 - C:\CAROL B GINTLOS\LOS\_082316.GPJ

# WELL NUMBER MW-2016-5

								PAGE 2 OF 3
	NT Basir			4240		PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton, ND		
PROJ	ECT NUN	IDER	0051	4340		PROJECT EOCATION Stanton, ND		
(#) 40	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION		WELL DIAGRAM
40	SONIC	100			/////	CLAY, reworked material; brown		
 				CL		43.5SANDY CLAY, reworked material; gray	1891.7	Grout (0' - 97' bgs) PVC Pipe (1.11' ags - 118' bgs)
45	-			CL		47.0	1888.2	
50	SONIC	100		CL		CLAY, sticky, reworked material; brown	1883.2	
55			_	CL		SANDY CLAY, reworked material; brown with orange clay horizons		
  - 60	SONIC	100		02		60.0SANDY CLAY, trace gravel, reworked material; gray	1875.2	
  5				CL		65.0	1870.2	
	-					SANDY CLAY, trace gravel, crumbly, reworked material; light brown	1070:2	
70	SONIC	100		CL		73.0	1862.2	
75				CL		CLAY, with lignite fragments, very hard; gray		
	-			CL		77.5  CLAY, sticky, trace gravel and lignite fragments, reworked materials; brown	1857.7	
80	SONIC	100		CL		CLAY, with lignite fragments, reworked materials; brown to light brown	1855.2	
85				CL		CLAY, with lignite, reworked horizons; brown with orange clay	1851.2	

AE	CON	4				WELL NO	JMB		<b>W-2016-5</b> PAGE 3 OF 3
	T Basir					PROJECT NAME Lelands Olds Landfill			
PROJ	ECT NUN	/IBER	6051	4340	ı	PROJECT LOCATION Stanton, ND			
DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION		WEL	L DIAGRAM
 	CONIC	100		CL		CLAY, with lignite, reworked horizons; brown with orange clay horizons 88.5	1846.7		← Grout (0' - 97' bgs) ¬ PVC Pipe (1.11' ags - 118'
 90 	SONIC	100		CL		SANDY CLAY, very hard, crumbly, reworked material; light brown			bgs)
95 				CL		94.0 CLAY, trace silt, very hard, native material; gray Very hard drilling	1841.2		
 100 	SONIC	100				100.0 CLAY, trace silt, very hard; gray Very hard drilling	1835.2		■Bentonite Seal (97'-105' bgs)
105	SONIC	100		CL					
 _ 110 			_			110.0_ LIGNITE, dry, crumbly; brown	1825.2		#40 Sand
  115	SONIC	100		COAL	3	116.0	1819.2		(105' - 119' bgs)  — 0.010 Slotted  Pipe (108' - 118' bgs)
  120	SONIC	100		CL		CLAY, hard; gray			Total Depth of Well 120.11¹ BTOC
  - 						123.0 Bottom of borehole at 123.0 feet.	1812.2		◆ Bentonite Chip Fill Below Well
110  - 115  - 120 									

LIENT Basin							ROJECT NAME Lelands O					
							GROUND ELEVATION		HAMME	R TY	PE Not App	licable
							GROUND WATER LEVE		_			
RILLING MET												
GGED BY	Ryan I	Klutes	(	CHECKED E	Y A. Lannin	g						
					'8 E			41.47 ft / Ele	ev 1894.83	ft		
7PE :R	ERY	POCKET PENE- TROMETER, TSF	Ö.	ಲ						Casir Casir	ng Top Elev: 2. ng Type: 2" PV	15 (ft) C Pipe
(ft) APLE TY NUMBER	% RECOVERY	(ET PI IETER	U.S.C.S.	GRAPHIC LOG		MA	ATERIAL DESCRIPTION				WELL DIAG	RAM
SAMPLE TYPE NUMBER	% RE	POCE	U	GR			ial; brown to light brown				Top of (estimated ags)	Casing ted 2.1
SONIC  SONIC  SONIC			CL	11.0	CLAY, stic	sky, reworked	d material; brown		1925.3		Grout (0' - 95 PVC P (2.15' a bgs)	
SONIC	100		CL	31.0	SANDY CI	LAY, rework	ed material; gray		1905.3			

A	CON	8				WELL NUME	BER MW-2016-6 PAGE 2 OF 3
	NT Basir					PROJECT NAME Lelands Olds Landfill	
PRO.	IECT NUN	/IBER	6051	4340		PROJECT LOCATION Stanton, ND	
(#) 35	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
   40	SONIC	100		CL		CLAY, reworked material; light brown  40.0	Grout (0' - 95' bgs) PVC Pipe (2.15' ags - 113' bgs)
   45	- JOINIC	100		CL		SILTY CLAY, stiff, reworked material; gray	
E TEMPLATE.GPJ	SONIC	100		CL		SANDY CLAY, very soft, reworked material; gray with brown clay lenses	
LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 13:37 - C.:/CAROL B GINTLOS/SAMPLE TEMPLATE.GPJ  2	SONIC	100		CL		SANDY CLAY, reworked material; gray with brown clay lenses  71.5  SANDY CLAY, with liquite fragments, reworked material; gray.	
CE GHENT SOIL				CL		SANDY CLAY, with lignite fragments, reworked material; gray	

A	COM	1				WELL NUM		<b>N-2016-6</b> PAGE 3 OF 3
CLIE	NT Basir	n Elec	tric			PROJECT NAME Lelands Olds Landfill		
PRO.	JECT NUN	/IBER	6051	4340		PROJECT LOCATION Stanton, ND		
H1(1)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WEL	L DIAGRAM
- ·				CL		SANDY CLAY, with lignite fragments, reworked material; gray 79.0	3	Grout (0' - 95' bgs) PVC Pipe (2.15' ags - 113' bgs)
- 80 	SONIC	100		CL		CLAY, with lignite fragments, reworked material; brown  84.0		
- 85 	SONIC	100				CLAY, very hard, native material; gray		
90 	SONIC	100		CL				
ATLOS/SAMPLE TEMPL	SONIC	100				100.0	.3	■Bentonite Seal (95'-100' bgs)
LGE GHENT SOIL-WELL LOG - GHENT GDT - 8/23/16 13:37 - C:\CAROL B GINT\LOS\SAMPLE TEMPLATE.GPJ  10	SONIC	100		CL		CLAY, very hard, native material; gray Very hard drilling		
LOG - GHENT.GDT - 8/23	SONIC	100		COAL		LIGNITE, crumbly; brown		#40 Sand (100' - 114' bgs) - 0.010 Slotted Pipe (103' - 113' bgs)
HENT SOIL-WELL	SONIC	100		CL		113.0		Total Depth of Well
LGE GF		İ		J.	<u> </u>	Bottom of borehole at 114.0 feet.	<u>.3 [+ . ; + . ; + . ; + . ]</u>	116.15' BTOC

AĒ	CON	7				WELL NUI	MRF	=K	MW-2016-7 PAGE 1 OF 2
CLIEN	T Dooin	Floor	rio			DDO IECT NAME I clando Oldo I andfill			
	T Basin					PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton, ND			
								TVD	E Not Applicable
						COMPLETED 8/8/2016 GROUND ELEVATION 1926.6 ft HA	INIINIEL	CITE	E Not Applicable
	ING MET					GROUND WATER LEVELS:  AT TIME OF DRILLING			
						ED BY _A. Lanning         AT END OF DRILLING           071.11 E         Y AFTER DRILLING _72.93 ft / Elev 185			
					1700	<u> </u>			T Fl. 47(0)
	'PE	R	후SF					Casing	Top Elev: 1.7 (ft) Type: 2" PVC Pipe
T (t	ΞΤΥ BEF	RECOVERY	r PEN ER, 1	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION		٧	VELL DIAGRAM
DEPTH (ft)	APL! JUM	EC	CKET	J.S.	LORA	MATERIAL DESCRIPTION			1
	SAMPLE TYPE NUMBER	% R	POCKET PENE- TROMETER, TSF	_	0			1	Top of Casing (estimated 1.70)
0						CLAY, sticky, reworked material; brown to light brown			àgs)
-						on the second se			
-	SONIC	100							
							8		
5				CL					
_									
_							8		
_									
10							917.1		Grout (0' - 56' bgs)
10	SONIC	100				SILTY CLAY, reworked material; gray	8		<b>X</b> /// `
								<b>X</b> 1	PVC Pipe (1.70' ags - 75'
									bgs)
_				CL			8		
15				OL					
_									
-							8		
-						19.0	907.6		
20						CLAY, reworked material; brown to light brown			
							8		
_									
-									
				CL			8		
25	SONIC	100		OL					
_									
							K		
_									
30						SULTY CLAY reworked material; gray	896.6		
_						SILTY CLAY, reworked material; gray	K		
_									
-				CL					
35							K		
			] ]			36.0 <u>1</u>	890.6		
. ]						CLAY, sticky; brown	- K	$\langle \! \rangle \mid$	Grout
. 4				CL			8		Grout (0' - 56' bgs)
								∅ 1	PVC Pipe (1.70' ags - 75'

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:50 - C.\CAROL B GINTLOS\LOS\_082316.GPJ

AE	CON					WELL NUM		<b>/-2016-7</b> AGE 2 OF 2
	T Basin					PROJECT NAME Lelands Olds Landfill		
PROJI	ECT NUM	IBER	6051	4340		PROJECT LOCATION Stanton, ND		
(#) 40	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL	DIAGRAM
	SONIC	100				CLAY, sticky, reworked material; brown		bgs)
				CL				
- – - – 45				ML		43.0	3.6	
						47.5		
  <u>50</u>	SONIC	100		CL		CLAY, sticky, reworked material; brown 51.0 1875		
- – - –				CL		CLAY, with lignite and gravel fragments, reworked material; brown  54.0 1872		
55 				CL		SILTY CLAY, reworked material; gray		
						58.5	<u>3.1</u>	Bentonite Seal
 60	SONIC	100		CL		CLAY, sticky, reworked material; brown 60.0 1866		(56'-61 bgs')
   - 65	SUNIC	100		CL		CLAY, sticky, reworked material; brown to orange  65.0  1861		
				CL		G6.0 CLAY, hard, native material; gray		
  70 	SONIC	100		COAL		LIGNITE, powdery; black to brown		#40 Sand (61' - 76' bgs) 0.010 Slotted Pipe (65' - 75' bgs)
  75						74.0 1852 CLAY, very hard; gray		Total Depth of Well 77.70' BTOC
80	SONIC	100		CL				77.70' BTOC Bentonite Chip Fill Below Well
65  - 70  - 75  80					<u> </u>	82.0 Bottom of borehole at 82.0 feet.	.6	

	T NUM ARTEI G CON	BER  0 8/8  TRAC	6051 3/2016 TOR	4340 Caso	(cade Dr	PR					
						(ED BY A. Lanning					
				IN	17659	94.31 E			Casing Top Elev: 1.67 (ft)		
(ft)	NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MA	TERIAL DESCRIPTION		Casing Type: 2" PVC Pipe  WELL DIAGRAM		
0   6		Ж	POC						Top of Casing (estimated 1. ags)		
	SOINIC			CL	14.0 SANDY CLAY, reworked material; light brown	d material; light brown	1922.9	Grout (0' - 87' bgs) PVC Pipe (1.67' ags - 1 bgs)			
0	SONIC	100		CL		CLAY, reworked materia horizons	al; brown with light brown sandy clay	1916.9			

#### **WELL NUMBER MW-2016-8 AECOM** PAGE 2 OF 3 CLIENT Basin Electric PROJECT NAME Lelands Olds Landfill PROJECT NUMBER 60514340 PROJECT LOCATION Stanton, ND SAMPLE TYPE NUMBER POCKET PENE-TROMETER, TSF % RECOVERY GRAPHIC LOG U.S.C.S. DEPTH (ft) WELL DIAGRAM MATERIAL DESCRIPTION 35 CLAY, reworked material; brown with light brown sandy clay horizons Grout CL (0' - 87' bgs) PVC Pipe (1.67' ags - 106' 40 SONIC 100 CLAY, with sandy clay, reworked material; brown with gray clay horizons CL 45 CLAY, reworked material; brown 50 CL SONIC 100 52.0 CLAY, with lignite, reworked material; brown CL 55 55.0 1881.9 SANDY CLAY, reworked material; brown LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:52 - C.\CAROL B GINT\LOS\LOS\_082316.GPJ CL CLAY, with lignite fragments, sticky, reworked material; brown CL 60 1876.9 SONIC 100 CLAY, sticky, reworked material; brown CL SANDSTONE, poorly cemented, very crumbly; red to orange 65 SANDSTONE 70 SONIC 100

AE	CON	8				WELL NUME	BER MW-2016-8 PAGE 3 OF 3					
CLIEN	I <b>T</b> Basin	ı Elect	tric			PROJECT NAME Lelands Olds Landfill						
	ECT NUM			4340		PROJECT LOCATION Stanton, ND						
DEPTH (#)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM					
80 	SONIC	100	SAN	IDST(		SANDSTONE, poorly cemented, very crumbly; red to orange  80.0 CLAY, very hard; light brown  83.5 CLAY, very hard, native material; gray						
90	SONIC	100		CL			■Bentonite Seal (87'-93' bgs)					
LGE GHENT SOIL-WELL LOG - GHENT.GDT - 8/23/16 14:52 - C:\CAROL B GINT\LOS\LOS\_082316.GPJ	SONIC	100	,			100.0 1836.9  LIGNITE, crumbly; brown to black	#40 Sand (93' - 107' bgs) 					
HENT.GDT - 8/23/16 14:52 - C:X	SONIC	100		COAL		106.0 1830.9 107.0 CLAY, hard; gray 1829.9 Bottom of borehole at 107.0 feet.	Total Depth of Well 108.67' BTOC					
LGE GHENT SOIL-WELL LOG - G												

CLIENT Basin					PROJECT NAME _Lelands Olds Landfill PROJECT LOCATION Stanton, ND						
						GROUND ELEVATION 19		HAMMER TY	PE Not Applicable		
						GROUND WATER LEVELS					
RILLING MET											
OGGED BY _	Ryan Klut	te				AT END OF DRILLING					
OORDINATES											
- YPE	ERY	, TSF S.	<u></u>					Casi Casi	ng Top Elev: 2.55 (ft) ng Type: 4" PVC Pipe		
(ft) APLE TY NUMBER	SOV	OMETER, T U.S.C.S.	PH OG		MATE	RIAL DESCRIPTION			WELL DIAGRAM		
SAMPLE TYPE NUMBER	% RECOVERY POCKET PENE-	TROME U.S	GRAPHIC LOG						Top of Casing (estimated 2.8 ags)		
5 SONIC  10 SONIC  20 SONIC	100	CL		FILL - CLAY, rewor					Grout (0' - 111' bgs)  PVC Pipe (2.55' ags - 1: bgs)		

A	<b>ECO</b> A	1				WELL NUM	BER MW-2016-9 PAGE 2 OF 4
	ENT Basi			4340		PROJECT NAME _Lelands Olds Landfill PROJECT LOCATION _Stanton, ND	
HTG 32	(π) SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF		GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
- - - - - - - - - - - - - - - - - - -	SONIC	2 100		CL		FILL - CLAY, reworked; brown	Grout ((0' - 111' bgs)  PVC Pipe (2.55' ags - 130' bgs)
LGE GHENT SOIL-WELL LOG - GHENT,GDT - 12/21/16 15:12 - C:BISMARK GINTAVS LOGS/112816 1215161LOS_082316.GPJ	SONIC	2 100					
LGE GHENT SOIL	-						

Æ	COM	1				WELL NUMB	BER MW-2016-9 PAGE 3 OF 4
CLIEN	T Basin	Elect	ric			PROJECT NAME Lelands Olds Landfill	
	ECT NUM			4340		PROJECT LOCATION Stanton, ND	
DEPTH (ff)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
	SONIC	100		CL		FILL - CLAY, reworked; brown  95.0  CLAY, native material, very hard; gray  1846.5  LIGNITE, clay; gray  1841.5  CLAY, very hard; moist; gray	Grout (0' - 111' bgs) PVC Pipe (2.55' ags - 130' bgs)
   115							■Bentonite Seal (111'-115' bgs)

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 12/21/16 15:12 - C.\BISMARK GINTAVS LOGS\112816 121516\LOS\_082316.GPJ

AEC	<b>XON</b>							WELL N	IUMBER N	/IW-2016-10 PAGE 1 OF	
DATE ST DRILLIN DRILLIN LOGGEI	TARTE IG CON IG MET D BY	IBER D 11 ITRAC HOD Ryan I	6051 /4/201 CTOR Rota Klute	4340 6 Caso ry Sor	cade Dri	COMPLETED _11/5/2016					
	SAMPLE TYPE NUMBER		POCKET PENE- TROMETER, TSF		GRAPHIC LOG		MAT	ERIAL DESCRIPTION	Casir Casir	ng Top Elev: 1.7 (ft) ng Type: 4" PVC Pipe  WELL DIAGRAM  Top of Casing (estimated 1.7' ags)	
5	SONIC					FILL - CLAY, rewo	rked; t	orown		Grout (0' - 114' bgs) PVC Pipe (1.7' ags - 132' bgs)	
20	SONIC	100		CL							
30	SONIC	100									

ΑΞ	COM					WELL NUMBE	PAGE 2 OF 4
CLIEN	IT Basin	Elect	ric			PROJECT NAME Lelands Olds Landfill	
	ECT NUM			4340		PROJECT LOCATION Stanton, ND	
DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
45 50	SONIC					FILL - CLAY, reworked; brown	Grout (0' - 114' bgs) PVC Pipe (1.7' ags - 132' bgs)
	SONIC	100		CL			
75 80	SONIC	100					
  85	SONIC	100					

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 12/21/16 15:10 - C.\BISMARK GINTAVS LOGS\112816 121516\LOS\_082316.GPJ

#### **WELL NUMBER MW-2016-10 AECOM** PAGE 3 OF 4 CLIENT Basin Electric PROJECT NAME Lelands Olds Landfill PROJECT NUMBER 60514340 PROJECT LOCATION Stanton, ND SAMPLE TYPE NUMBER POCKET PENE-TROMETER, TSF % RECOVERY GRAPHIC LOG U.S.C.S. DEPTH (ft) WELL DIAGRAM MATERIAL DESCRIPTION Grout (0' - 114' bgs) PVC Pipe (1.7' ags - 132' FILL - CLAY, reworked; brown bgs) 90 CL 94.0 1857.6 LIGNITE; black and brown 95 SONIC 100 COAL 1855.6 CLAY, very hard; gray 100 .GE GHENT SOIL-WELL LOG - GHENT.GDT - 12/21/16 15:10 - C.\BISMARK GINT\AVS LOGS\112816 121516\LOS\_082316.GPJ 105 SONIC 100 $\mathsf{CL}$ 110 115 SONIC 100 Bentonite Seal (114'-117' bgs) 120 122.0 1829.6 LIGNITE; brown 125 #60 (top 2') and #40 Sand (117' - 132.5' SONIC 100 COAL bgs) 0.010 Slotted Pipe (122' - 132' bgs) 130 1821.6 CLAY, very hard; gray CL

# WELL NUMBER MW-2016-10 PAGE 4 OF 4

	IT <u>Basin</u> ECT NUM			4340		PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton, ND					
DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM				
135	SONIC	100		CL		CLAY, very hard; gray  LIGNITE (<1")		Total Depth of Well 133.70' BTOC			
140    145	SONIC	100		IDSTO	ONE DNE	SANDSTONE, unconsolidated; gray and light brown  LIMESTONE  Bottom of borehole at 145.0 feet.		Fill Below We <sup>i</sup> ll			

Bottom of borehole at 145.0 feet.

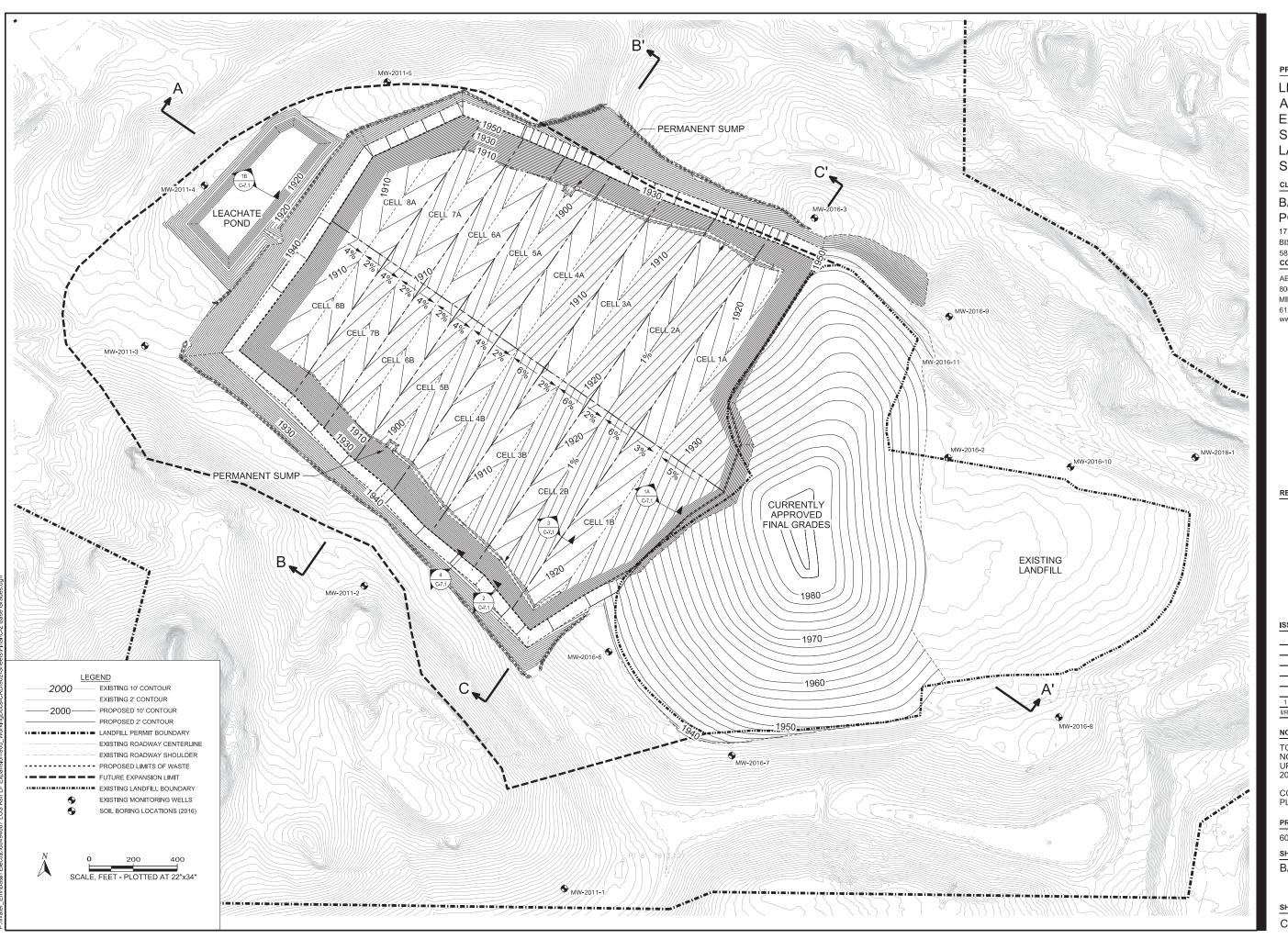
AE(	CON							WELL N	UMBER N	MW-2016-11 PAGE 1 OF	
DATE S DRILLIN DRILLIN LOGGE	CT NUM TARTE NG CON NG MET D BY	IBER D 11 ITRAC HOD Ryan I	6051 /18/20 CTOR Rota Klute	4340 016 Caso ry Sor	cade Dr	COMPLETED 11/20/2016 rilling	PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton, ND  GROUND ELEVATION 1954.851 ft HAMMER TYPE Not Applicated HAMMER T				
	SAMPLE TYPE NUMBER		POCKET PENE- TROMETER, TSF		GRAPHIC LOG		MAT	ERIAL DESCRIPTION	Casir Casir	ng Top Elev: 1.2 (ft) ng Type: 4" PVC Pipe  WELL DIAGRAM  Top of Casing (estimated 1.2' ags)	
5 5 10 15	SONIC					FILL - CLAY, rewor	ked; t	prown		Grout (0' - 120' bgs) PVC Pipe (1.2' ags - 140' bgs)	
20	SONIC	100		CL							
30	SONIC	100									

ΑĒ	COM					WELL NUMBE	ER MW-2016-11 PAGE 2 OF 4	
CLIEN	T Basin	Elect	ric			PROJECT NAME Lelands Olds Landfill		
	ECT NUM			4340		PROJECT LOCATION Stanton, ND		
(#) OEPTH	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM	
45	SONIC	100				FILL - CLAY, reworked; brown	Grout (0' - 120' bgs) PVC Pipe (1.2' ags - 140' bgs)	
55   60	SONIC	100						
 65   70	SONIC	100		CL				
80	SONIC	100				CLAV reworked; brown		
   85	SONIC	100				CLAY, reworked; brown trace lignite fragments		

LGE GHENT SOIL-WELL LOG - GHENT.GDT - 12/21/16 15:11 - C.\BISMARK GINTAVS LOGS\112816 121516\LOS\_082316.GPJ

	AE	CON	1				WELL NUMBI	ER MV	<b>V-2016-11</b> PAGE 3 OF 4
		T Basir			4340		PROJECT NAME Lelands Olds Landfill PROJECT LOCATION Stanton, ND		
	DEPTH (ft)	SAMPLE TYPE NUMBER	% RECOVERY	POCKET PENE- TROMETER, TSF		GRAPHIC LOG	MATERIAL DESCRIPTION	WE	ELL DIAGRAM
	90				CL		FILL - CLAY, reworked; brown  94.0 1860.5		Grout (0' - 120' bgs) PVC Pipe (1.2' ags - 140' bgs)
	95	SONIC	100	SAN	IDST		SANDSTONE/CHERT, unconsolidated, reworked material; orange  97.0  FILL - CLAY, reworked; brown and orange  100.0  1854.9		
182316.GPJ	   105	SONIC	100		CL		FILL - CLAY, reworked, minor lignite fragments; brown and orange  103.0  FILL - CLAY, reworked material; orange  106.0  1848.5		
12816 121516\LOS_C	   110				CL		CLAY/SILT, very hard; gray  LIGNITE (<1")  CLAY, crumbly, native material; gray		
LGE GHENT SOIL-WELL LOG - GHENT.GDT - 12/21/16 15:11 - C.\BISMARK GINTAVS LOGS\112816 121516\LOS_082316.GPJ		SONIC	100		CL		120.0 1834.S		
LOG - GHENT.GDT - 12/21/	   125	SONIC	100		CL		CLAY, very hard; gray		■Bentonite Seal (120'-124' bgs)
LGE GHENT SOIL-WELL	   130	SONIC	100		COAL		128.0 LIGNITE, minor moisture present in fractures; brown and black		

# Appendix C – Permitted Base Grade Plan Sheet



PROJECT

LELAND OLDS STATION ASH LANDFILL EXPANSION - PHASE 6 SPECIAL WASTE LANDFILL PERMIT SP-143

CLIENT

# BASIN ELECTRIC POWER COOPERATIVE

1717 EAST INTERSTATE AVE BISMARCK, NORTH DAKOTA 58503-0564 CONSULTANT

FCOM

800 LASALLE AVENUE, SUITE 500 MINNEAPOLIS, MN 55402 612-376-2000 tel 612-376-2271 fax www.aecom.com

REGISTRATION



ISSUE/REVISION

1	2017-02-24	ISSUED-PERMIT SUBMITTAL
I/R	DATE	DESCRIPTION
_		

NOTES

TOPOGRAPHIC SURVEY BY KBM, NOVEMBER 2015. TOPOGRAPHY UPDATED BY BEPC, OCTOBER 5, 2016.

COORDINATES ARE ND STATE PLANE SOUTH, NAD 1929.

PROJECT NUMBER

60494667

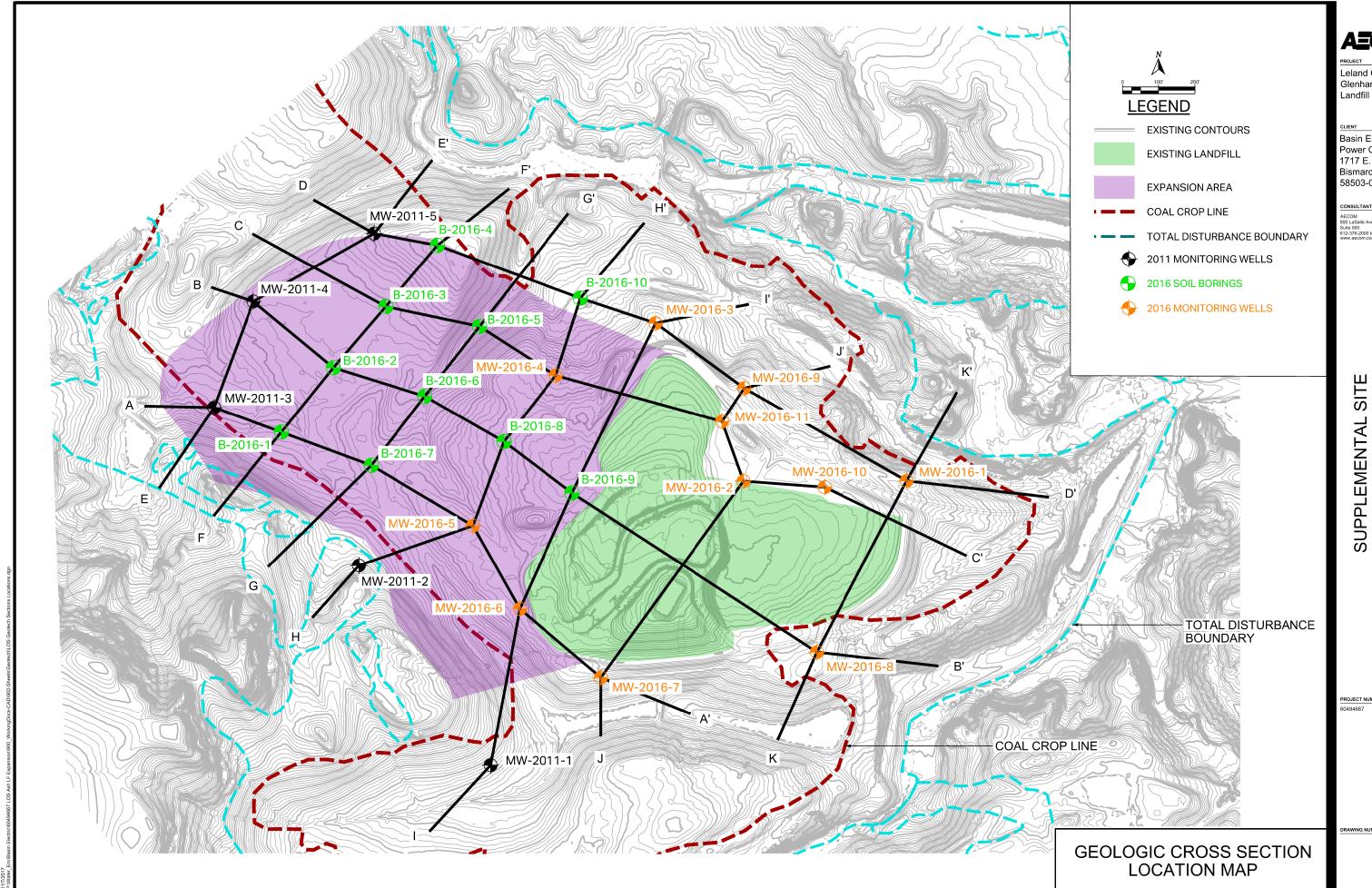
SHEET TITLE

BASE GRADES

SHEET NUMBER

C-2 (

# **Appendix D – Geologic Cross Sections**



Leland Old Station Glenharold Mine Landfill Expansion

Basin Electric Power Cooperative 1717 E. Interstate Ave Bismarck, ND 58503-0564

SUPPLEMENTAL SITE CHARACTERIZATION REPORT

ulte 500 12-376-2000 tel 612-376-2271 fax www.aecom.com



PROJECT NUMBER

LEGEND OF THE **GEOLOGIC CROSS SECTIONS** 

50'

40'

30'

20'

10'

**BOTTOM OF** 

SCREENED ZONE

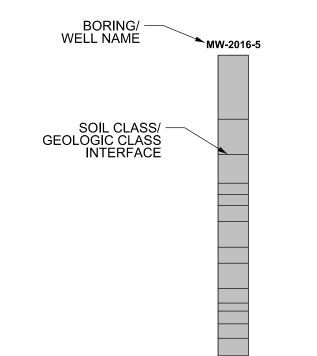
SEAL

200'

NOTE: VERTICAL EXAGGERATION = 15X

**EXISTING GRADE** PROPOSED EXPANSION BASE GRADE PROPOSED EXPANSION FINAL GRADE EXISTING LANDFILL BASE GRADE EXISTING LANDFILL FINAL GRADE CONTACT BETWEEN GEOLOGIC UNITS INFERRED CONTACT BETWEEN GEOLOGIC UNITS PIEZOMETRIC SURFACE (SEPT. 27, 2016, 3rd QUARTER)

FILL (SEE LOGS FOR DESCRIPTIONS) COAL/LIGNITE CLAY SANDSTONE SILTY CLAY **CLAYEY SAND** LIMESTONE

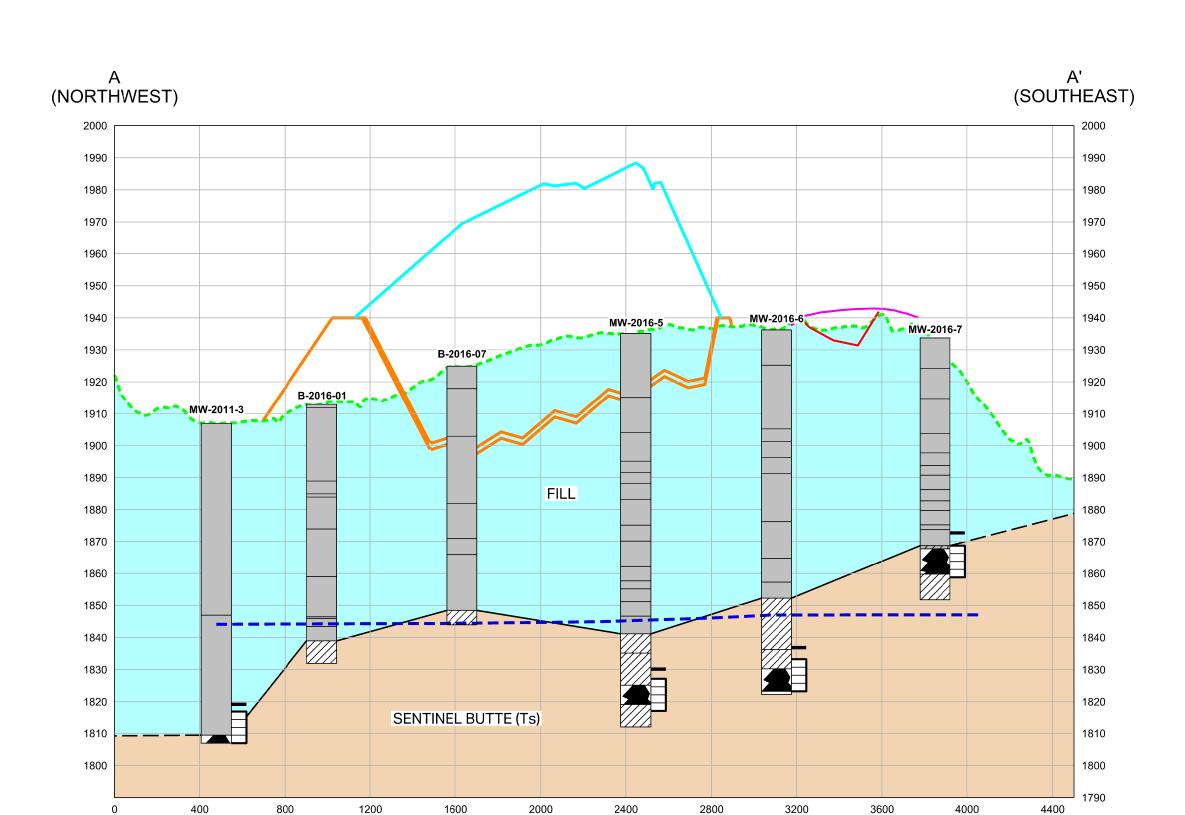


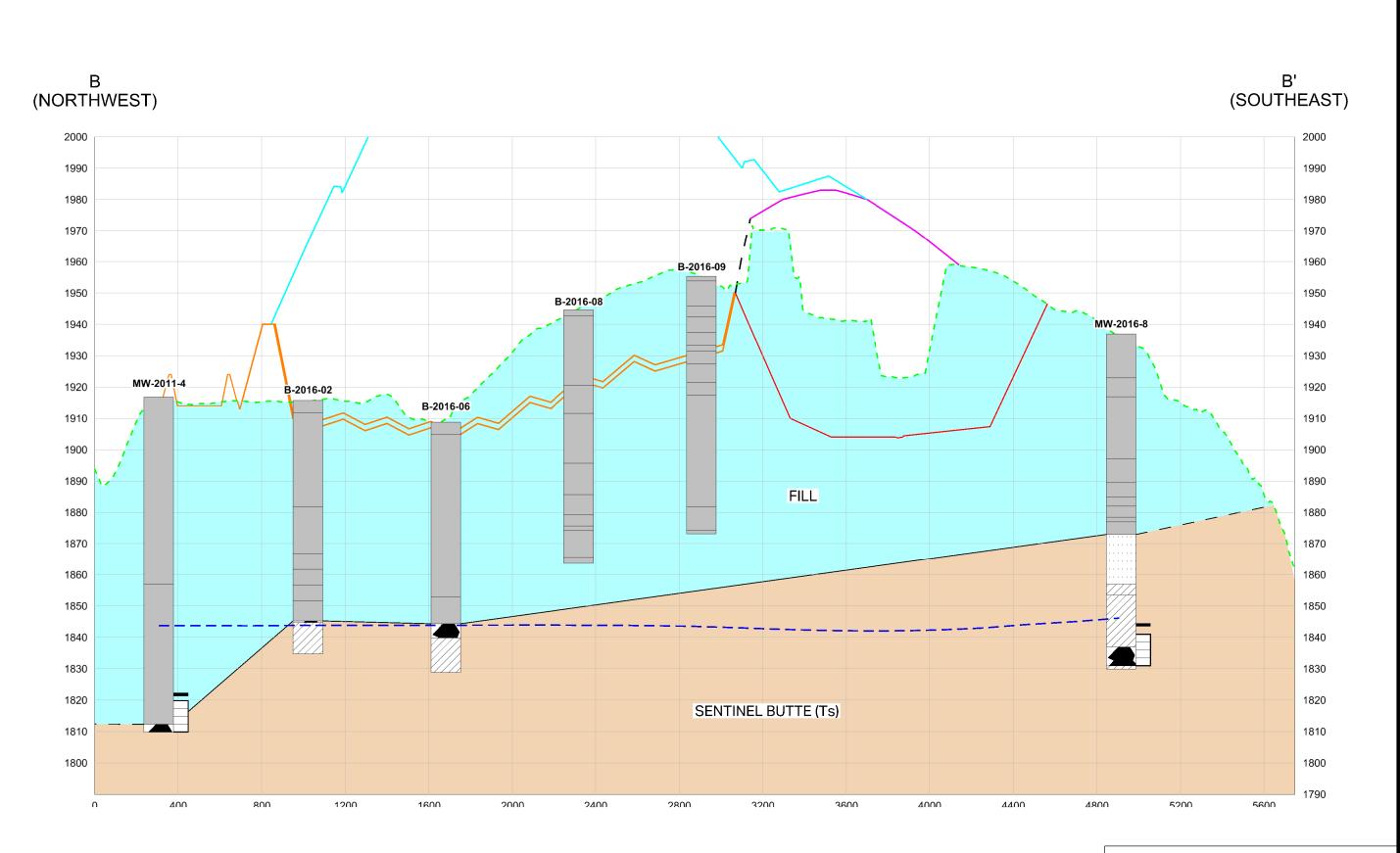
### NOTES:

- ELEVATIONS ARE BASED ON THE NORTH AMERICAN VERTICAL DATUM OF 1927 HORIZONTAL DATUM IS BASED ON THE NORTH DAKOTA STATE PLANE COORDINATE SYSTEM OF 1927 SOUTH ZONE.
- BORING LOG ELEVATIONS REPRESENT GROUND SURFACE ELEVATIONS AT THE TIME OF DRILLING.
- FINAL BORING LOGS BASED ON FIELD VISUAL IDENTIFICATION AND GEOTECHNICAL LABORATORY TEST RESULTS.
- THE DEPTH AND THICKNESS OF SUBSURFACE STRATA INDICATED ON THESE CROSS-SECTIONS WERE GENERALIZED FROM AND INTERPOLATED BETWEEN BORINGS. INFORMATION ON ACTUAL SUBSURFACE CONDITIONS EXISTS ONLY AT THE LOCATION OF THE BORINGS.
- 5. GROUNDWATER ELEVATIONS WERE OBTAINED ON SEPTEMBER 27, 2016.

Landfill Expansion

GEOLOGIC CROSS SECTION A - A'





PROJECT

Leland Old Station Glenharold Mine Landfill Expansion

CLIENT

Power Cooperative
1717 E. Interstate Ave
Bismarck, ND
58503-0564

SULTANT

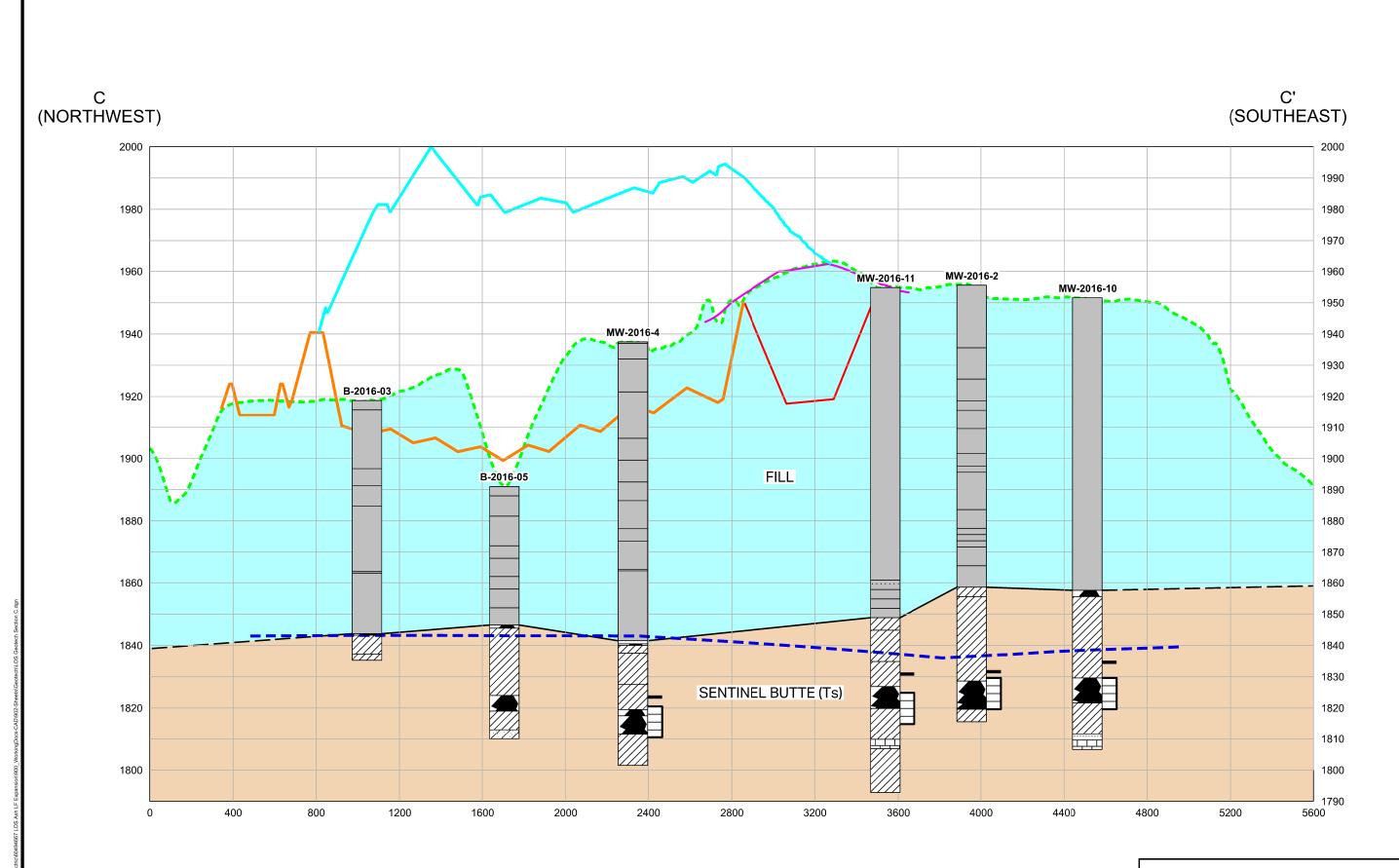
AECOM 800 LaSalle Ave. Suite 500

w.accom.com

LOCATION RESTRICTIONS REPORT

60545172

DRAWING NU



PROJECT

Leland Old Station Glenharold Mine Landfill Expansion

CLIENT

Basin Electric Power Cooperative 1717 E. Interstate Ave Bismarck, ND 58503-0564

NSULTANT

ECOM 00 LaSalle Ave. uite 500

SUPPLEMENTAL SITE CHARACTERIZATION REPORT

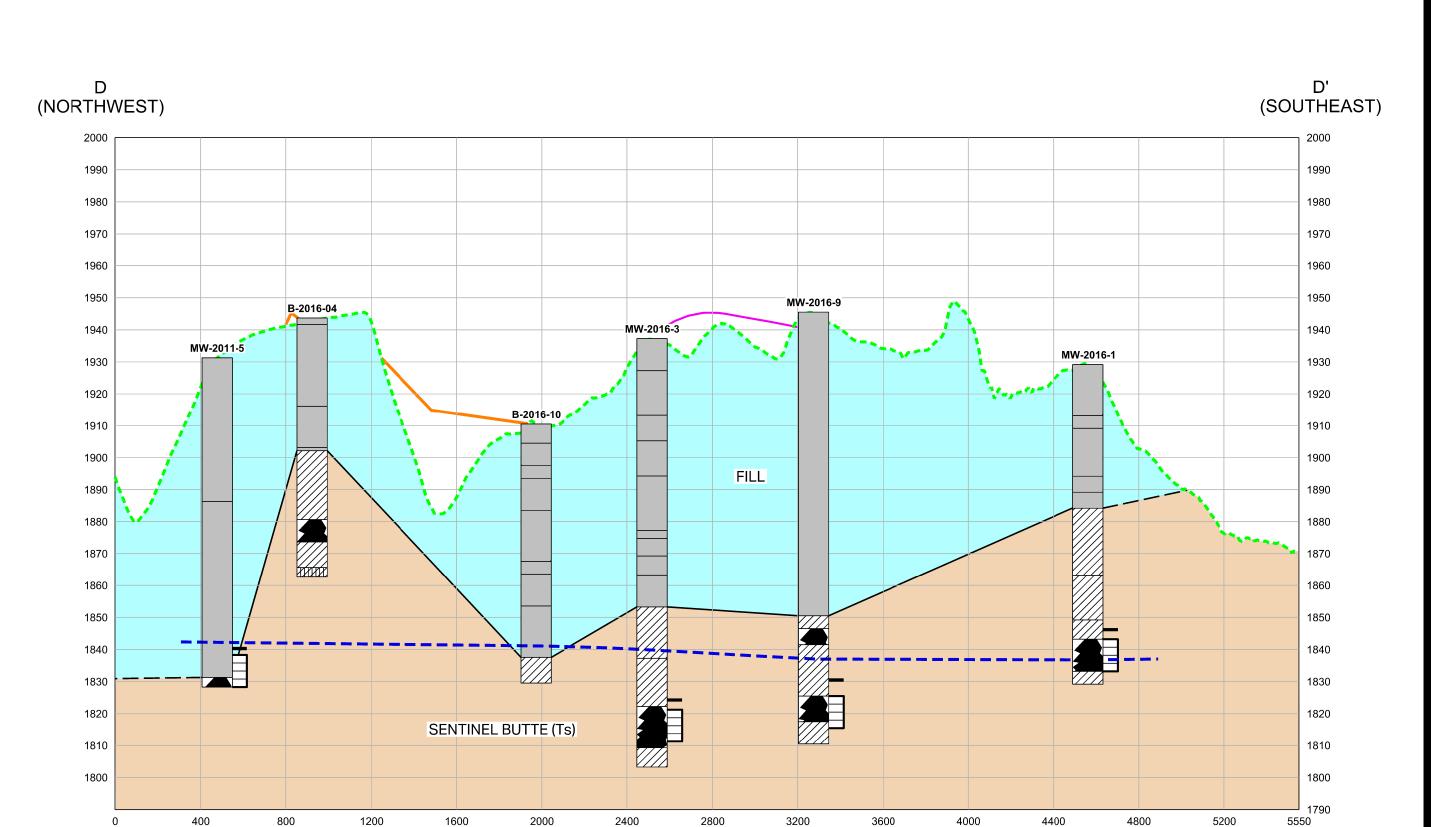
ROJECT NUMBER

494667

DRAWING NUM

DRAWING

GEOLOGIC CROSS SECTION C - C'



Leland Old Station Glenharold Mine Landfill Expansion

Basin Electric Power Cooperative 1717 E. Interstate Ave Bismarck, ND 58503-0564

SUPPLEMENTAL SITE CHARACTERIZATION REPORT

GEOLOGIC CROSS SECTION D - D'

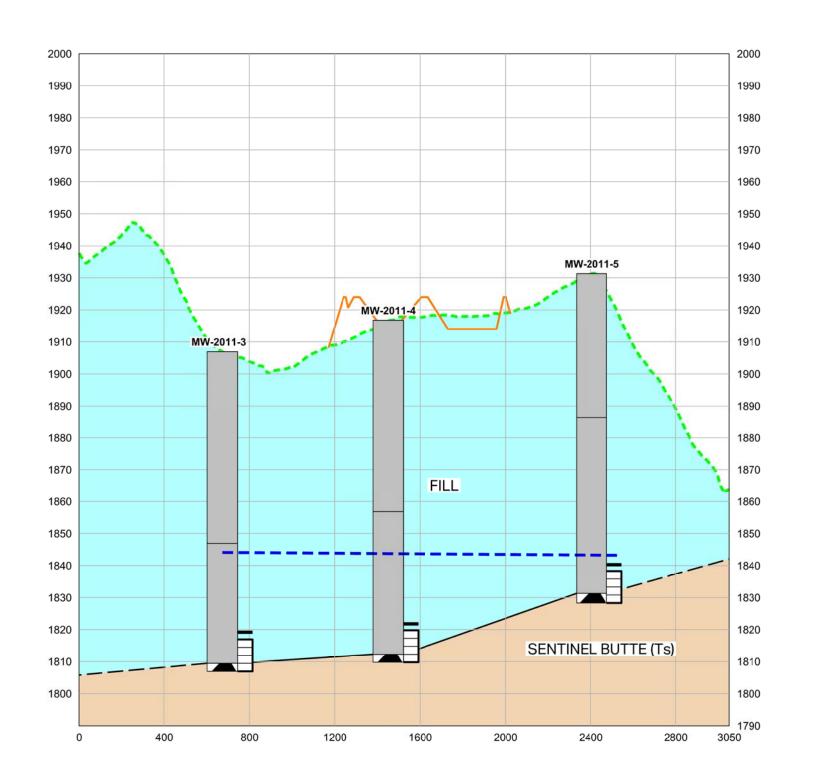
E' (NORTHEAST)

PROJECT NUMBER 60545172

.....

GEOLOGIC CROSS SECTION E - E'

E (SOUTHWEST)



F' (NORTHEAST)

CONSULTANT

AECOM 800 LaSalle Ave. Suite 500

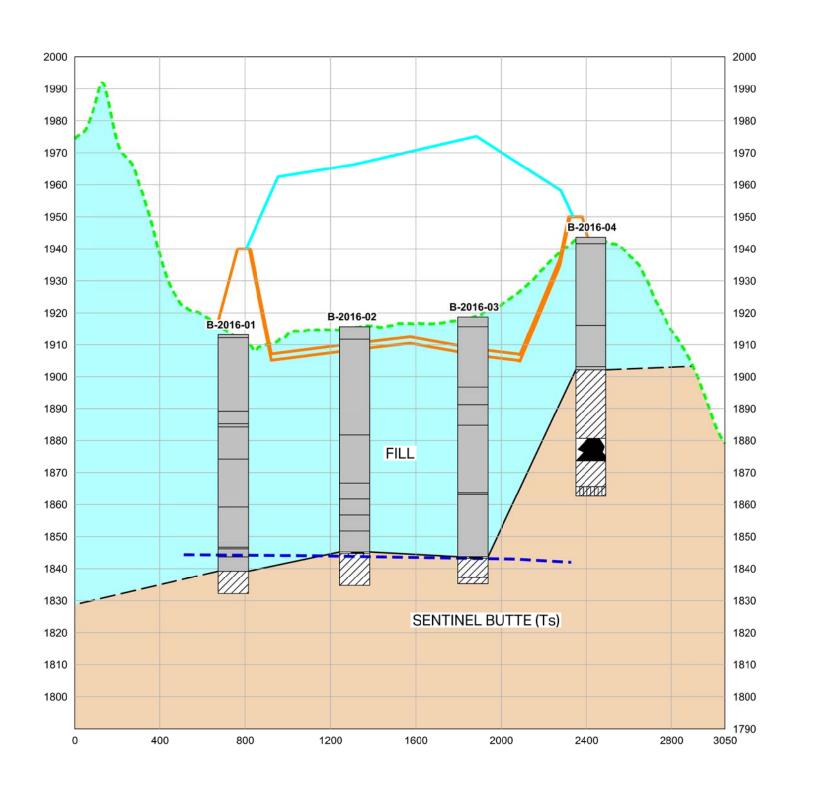
LOCATION RESTRICTIONS REPORT

PROJECT NUMBE 60545172

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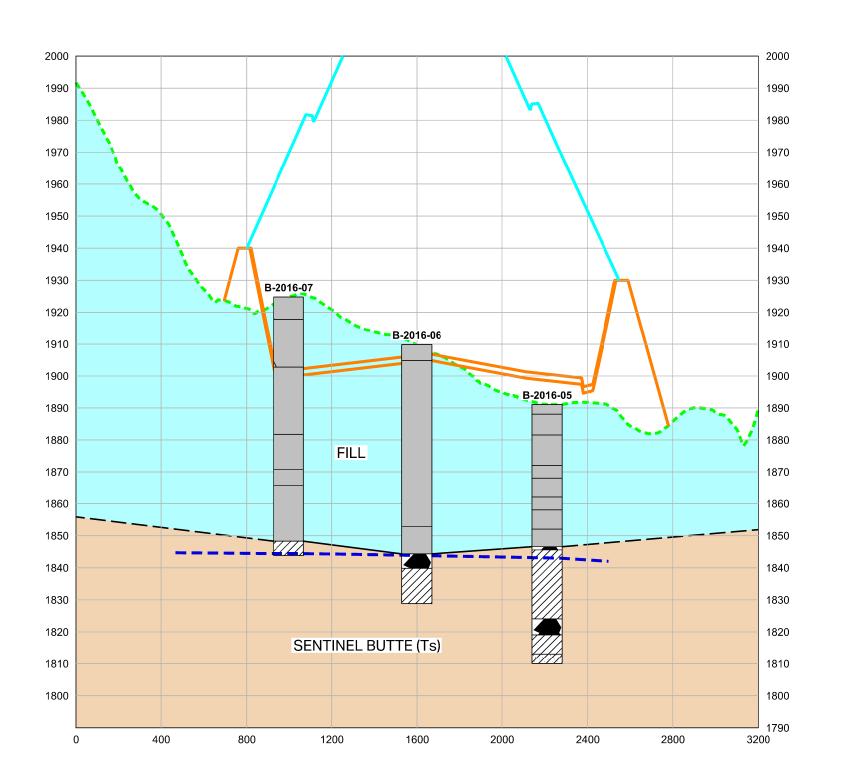
GEOLOGIC CROSS SECTION F - F'

F (SOUTHWEST)



GEOLOGIC CROSS SECTION G - G'

G (SOUTHWEST)



G' (NORTHEAST)

Basin Electric Power Cooperative 1717 E. Interstate Ave Bismarck, ND 58503-0564

**AECOM** 

Leland Old Station Glenharold Mine Landfill Expansion

LOCATION RESTRICTIONS REPORT

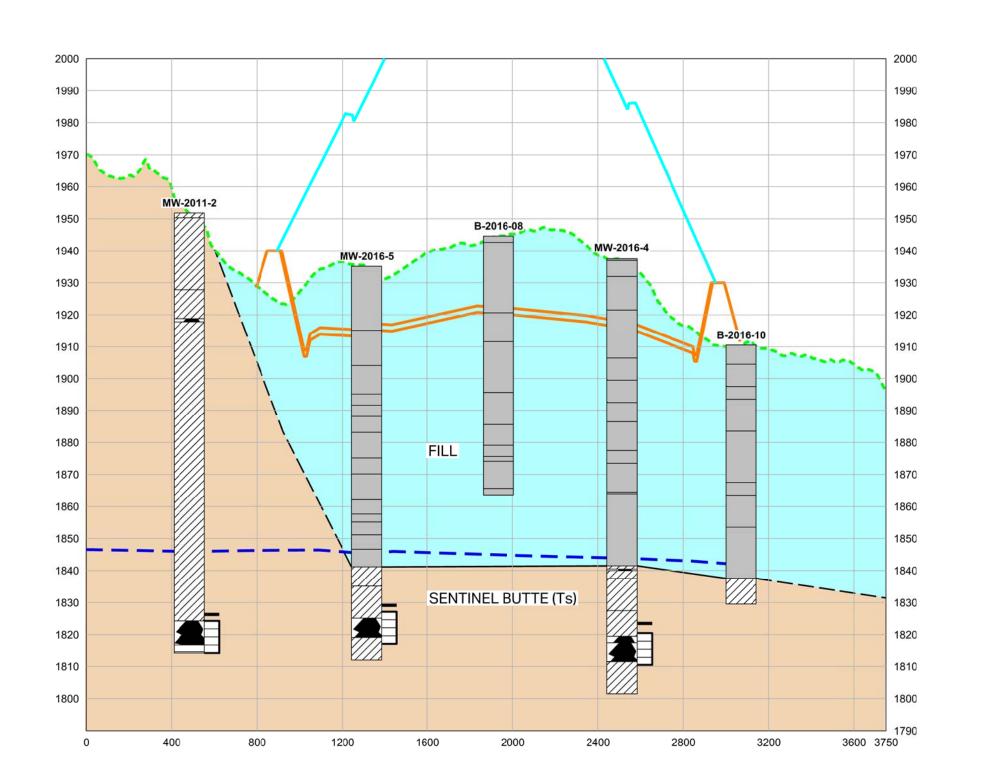
H' (NORTHEAST)

LOCATION RESTRICTIONS REPORT

60545172

GEOLOGIC CROSS SECTION H - H'

H (SOUTHWEST)



Leland Old Station
Glenharold Mine
Landfill Expansion

CLIENT

Basin Electric
Power Cooperative

1717 E. Interstate Ave Bismarck, ND

**AE**COM

CONSULTANT

58503-0564

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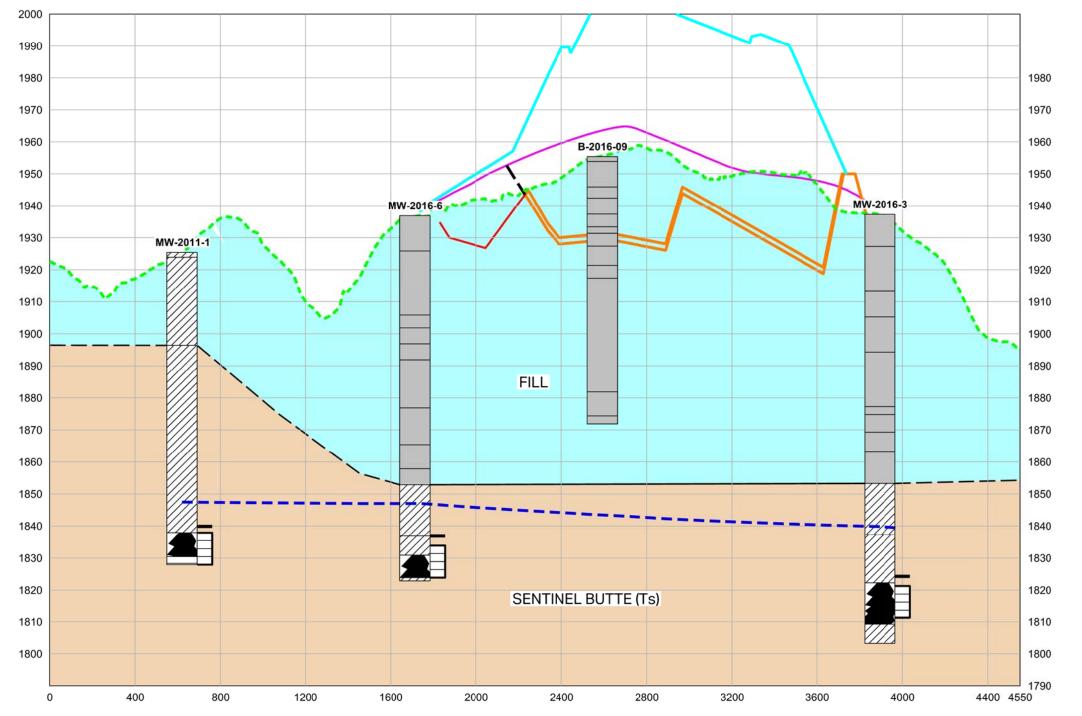
LOCATION RESTRICTIONS REPORT

PROJECT NUMBER 60545172

\_\_\_\_\_

GEOLOGIC CROSS SECTION I - I'

I' (SOUTH) (NORTHEAST)



J' (NORTHEAST) 2000 2000 1990 1980 1980 1970 1960 1960 MW-2016-2 MW-2016-11 MW-2016-9 1950 1940 1940 MW-2016-7 1930 1920 1920 1910 1900 1900 1890 FILL 1880 1880 1870 1860 1860 1850 1840 1840 1830 1820 1820 SENTINEL BUTTE (Ts) 1810 1800 1800 1790 800 1600 2000 2400 3200 3400 400 1200 2800

J (SOUTH) AECOM

PROJEC

Leland Old Station Glenharold Mine Landfill Expansion

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Basin Electric Power Cooperative 1717 E. Interstate Ave Bismarck, ND 58503-0564

CONSULTANT

AECOM 800 LaSalle Ave. Suite 500 612-376-2000 tel 612-376-2271 www.aecom.com

PROJECT NUMBER

0494667

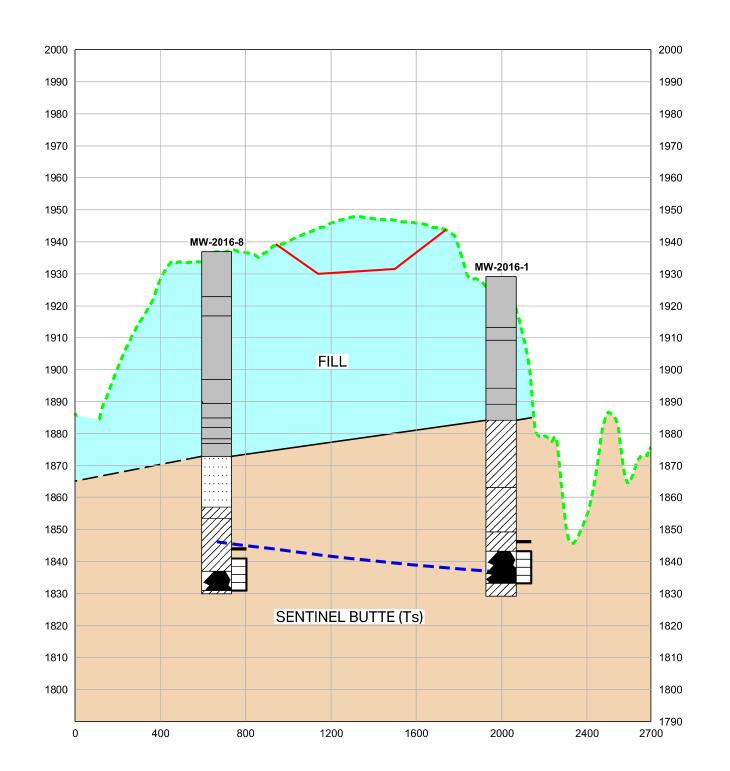
DRAWING NU

GEOLOGIC CROSS SECTION J - J'

K' (NORTHEAST)

GEOLOGIC CROSS SECTION K - K'

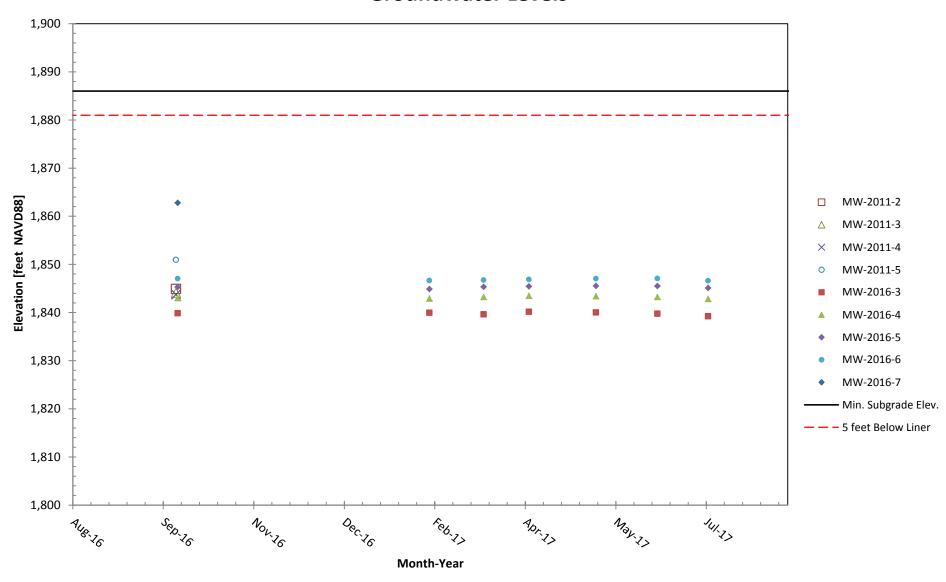
K (SOUTH)



# **Appendix E – Groundwater Data**

Location Restriction Report Figure 3.4

## LOS Ash Landfill Expansion Groundwater Levels



#### **Groundwater Level Data Collected Since 2012**

2011 Wells - Groundwater Data

Well ID	MW	/-2011-1	MW-2	2011-2	MW-2	2011-3	MW-2	2011-4	MW-2011-5	
Reference Elevation Top of Casing* (ft, NAVD88)	19	28.39	195	4.80	191	0.09	191	9.80	193	4.26
Date	DTW (feet)	GW Elev. (ft, NAVD88)								
2/21/2012	77.88	1850.51	106.23	1848.57	62.3	1847.79	72.33	1847.47	81.44	1852.82
4/17/2012	78.42	1849.97	106.94	1847.86	62.9	1847.19	73.99	1845.81	82.23	1852.03
7/31/2012	79.06	1849.33	107.7	1847.10	63.68	1846.41	73.78	1846.02	82.13	1852.13
10/8/2012	79.27	1849.12	108.06	1846.74	64.03	1846.06	74.15	1845.65	82.01	1852.25
1/9/2013	79.64	1848.75	108.44	1846.36	64.48	1845.61	74.58	1845.22	82.6	1851.66
5/6/2013	80.04	1848.35	108.75	1846.05	64.84	1845.25	74.97	1844.83	82.77	1851.49
7/29/2013	79.48	1848.91	108.25	1846.55	64.3	1845.79	74.42	1845.38	82.55	1851.71
10/7/2013	79.14	1849.25	107.95	1846.85	63.94	1846.15	74.01	1845.79	82.42	1851.84
5/12/2014	80.14	1848.25	108.69	1846.11	64.77	1845.32	74.85	1844.95	82.64	1851.62
9/22/2014	79.3	1849.09	108.17	1846.63	64.16	1845.93	74.2	1845.60	82.05	1852.21
4/13/2015	80.17	1848.22	109.4	1845.40	64.69	1845.40	74.72	1845.08	82.34	1851.92
9/27/2016	80.95	1847.44	109.89	1844.91	65.98	1844.11	76.05	1843.75	83.29	1850.97

#### 2016 Wells - Groundwater Data

Well ID	MW-2016-1		MW-2016-2		MW-2016-3		MW-2016-4		MW-2016-5		MW-2016-6	
Reference Elevation Top of Casing* (ft, NAVD88)	1931.73		1957.98		1939.88		1939.97		1937.54		1939.31	
Date	DTW (feet)	GW Elev. (ft, NAVD88)										
9/28/2016	94.97	1836.76	121.99	1835.99	100.04	1839.84	96.96	1843.01	92.24	1845.30	92.29	1847.02
1/25/2017	NM	NM										
2/14/2017	95.59	1836.14	115.22	1842.76	99.92	1839.96	97.05	1842.92	92.65	1844.89	92.69	1846.62
3/16/2017	93.04	1838.69	123.02	1834.96	100.27	1839.61	96.72	1843.25	92.20	1845.34	92.58	1846.73
4/10/2017	92.94	1838.79	118.36	1839.62	99.73	1840.15	96.50	1843.47	92.10	1845.44	92.45	1846.86
5/17/2017	92.55	1839.18	116.32	1841.66	99.85	1840.03	96.57	1843.40	91.99	1845.55	92.26	1847.05
6/20/2017	92.70	1839.03	116.26	1841.72	100.13	1839.75	96.71	1843.26	92.03	1845.51	92.24	1847.07
7/18/2017	93.20	1838.53	118.18	1839.80	100.66	1839.22	97.12	1842.85	92.44	1845.10	92.70	1846.61

Well ID	MW-2016-7		MW-2016-8		MW-2016-9		MW-2	016-10	MW-2016-11	
Reference Elevation	1936.11		1939.36		1947.39		1953.32		1956.73	
Top of Casing* (ft, NAVD88)	1330.11				== :: .03		1333.32		======	
Date	DTW (feet)	GW Elev. (ft, NAVD88)								
9/28/2016	73.31	1862.80	93.21	1846.15	NM	NM	NM	NM	NM	NM
1/25/2017	NM	NM	NM	NM	109.22	1838.17	112.1	1841.22	117.26	1839.47
2/14/2017	NM	NM	92.77	1846.59	116.77	1830.62	112.12	1841.20	124.68	1832.05
3/16/2017	NM	NM	92.66	1846.70	113.65	1833.74	111.60	1841.72	123.05	1833.68
4/10/2017	NM	NM	92.36	1847.00	113.57	1833.82	111.20	1842.12	122.60	1834.13
5/17/2017	NM	NM	92.62	1846.74	111.30	1836.09	111.56	1841.76	119.91	1836.82
6/20/2017	NM	NM	92.71	1846.65	113.43	1833.96	111.69	1841.63	121.12	1835.61
7/18/2017	NM	NM	92.97	1846.39	115.69	1831.70	112.03	1841.29	123.09	1833.64

NAVD = North American Vertical Datum of 1988 (NAVD 88)

NM = Not Measured (Well did not exist or no longer sampled)

DTW = Depth To Water

GW = Groundwater

# **Appendix F – Environmental and Wetland Delineation Report** (Excerpt)

#### **EXECUTIVE SUMMARY**

Basin Electric Power Cooperative (BEPC) contracted AECOM to conduct wetland delineations within the ash landfill expansion (Project) near Stanton, North Dakota in Mercer County. The purpose of this report is to provide a summary of the available desktop data and wetland delineations conducted on August 19, 2016 and an evaluation of potential waters of the U.S. (WOTUS). A desktop analysis and literature search were also conducted to identify federally listed species of concern with the potential to occur within the proposed Project area.

One soil type was found within the Project area, mined land complex with 0 to 60 percent slopes (Figure 4-1). The mined land complex soils are not characterized as having hydric characteristics. Hydrology of the Project area is influenced by drainages and creeks contributing to the Missouri River, and the Project area is entirely within the Missouri River Basin. Historically, the dominant natural vegetation type of the Project area is shortgrass prairie (Dyke, S.R., S.K. Johnson, and P.T. Isakson. 2015. North Dakota State Wildlife Action Plan. North Dakota Game and Fish Department, Bismarck, ND). Found mostly in the Missouri Slope ecoregion of North Dakota, this vegetation type is dominated by warm season species that can survive on little rainfall (Figure 4-2).

A desktop analysis and literature search were conducted to identify federally listed species of concern with the potential to occur within the proposed Project area. Using the United States Fish and Wildlife Service's (USFWS's) Information for Planning and Conservation tool, AECOM identified seven threatened and endangered (T&E) species of concern and assigned each a determination of affect. North Dakota does not have a state endangered or threatened species list; only those species listed by the Endangered Species Act are considered threatened or endangered in North Dakota, and the USFWS has primary oversight over these species.

A no effect determination was given to the least tern (*Sterna antillarum*), piping plover (*Charadrius melodus*), red knot (*Calidris canutus rufa*), whooping crane (*Grus Americana*), pallid sturgeon (*Scaphirhynchus albus*), gray wolf (*Canis lupus*), and northern long-eared bat (*Myotis septentrionalis*). Additionally, no T&E species were observed during the field survey on August 19, 2016.

AECOM conducted a desktop evaluation of wetlands to determine potential United States Army Corps of Engineers (USACE) jurisdictional waters. Potential impacts to WOTUS are subject to USACE permitting under Section 404 of the Clean Water Act. The Project area lies entirely within the Omaha District of the USACE. The Project area evaluated by AECOM contains two mapped National Wetlands Inventory (NWI) features and one National Hydrography Dataset (NHD) tributary (Figure 4-3). The two NWI features did not meet wetland criteria in the field. The NHD-mapped creek appeared to be an upland drainage that flowed into Alderin Creek. This drainageway did not contain hydrophytic vegetation or an ordinary high water mark.

Four wetlands were delineated within the Project area (Figures 4-4, 4-5 and 4-6). AECOM has evaluated the characteristics of Wetland-1, Wetland-2, Wetland-3, and Wetland-4 and has come to the conclusion that these wetlands appear to be non-relatively permanent waters (non-RPW) that are formed by geomorphic position, are isolated from jurisdictional waters, and appear to be without significant nexus. Wetlands-1-3 formed following the mineland reclamation when soils settled forming small basins. Wetland-4 is a depressional wetland formed within a ditch created during the construction of the adjacent road.

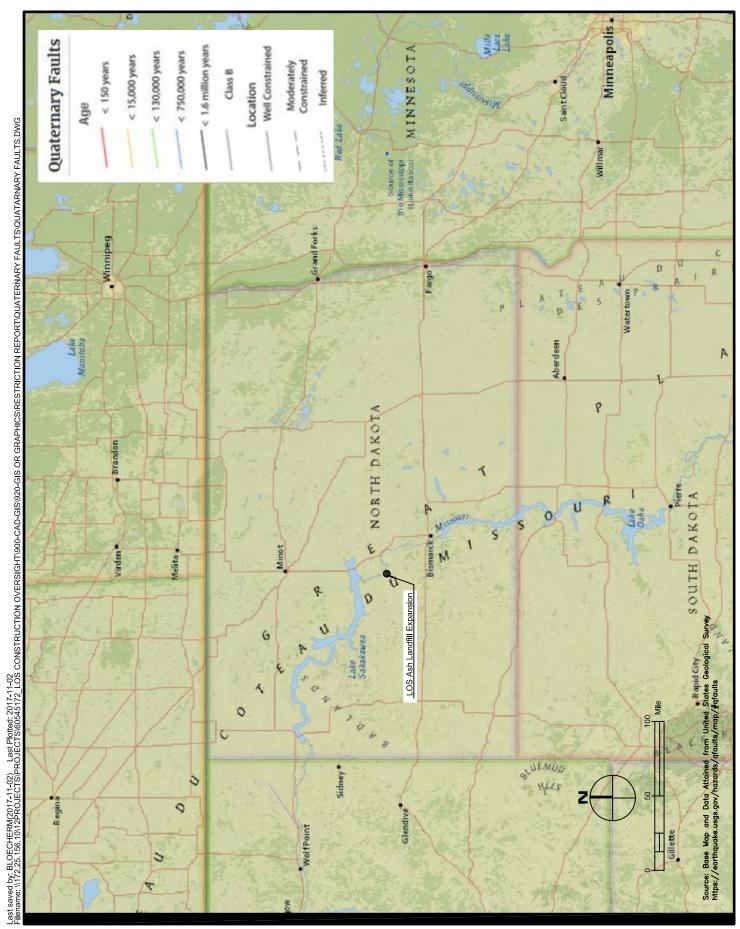
However, these are the recommendations of AECOM based on our experience, observations and data collected in the field, and best professional judgement. The final authority over wetland jurisdiction is the responsibility of the USACE. AECOM recommends that an official jurisdictional determination (JD) is obtained from the USACE for the wetlands and drainageway in question.

#### STATEMENT OF LIMITATIONS

This report was prepared by the staff of AECOM under the supervision of experienced professionals. The data interpretation, conclusions, and recommendations presented in the report were governed by AECOM's experience and professional judgment. This report has been prepared based on data current at

the time of preparation. Assumptions based on this data, although believed reasonable and appropriate based on the data provided herein, may not prove to be true in the future as new data are collected. The conclusions and recommendations of AECOM are conditioned upon these assumptions.	,

# **Appendix G – Geologic Maps**



Location Restrictions Report LOS Ash Landfill Expansion Basin Electric Power Cooperative Project No.: 60545172 2017-03-14 Quaternary Faults in Proximity to Leland Olds Station Mercer County, North Dakota



